

Beyond-CMOS computing: non-von Neumann architectures for ML

MAS General Exam

Camron Blackburn

4 | 12 | 24

Exam Content

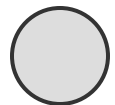
Dissertation (broad) Objective:

to propose a new computing framework for ultra-low power computing with devices which have the capability of reaching fundamental physical limits for information processing and an architecture that can optimally map software applications to efficient hardware

Required understanding:



Non-von Neumann Architectures for Energy Efficient Computing



Superconducting Device Physics and Electronics Design



Fundamental Physical Limits to Information Processing



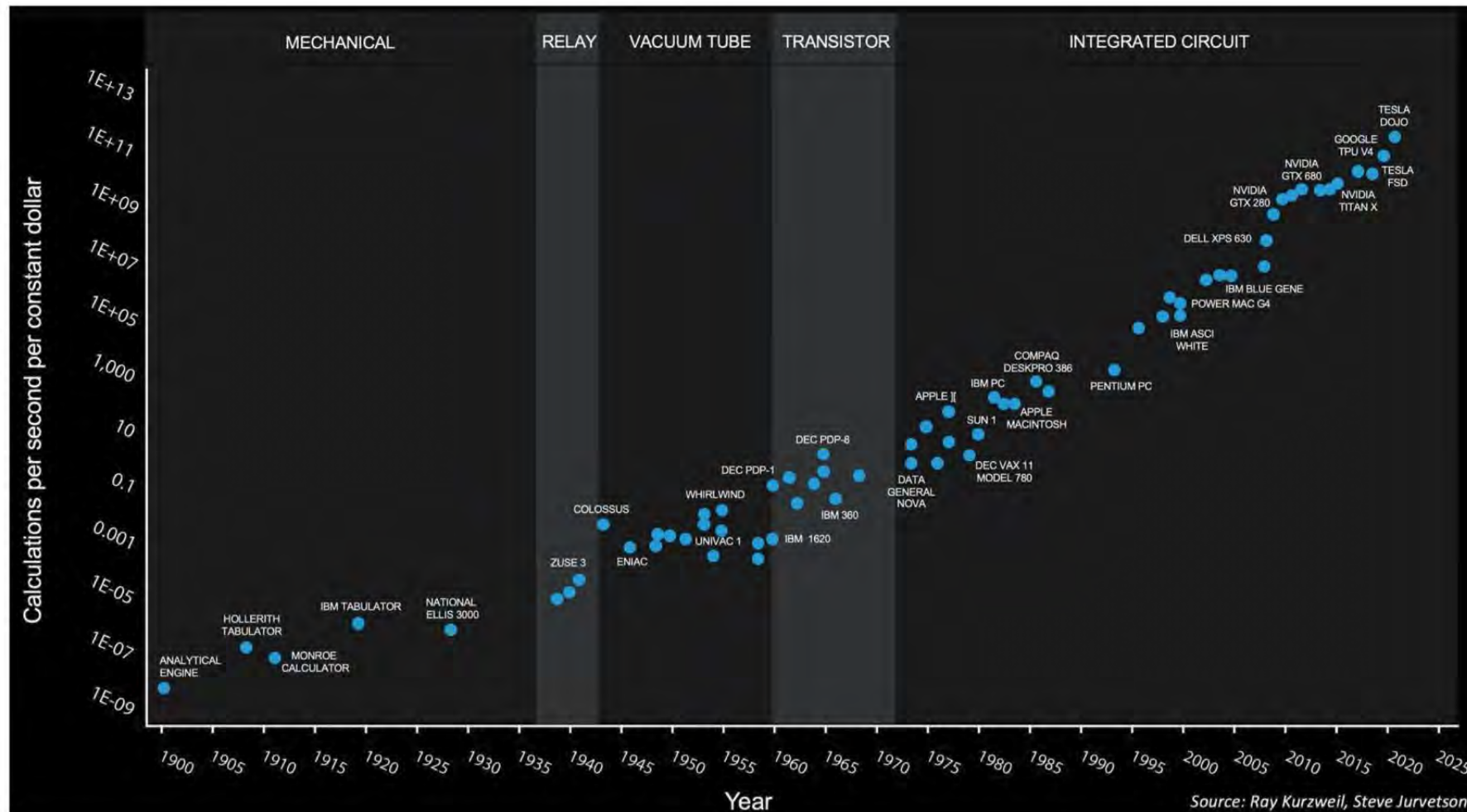
Non-von Neumann Architectures for Energy Efficient Computing



CONTENTS

- Current state of High-Performance Computing
- Computing Architecture Categorizations
- Metrics for evaluating computing systems
- Coarse-grain Reconfigurable Architectures (CGRAs)
- Globally Asynchronous, Locally Synchronous (GALS) pipelining methods
- DNN Accelerator Design
- Tools for modeling DNN Accelerator architectures
 - AQFP implementation

1. The State of High-Performance Computing

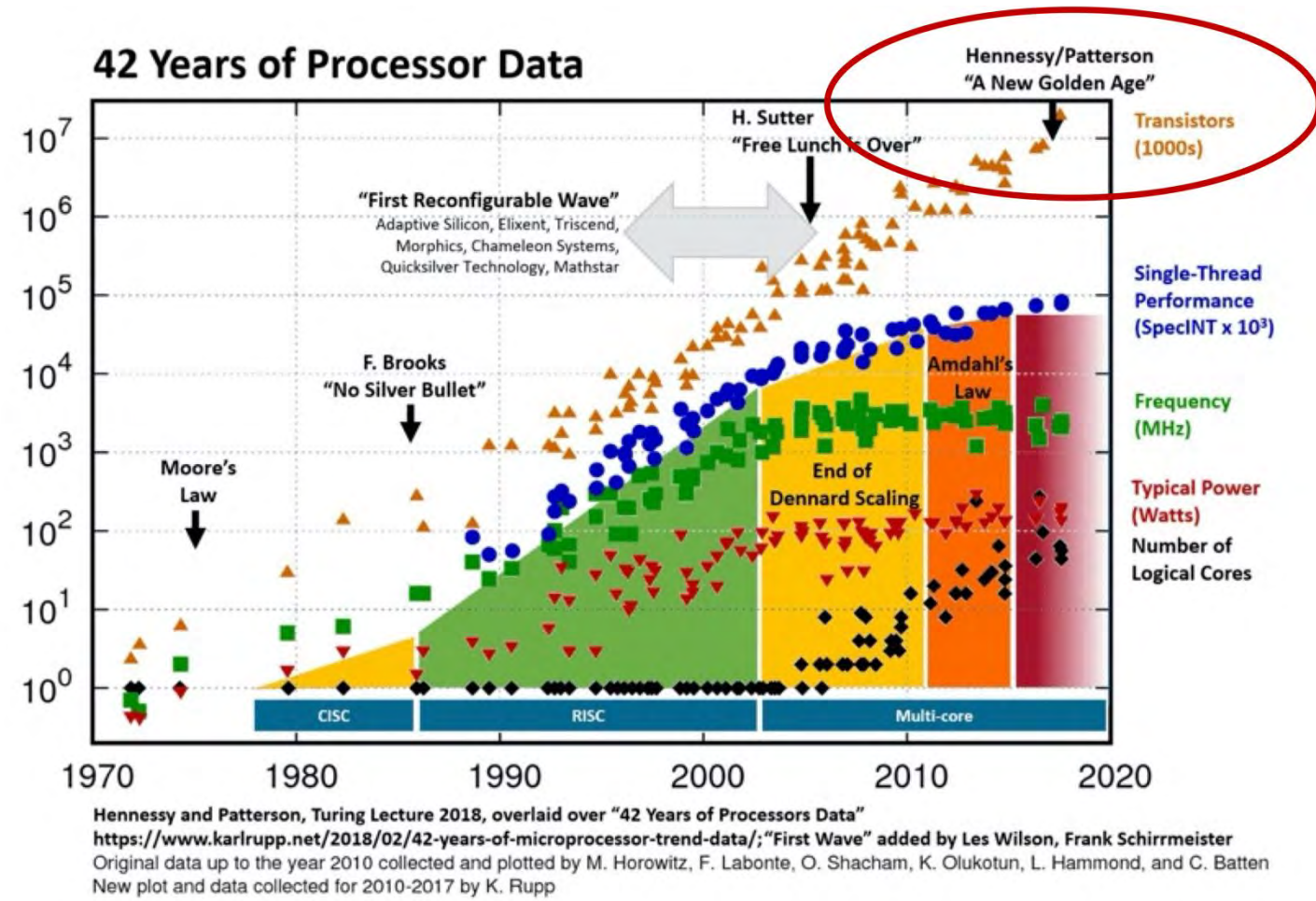


1. Scaling laws slowing down



Scaling laws that enabled the boom in IC development over the last 50 years are slowing down

- Moore's Law
- Dennard Scaling
- The power wall



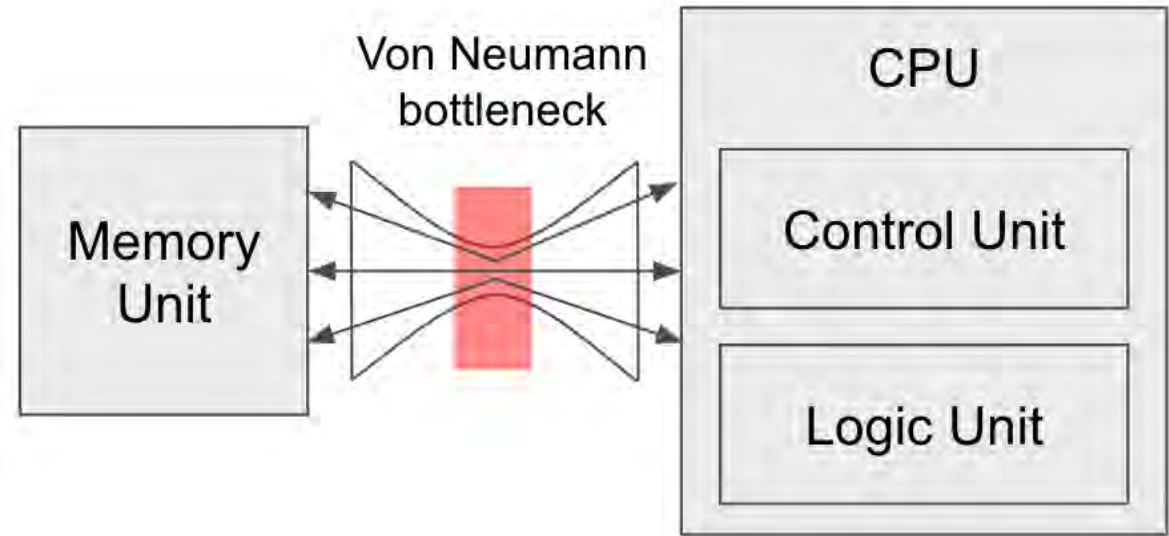
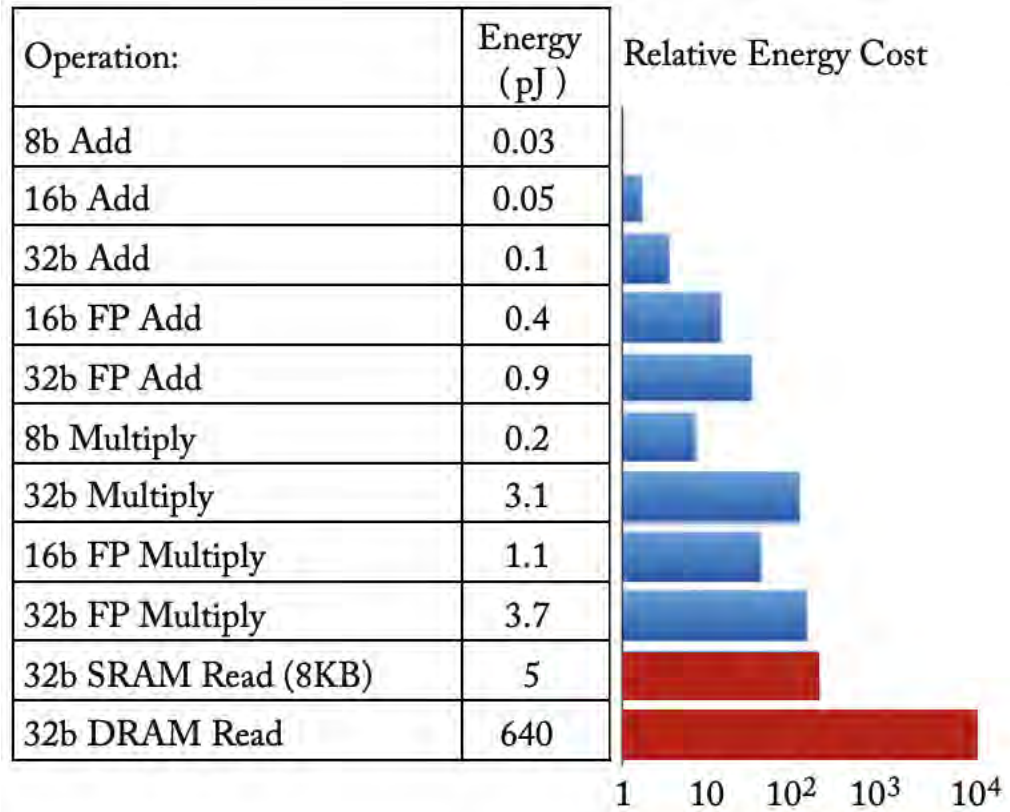
Hennessy & Patterson predict a new golden age is approaching: one which relies on hardware/software co-design and open-source cores and architectures [2]

[fig] Vivienne Sze, 6.6010 Analysis and Design of Digital Integrated Circuits, 2022
[2] J. Hennessy and D. Patterson, "A new golden age for computer architecture," *ACM/IEEE 45th ISCA*, (2018)

Von Neumann Bottleneck



Find plot to demonstrate the interconnect bottleneck –
back throughput and very energy expensive
Energy consumption of data movement



AI applications Demand More Compute



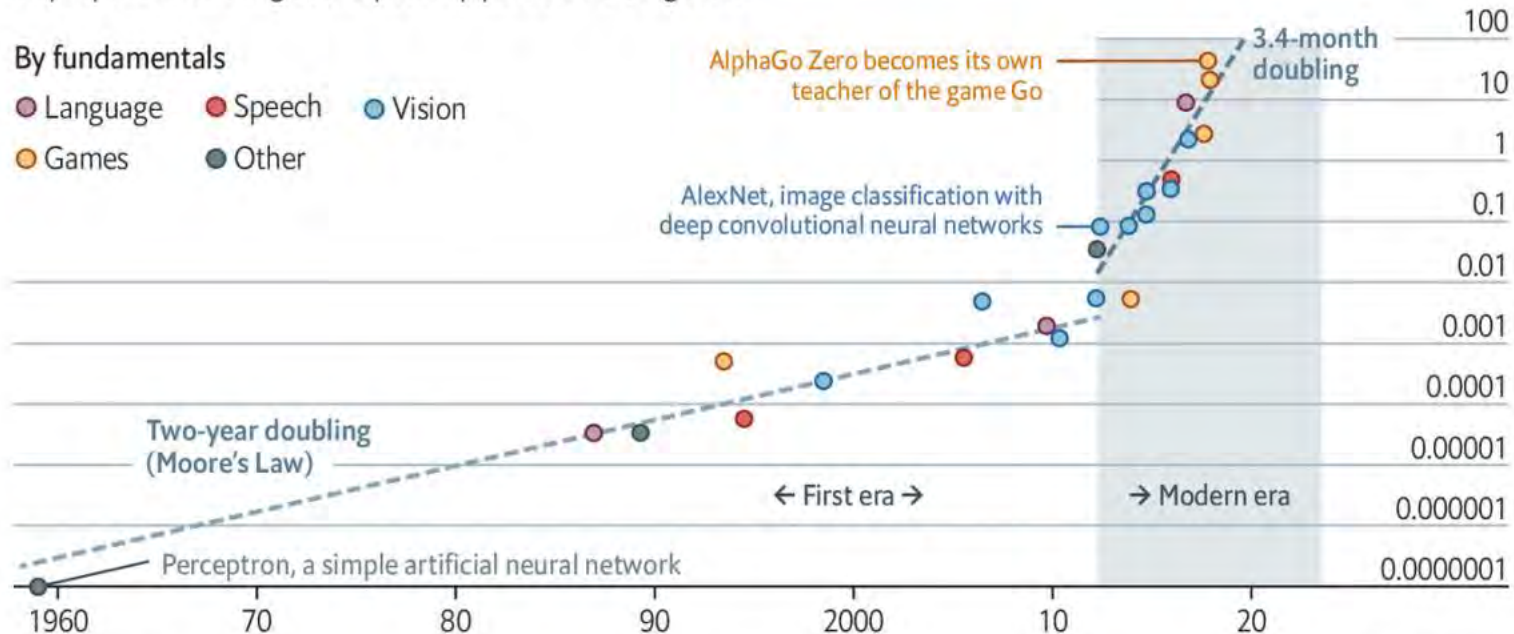
AlexNet to AlphaGo Zero: A 300,000x Increase in Compute

Deep and steep

Computing power used in training AI systems
Days spent calculating at one petaflop per second*, log scale

By fundamentals

- Language
- Speech
- Vision
- Games
- Other



Source: OpenAI

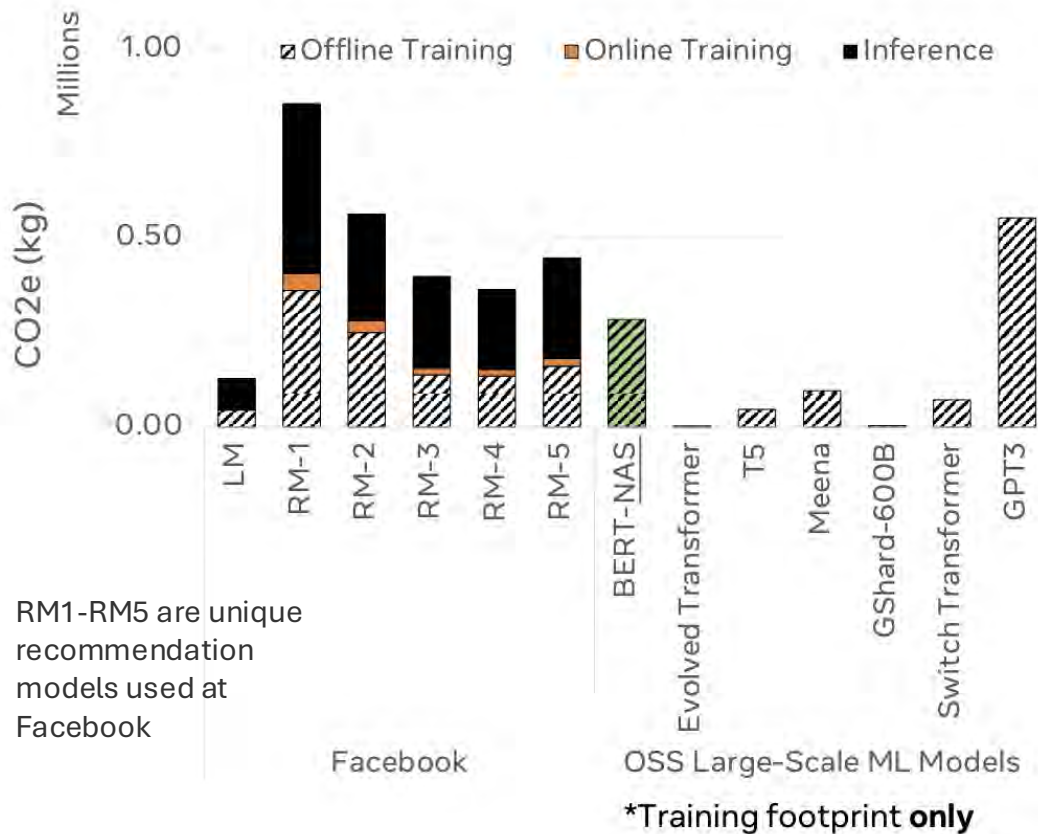
The Economist

*1 petaflop=10¹⁵ calculations

AI Training vs. Inference: Energy Impact



Operational Carbon Footprint of Large-Scale ML Tasks



Facebook AI Compute Energy



Google AI Compute Energy

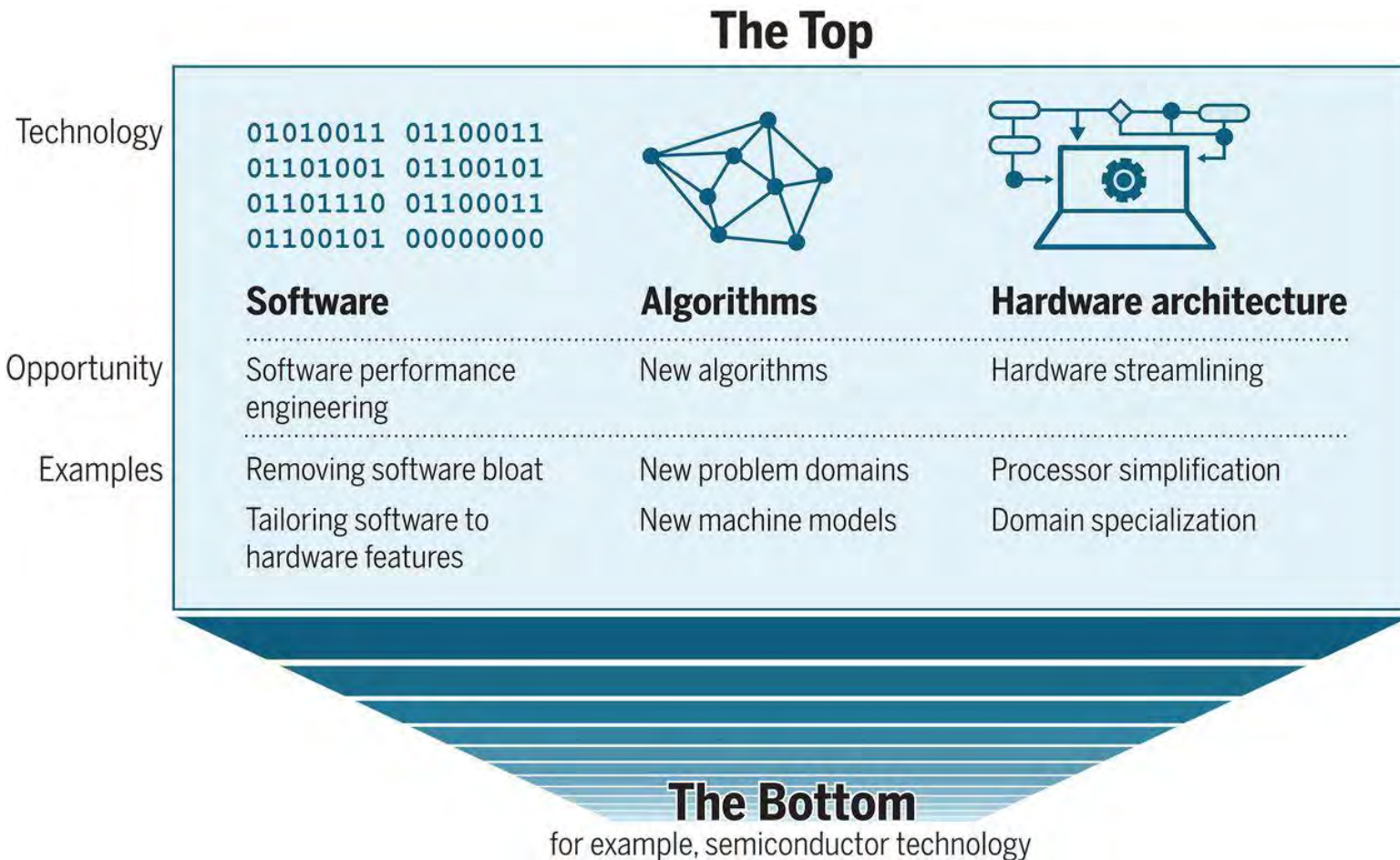


“Across all three years [2019 – 2021], about **three-fifths** of the ML energy use was for **inference**, and **two-fifths** were for **training**.” [1]

[1] D. Patterson et al., "The Carbon Footprint of Machine Learning Training Will Plateau, Then Shrink," in Computer (July 2022)

[2] C.-J. Wu et al., "Sustainable AI: Environmental Implications, Challenges and Opportunities." arXiv, (Jan 2022)

Entering a New Computing Era



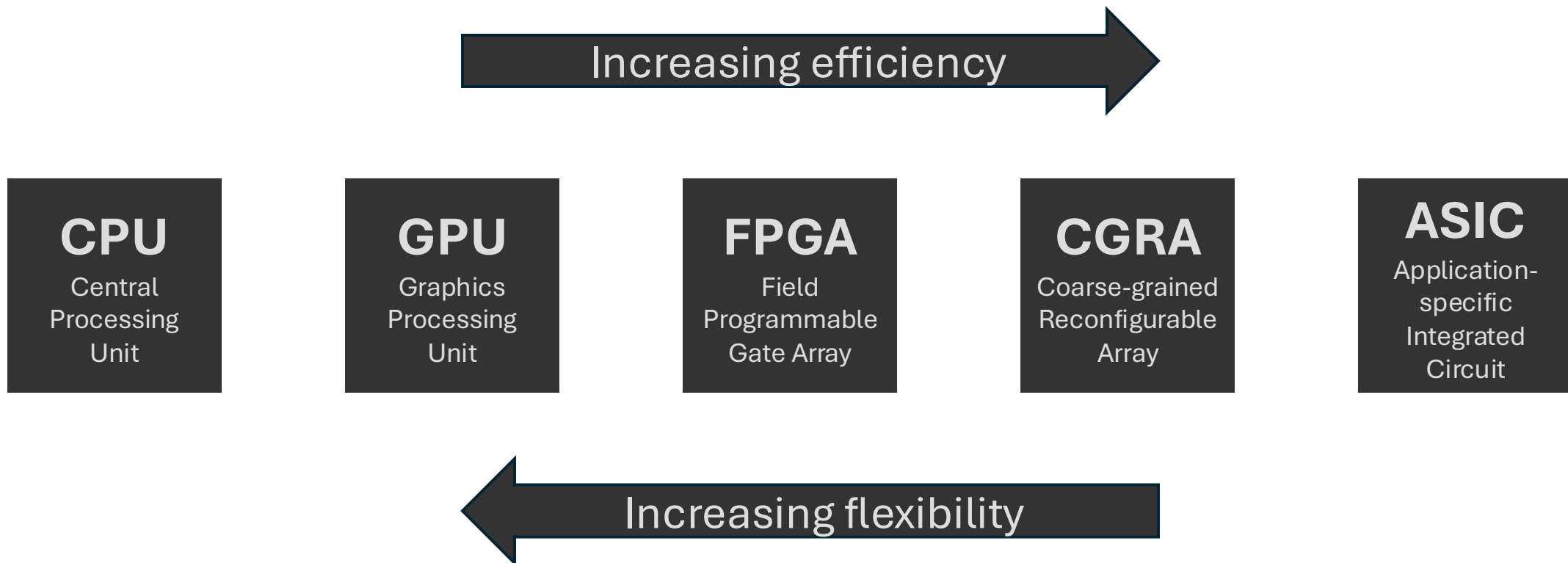
“In the post-Moore era, performance improvements from software, algorithms, and hardware architecture will increasingly require concurrent changes across other levels of the stack”

→ this will be easiest by relying on MODULAR DESIGN across the stack

Computing Architecture Landscape



The most important trade-off in the post-Moore era is flexibility/programmability vs. efficiency (energy, area, and performance)

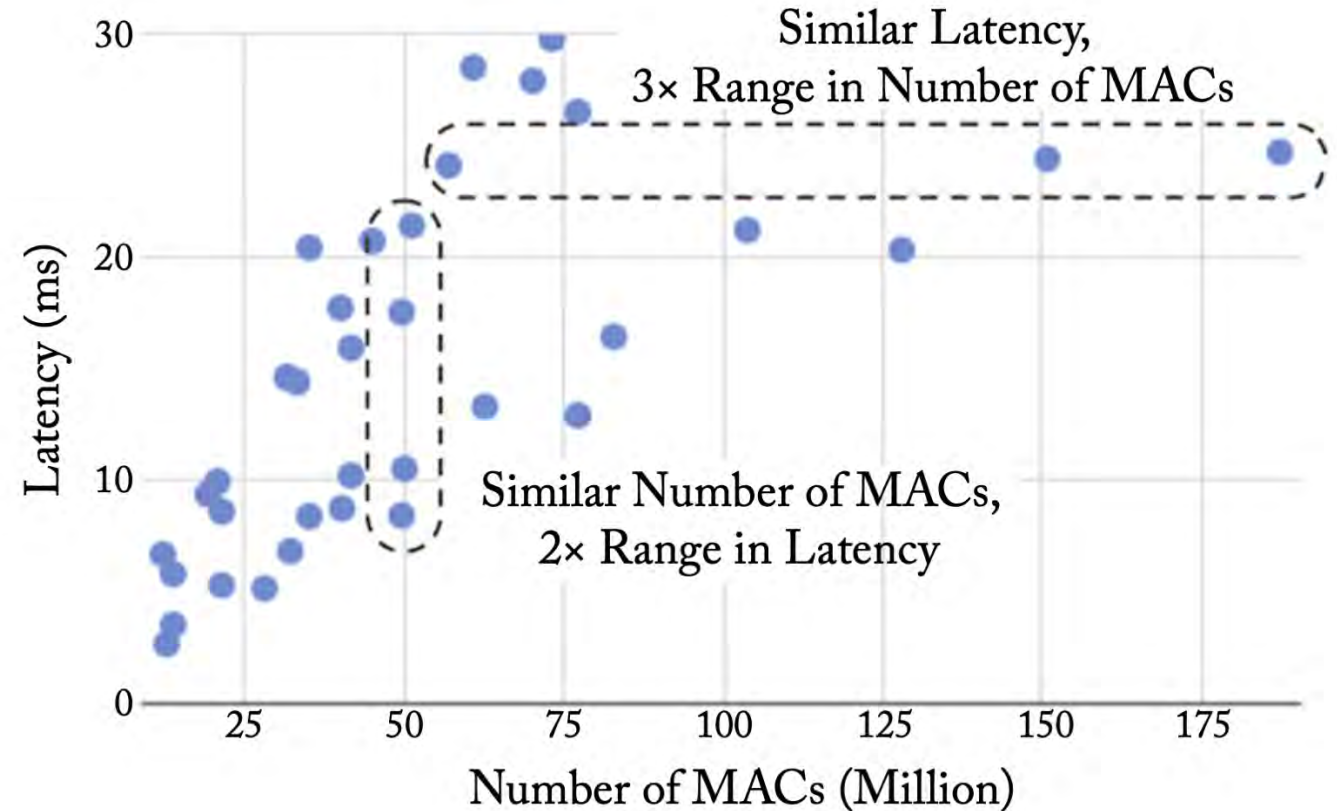


Metrics for Evaluating Computing



- Accuracy
- Throughput and Latency
- Energy and Power
- Cost
- Flexibility
- Scalability

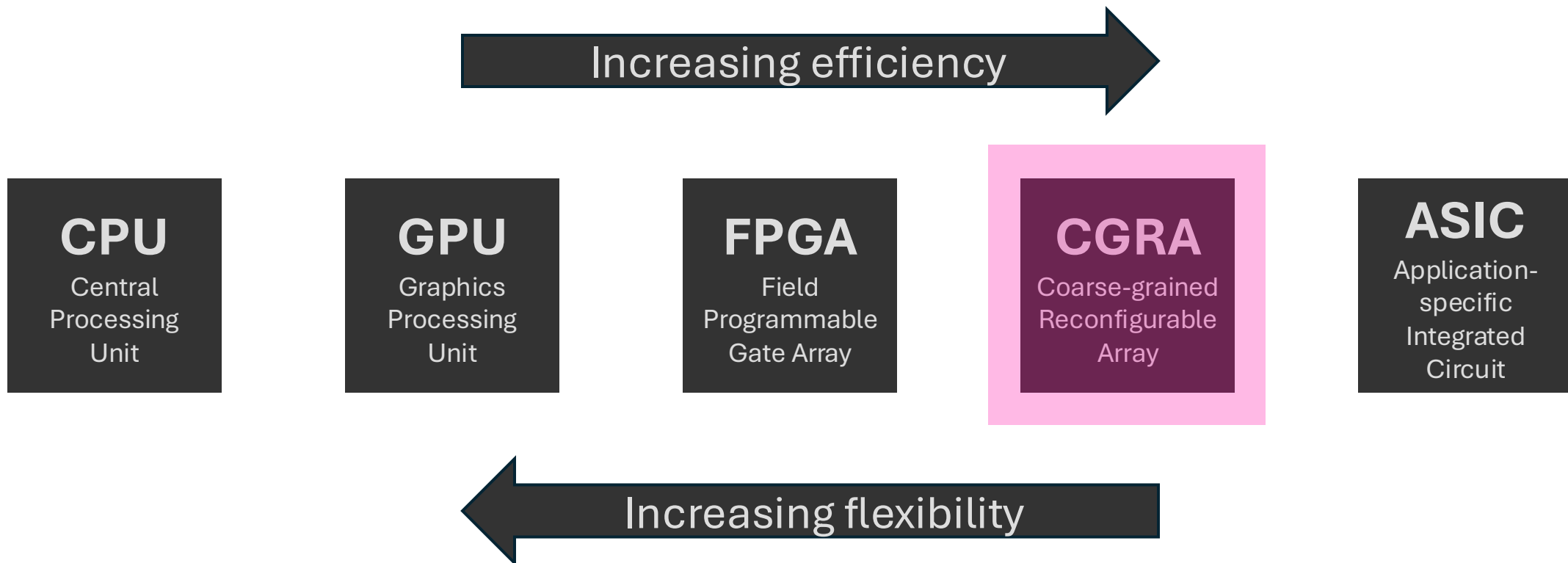
All with interdependent tradeoffs, that can be very application dependent



Coarse-Grain Reconfigurable Architecture



The most important trade-off in the post-Moore era is flexibility/programmability vs. efficiency (energy, area, and performance)



Coarse-Grain Reconfigurable Architectures



“CGRAs are defined as domain-specific flexible hardware, on which the computation is performed both spatially and temporally and the execution is driven by configuration flow or data flow.” [1]

Domain-specific Flexibility:

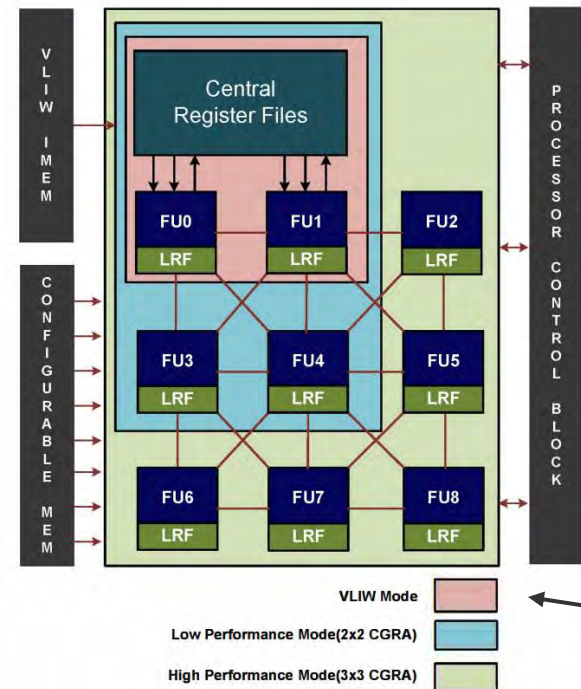
- Some element of post-fabrication flexibility, but it's confined to specific uses or applications
- Not as general as FPGA

Both Spatial and Temporal Computation:

- Computational modules are tiles to form spatial architecture that can take advantage of parallel computing resources and dataflow communication
- Unlike FPGAs, The modules still have control logic and local register/scratchpad cache allowing for time multiplexing

Configuration- or Data-driven Execution:

- At the configuration or data level, operations are defined by propagation, as opposed to conventional CPU pipelining
- Configuration-driven CGRAs can exploit interconnects for efficient execution order
- Data-driven CGRAs are full dataflow machines, i.e. execution is only set by producer-consumer relationship



Samsung Reconfigurable Processor (SRP) [2] can select how many processing elements are used

[1] L. Liu, et. al., “A Survey of Coarse-Grained Reconfigurable Architecture and Design: Taxonomy, Challenges, and Applications”, *ACM Computing Surveys*, (Nov 2020)

[2] C. Kim, et. al., “ULP-SRP: Ultra low power Samsung Reconfigurable Processor for biomedical applications,” in *2012 Int’l Conf. FPT*, Seoul, Korea (South): IEEE, (Dec. 2012)

Coarse-Grain Reconfigurable Architectures



Abstracts away all the underlying computing system to describe algorithms and data structures



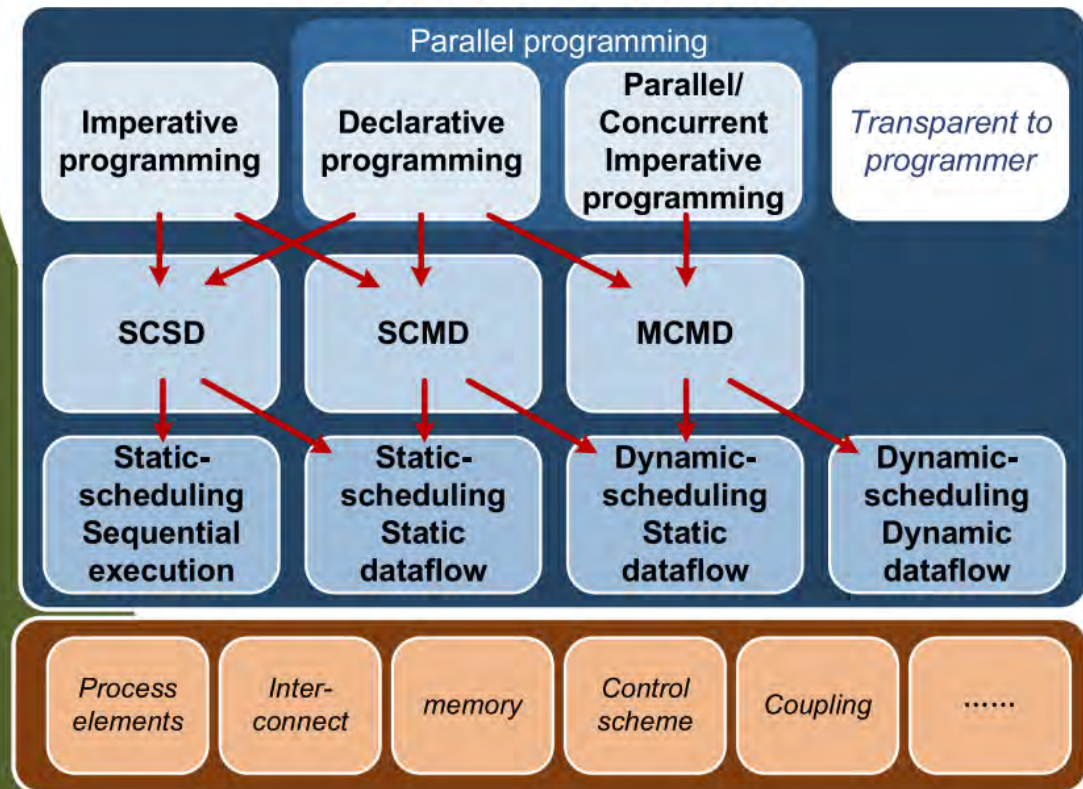
Represents the computational semantics that produces solutions for executing applications described by the programming model and reflects the physical characteristics of the system



The abstract representation of the micro-architecture handling operation scheduling scheme



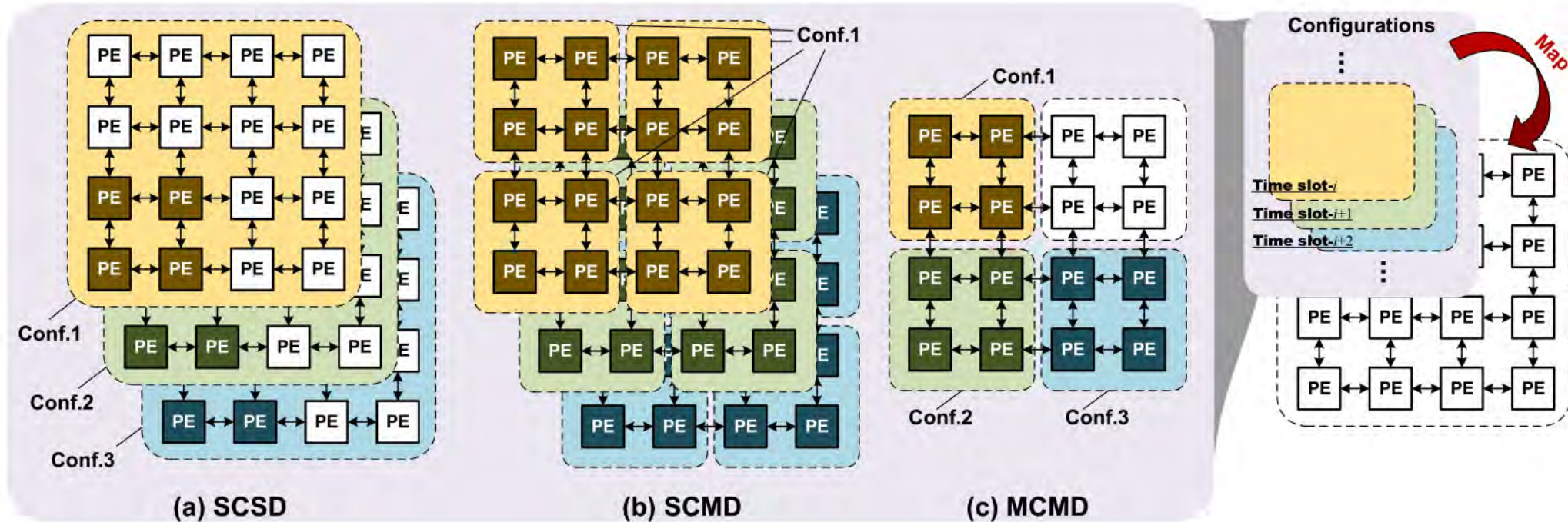
CGRA Classification



Coarse-Grain Reconfigurable Architectures



All CGRAs are MIMD (multiple instruction, multiple data) according to Flynn's taxonomy, so we can further categorize according to configuration



Single configuration, single data (SCSD)

Strength: instruction level parallelism, simple implementation

Single configuration, multiple data (SCMD)

Strength: data-level parallelism, like a spatially tiled SIMD

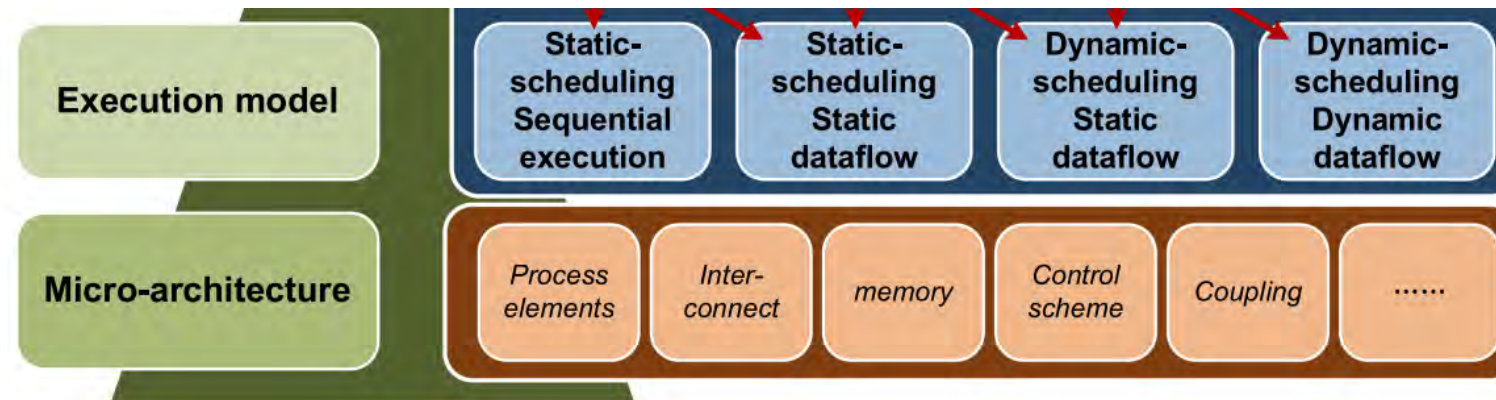
Multiple configuration, multiple data (MCMD)

Strength: thread-level parallelism, simultaneous multithreading and temporal multithreading

Coarse-Grain Reconfigurable Architectures



Execution model is like the lower-level instruction set determining how and when operations are performed



Scheduling

Refers to mechanism for fetching configurations and mapping them to hardware memory

- Static: configurations are mapped by the compiler and not updated at runtime. Lower hardware overhead at expense of performance
- Dynamic: configuration mapping is done on the fly determined by resource allocation. Higher performance at the expense of circuit overhead

Execution

Refers to the mechanism for executing computation within a single configuration

- Sequential: operations are executed in the order that the compiler defines before runtime
- Dataflow: operations are executed based on operand availability
 - Static: operand arrival is signaled by tokens, only once all are present is operation executed
 - Dynamic: operand arrival is signaled by tokens and tagged, only once all with matching tags are present is the operation executed (to allow for multiple instances of the same routine)

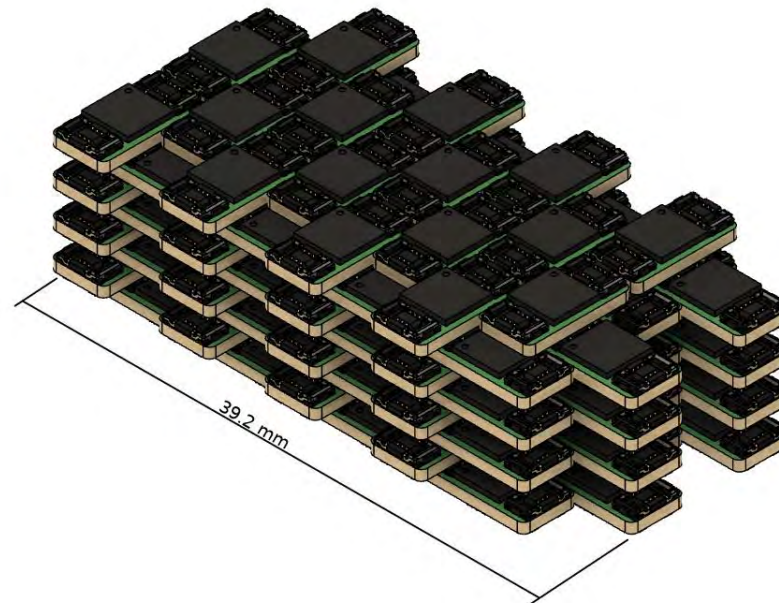
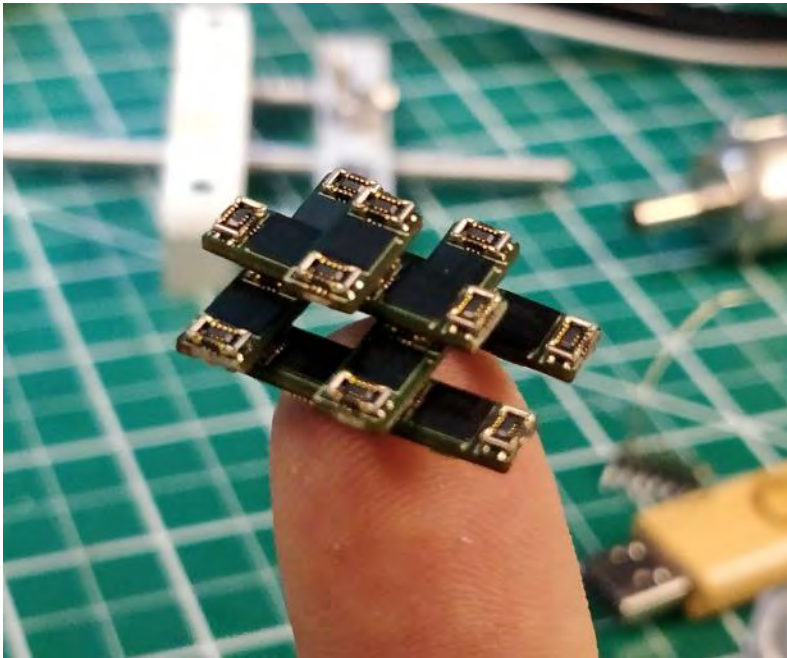
Coarse-Grain Reconfigurable Architectures



DICE: Discrete Integrated Circuit Elements

computation: MCMD

execution: dynamic scheduling, dynamic dataflow



Coarse-Grain Reconfigurable Architectures



CGRAs are not saved from the memory wall problem!!

Depending on the shared memory allocation, they could be more sensitive to the memory wall problem than vector machines (full dataflow architectures) because multiple PEs running multiple threads could run into scheduling conflicts accessing shared memory, and therefore increase latency



State of the art High Bandwidth Memory solution → HBM3E from Micron capable of 1.2 TB/s with 24GB of capacity [1]

To be integrated into upcoming Nvidia H200 GPU with 141 GB at 4.8 TB/s

[vid] Micron HBM3E, <https://www.micron.com/products/memory/hbm/hbm3e>

[1] “Micron Commences Volume Production of Industry-Leading HBM3E Solution to Accelerate the Growth of AI | Micron Technology” Press release (Feb 2024)

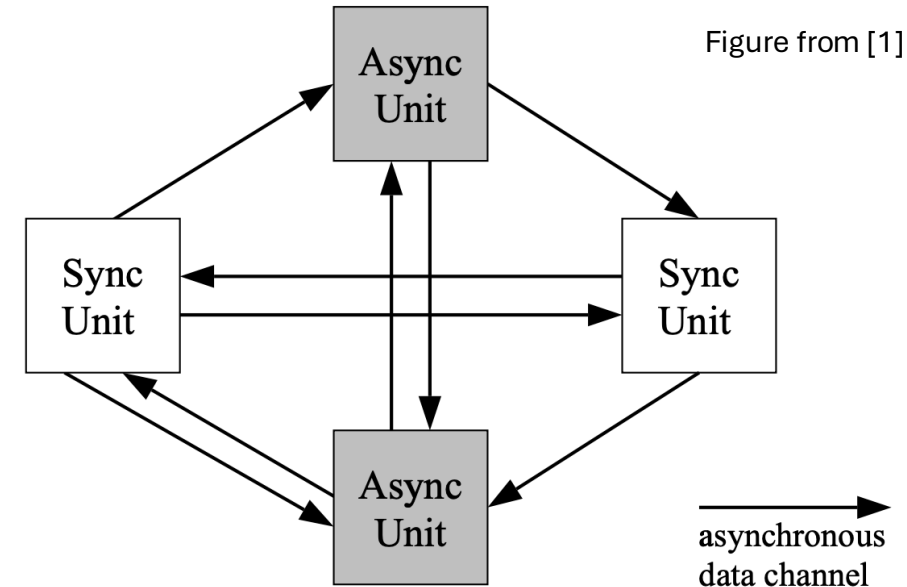
Globally Asynchronous, Locally Synchronous



GALS: An asynchronous method for sending data signals across clock domains

Metastability: THE major issue in designing GALS systems

- At any boundary between independent clock domains the system can enter a metastable point which requires significant power, area, and timing costs to overcome
- Main strategies for reliable data transfer:
 - Pausible-clock generators
 - FIFO buffers
 - Boundary synchronization

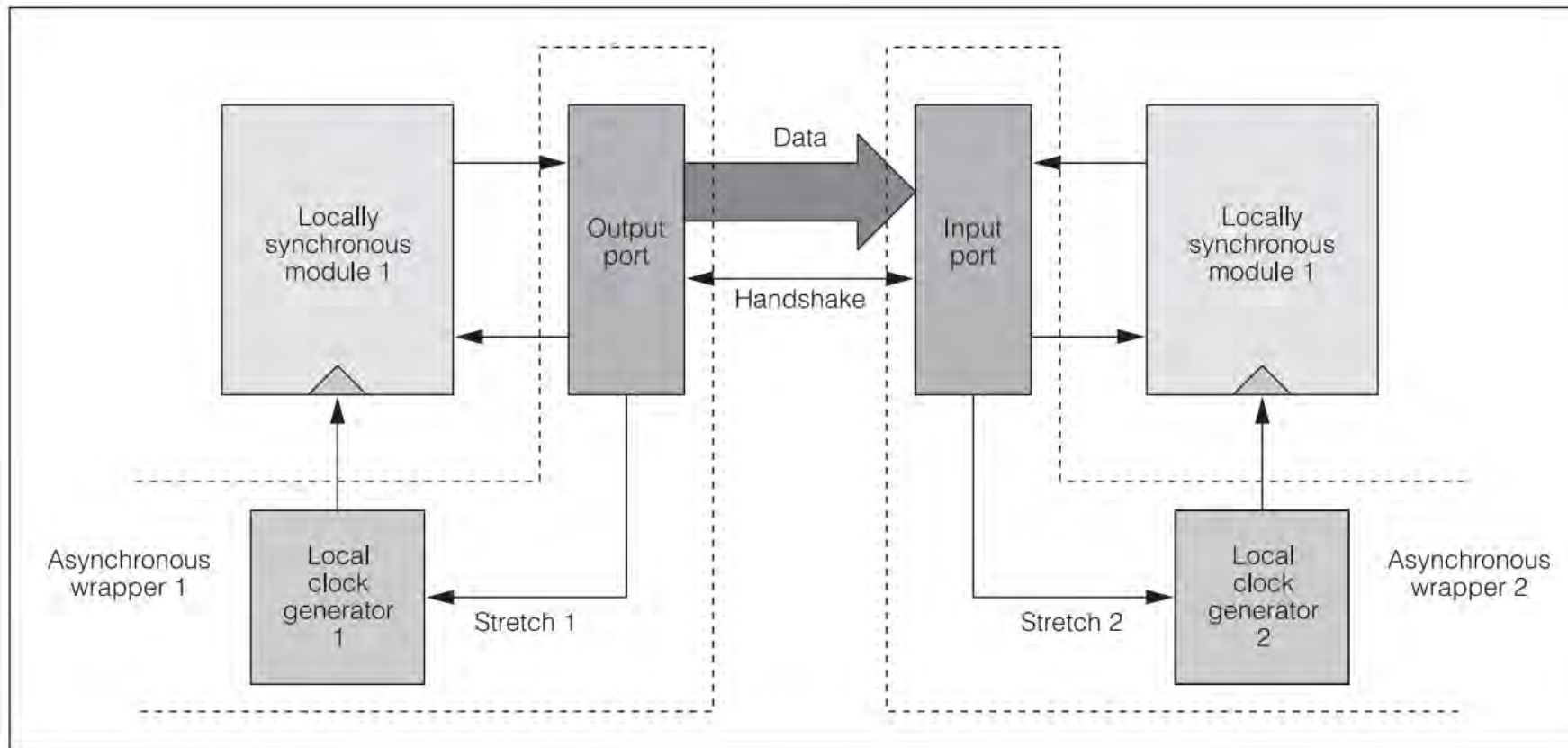


- Locally synchronous operations are required at minimum at combinational logic level
- Asynchronous buffers introduce some amount of overhead so the tradeoff becomes area and energy versus flexibility

Globally Asynchronous, Locally Synchronous



Pausable clocking scheme:



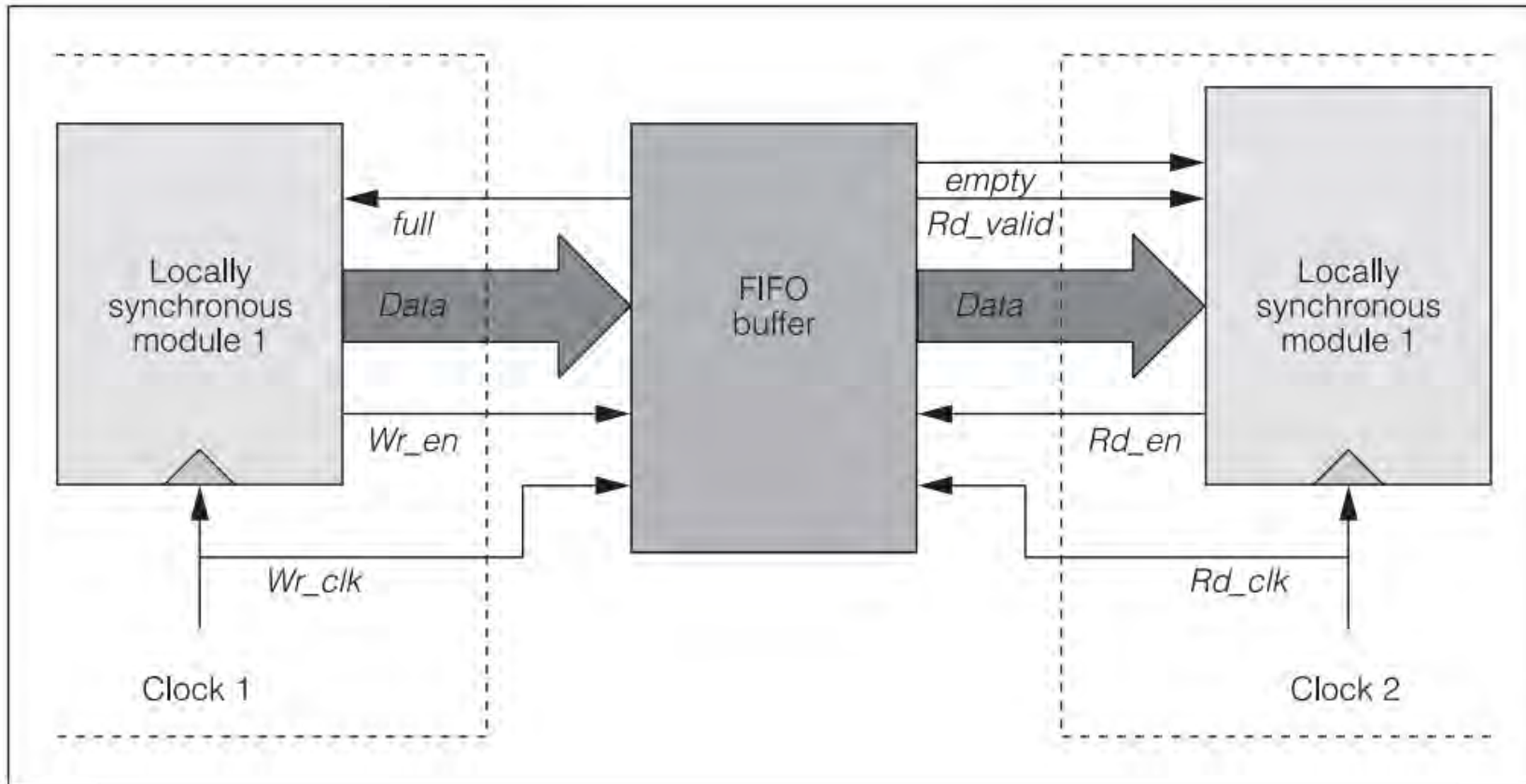
Local clock generators within the asynchronous wrappers drive the locally synchronous modules so that data transmission/receiver signals are guaranteed to be OFF when data is transferred across clock domains

Perhaps similar to a module-scale version of the Variable Activation QFP clocking scheme I've discussed in the past

Globally Asynchronous, Locally Synchronous



FIFO buffer scheme:

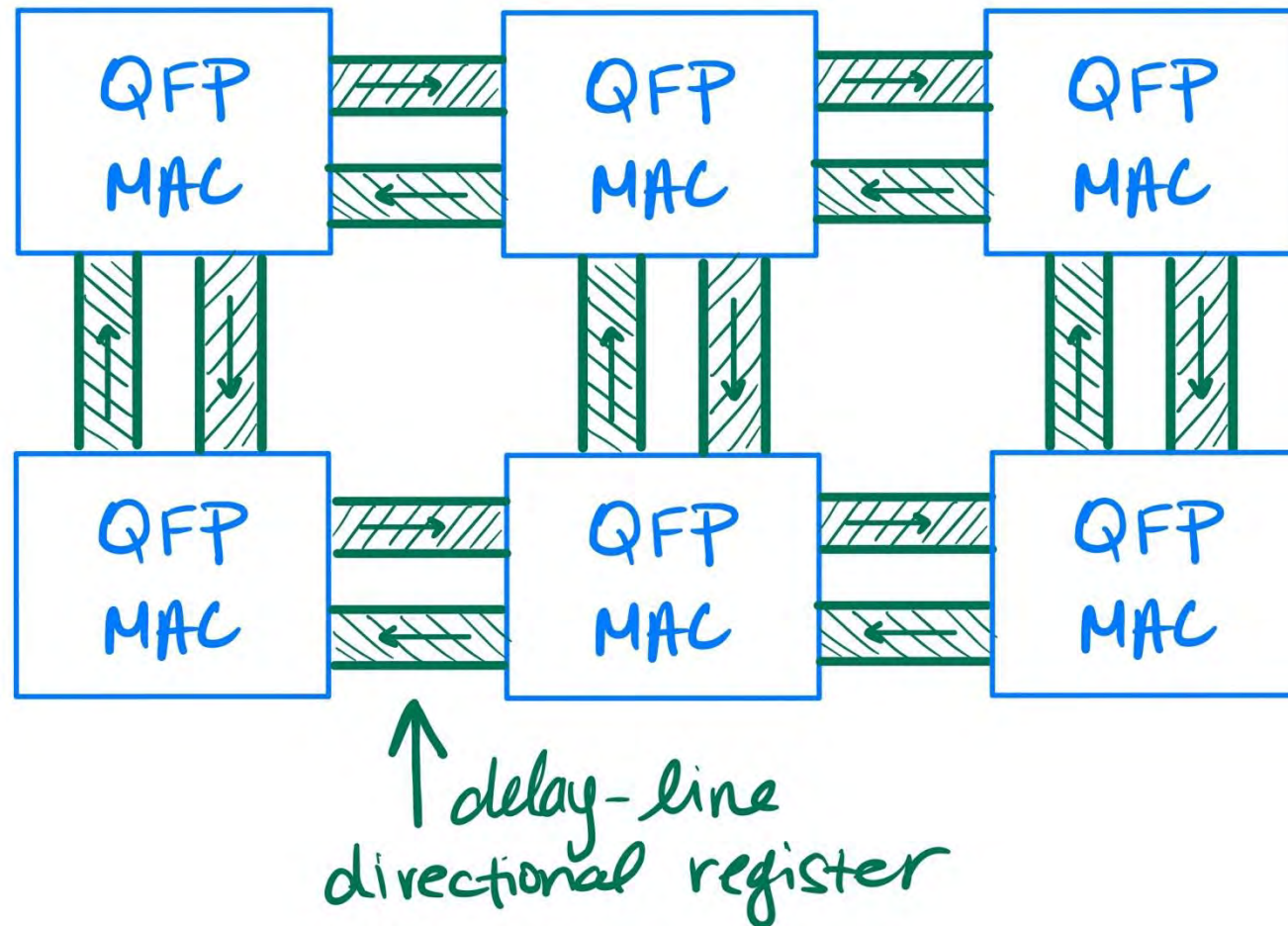


- FIFO buffers are added between adjacent synchronous modules, moving data in one direction. Additional buffers can be added to allow multi-directional dataflow.
- For large SoC applications, this can be best because it hides long interconnect delays.
- Most common implementation in GALS systems

Globally Asynchronous, Locally Synchronous



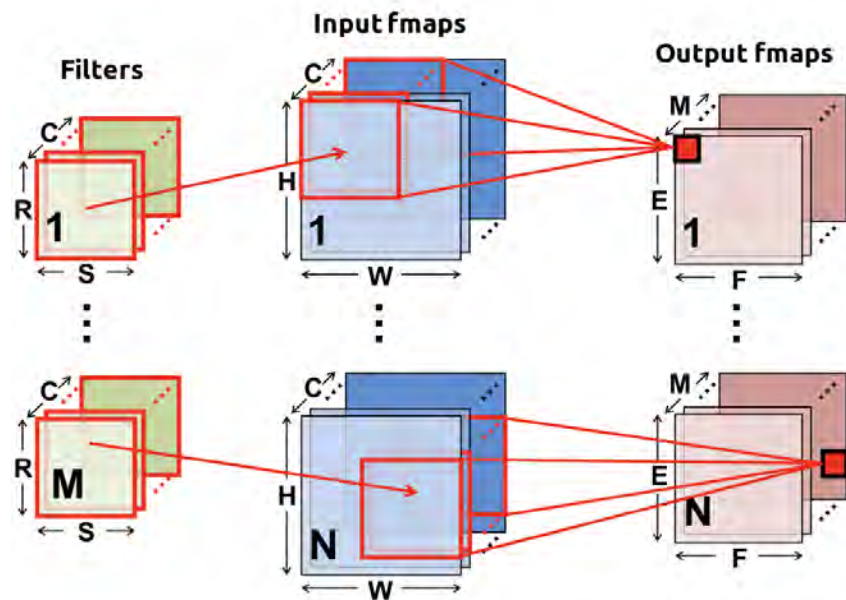
Delay Line Memory behaving as FIFO buffers



DNN Accelerator Design

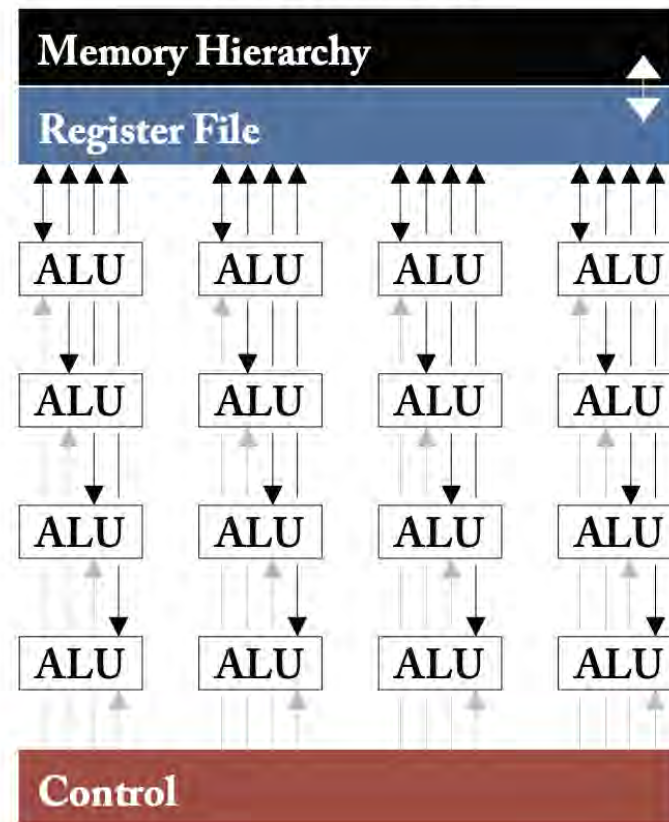


Deep Neural Networks (DNN) can exploit highly parallel computation

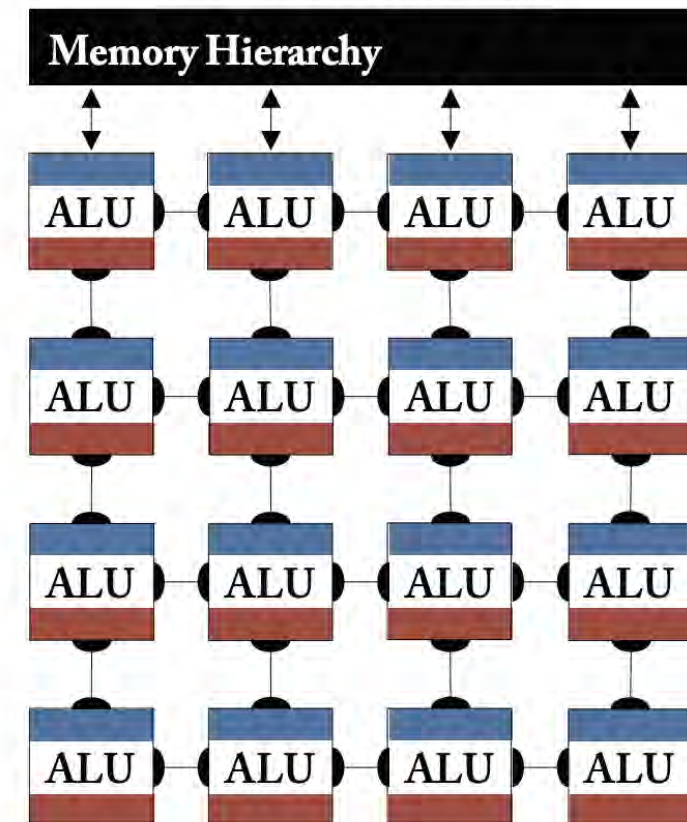


Convolutional Neural Network (CNN) layer

Temporal Architecture (SIMD/SIMT)



Spatial Architecture (Dataflow Processing)



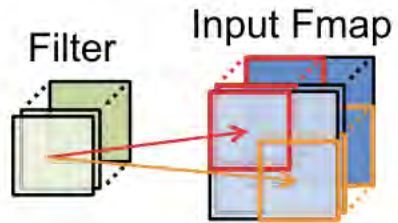
DNN Accelerator Design



Hardware accelerators can exploit data reuse to minimize data movement

Convolutional Reuse

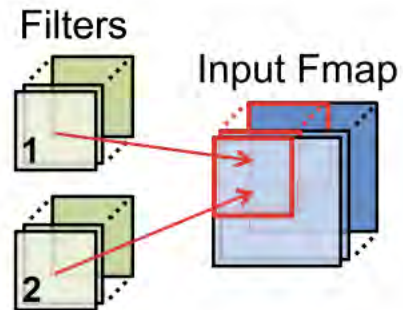
CONV layers only
(sliding window)



Reuse: Activations
Filter weights

Fmap Reuse

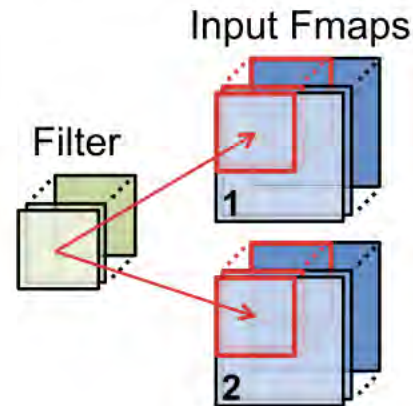
CONV and FC layers



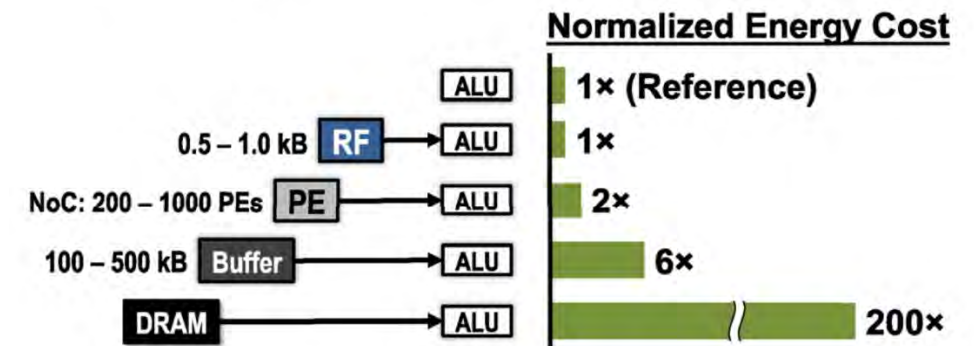
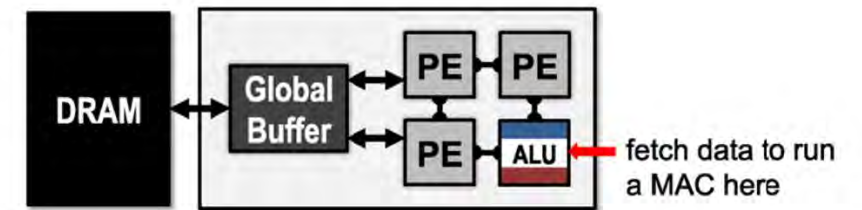
Reuse: Activations

Filter Reuse

CONV and FC layers
(batch size > 1)



Reuse: Filter weights

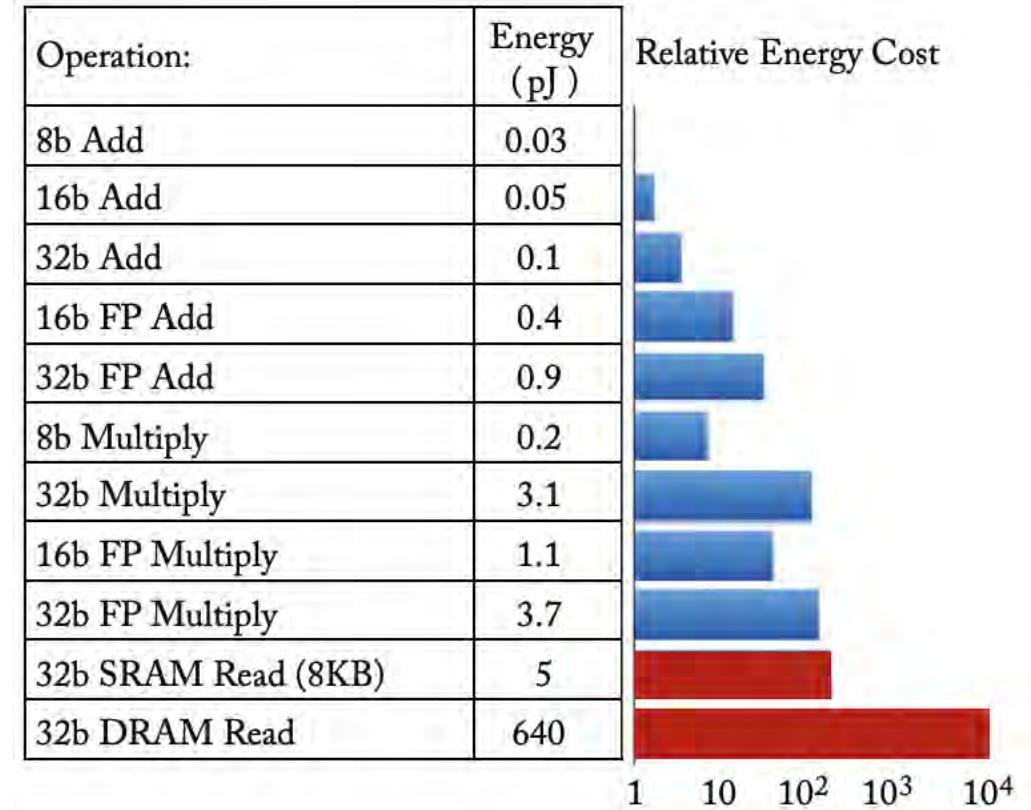
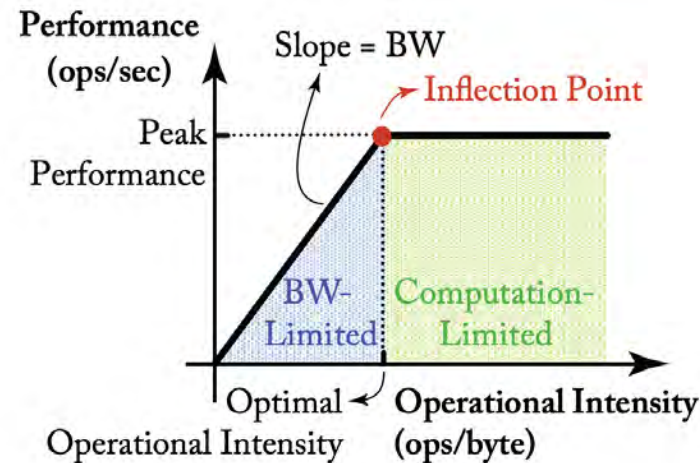


DNN Accelerator Design

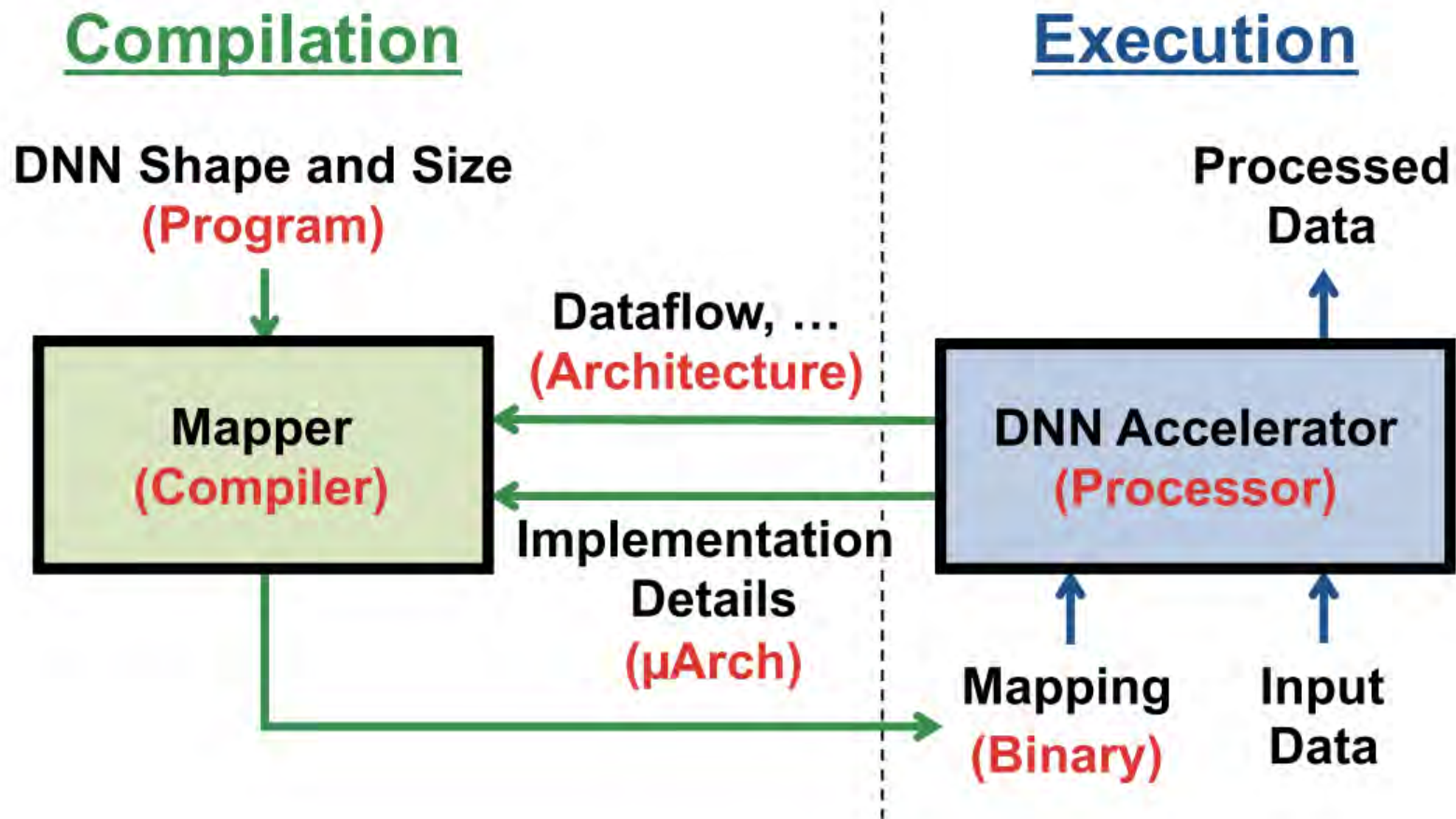


Can improve energy performance by exploiting sparsity:

$$\frac{\text{operations}}{\text{joule}} = \frac{\text{effectual operations} + \text{unexploited ineffectual operations}}{\text{joule}} \times \frac{\text{effectual operations}}{\text{effectual operations} + \text{unexploited ineffectual operations}} \times \frac{1}{\frac{\text{effectual operations}}{\text{operations}}}$$

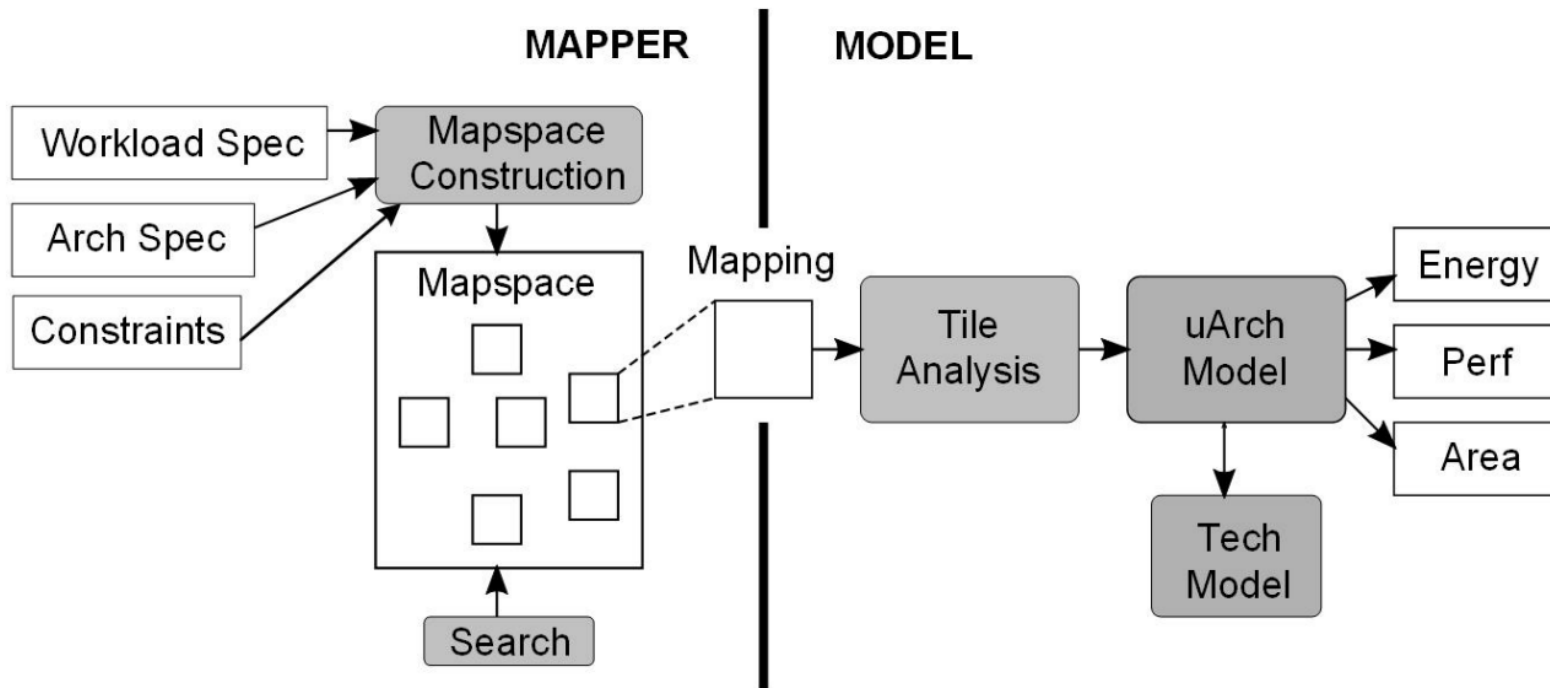


Accelerator Operation Workflow



Accelerator workflow (black text) in comparison to typical CPU workflow (red text)

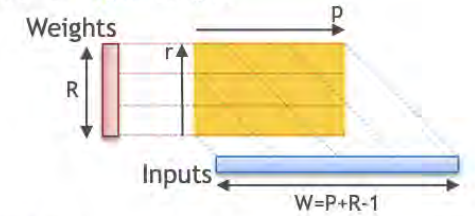
Timeloop: Architecture Modeling Tool



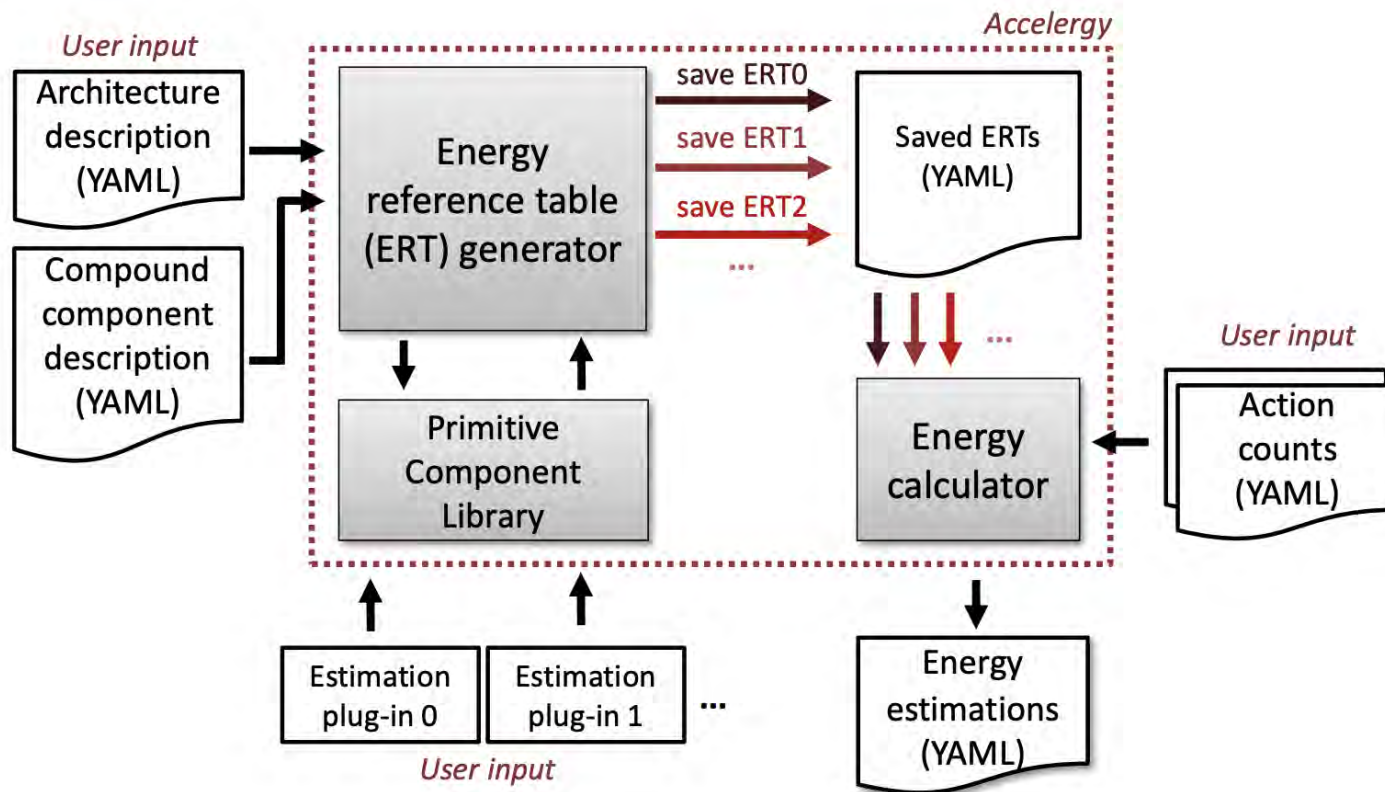
```

1 // === 1D Convolution Workload ===
2 for r=[0:R):
3   for p=[0:P):
4     Output[p] += Weight[r] * Input[r+p];
5
6 // === Mapping ===
7 // DRAM
8 for r3=[0:R3):
9   for p3=[0:P3):
10    // GBuf
11   for r2=[0:R2):
12     for p2=[0:P2):
13       // Spatial: GBuf->RFile
14       parallel_for r1=[0:R1):
15         parallel_for p1=[0:P1):
16           // RFile
17           for r0=[0:R0):
18             for p0=[0:P0):
19               p = p3+P2+P1*p0 + p2+P1*p0 + p1*p0 + p0;
20               r = r3+R2+R1*r0 + r2+R1*r0 + r1*r0 + r0;
21             Output[p] += Weight[r] * Input[r+p];

```



Accelergy: Energy Estimator for Timeloop



Example 1: a counter primitive component class

```

1 name: counter #class name
2 attributes: #default attributes
3   technology: 65nm
4   datawidth: 16
5 actions: #list of actions
6   - name: count
7   - name: idle
    
```

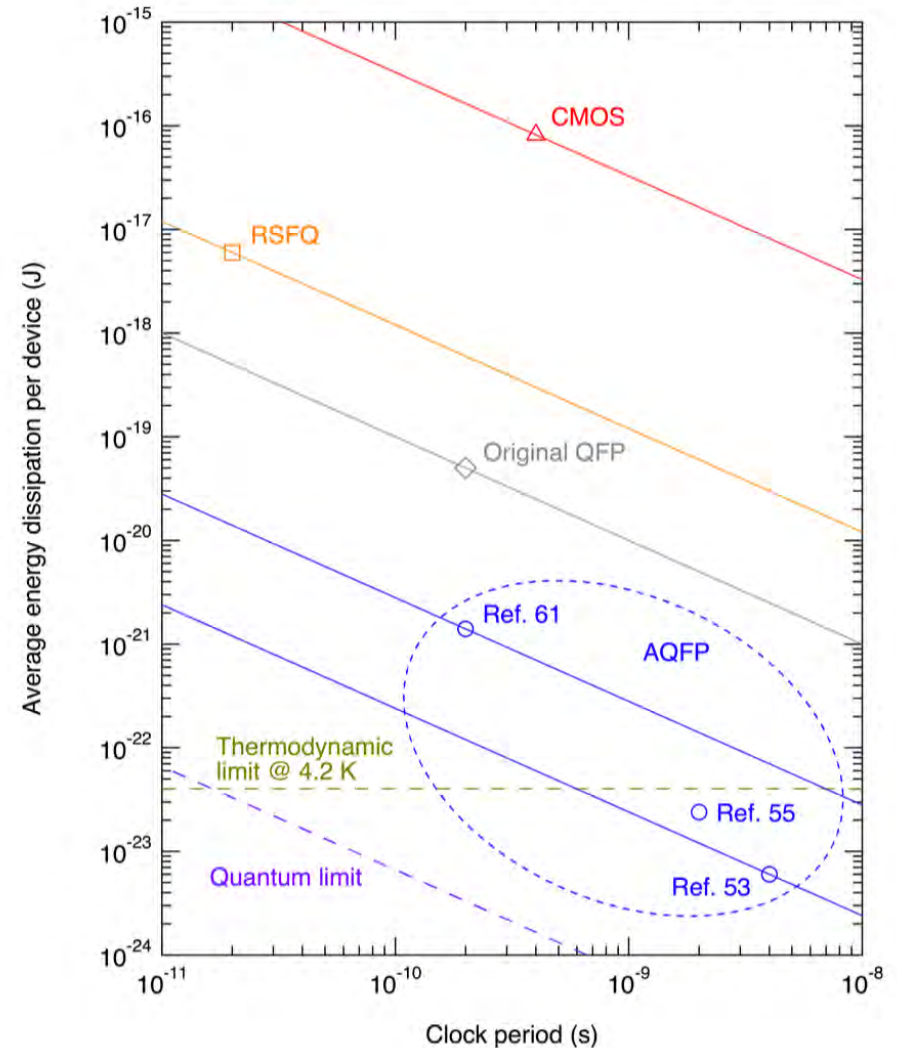
Table 1: Selected components, hardware attributes, and action types in DNN primitive component library

Primitive Components	Hardware Attributes	Action Types
SRAM	width depth # of read ports # of write ports # of banks	random_read random_write repeated_read repeated_data_write bypassed_read
MAC	bitwidth # of pipeline stages	random_MAC constant_MAC gated_MAC zero_gated_MAC
counter	count limit	count
router	FIFO width crossbar input ports crossbar output ports	random_transfer repeated_transfer gated_transfer
wire	data width wire length	random_transfer repeated_transfer

Extending the Tools for AQFP

Adiabatic Quantum Flux Parametron

- Ultra-low switching energy, $\gg I_c \Phi_0$ because of adiabatic operation
 - **1.4zJ** (10^{-21} J) experimentally recorded energy dissipation for a single QFP switch [1]
- Clock speed comparable to CMOS at **5-10 GHz**
- High gain device
 - **50x – 100x gain** from a few uAs of current
- Decently robust to issues of flux trapping (when compared to SFQ)



[1] N. Takeuchi et. al., Appl. Phys. Lett., vol. 144, no. 4, p. 042602 (2019)

Extending the Tools for AQFP



camronblackburn / accelergy-library-plugin-in

Code Pull requests Actions Projects Security Insights Settings

Files

sce-tables + 🔍

Go to file t

- prime
- qfp
 - SRAM_reg_16x512.csv
 - _citation.bib
 - intmac.csv
 - reg.csv
 - regfile.csv
- raella
- timely

accelergy-library-plugin-in / library / qfp / intmac.csv

Camron update QFP numbers

Preview Code Blame 3 lines (3 loc) · 181 Bytes Code 55% faster with GitHub Copilot

Search this file

	technology	global_cycle_seconds	latency (ps)	datawidth	energy	area	action
1	qfp	2e-10	3840	16	0.000013601021	30000	read write update
2	qfp	2e-10	0	16	0	30000	leak

Single PE example: CMOS vs AQFP



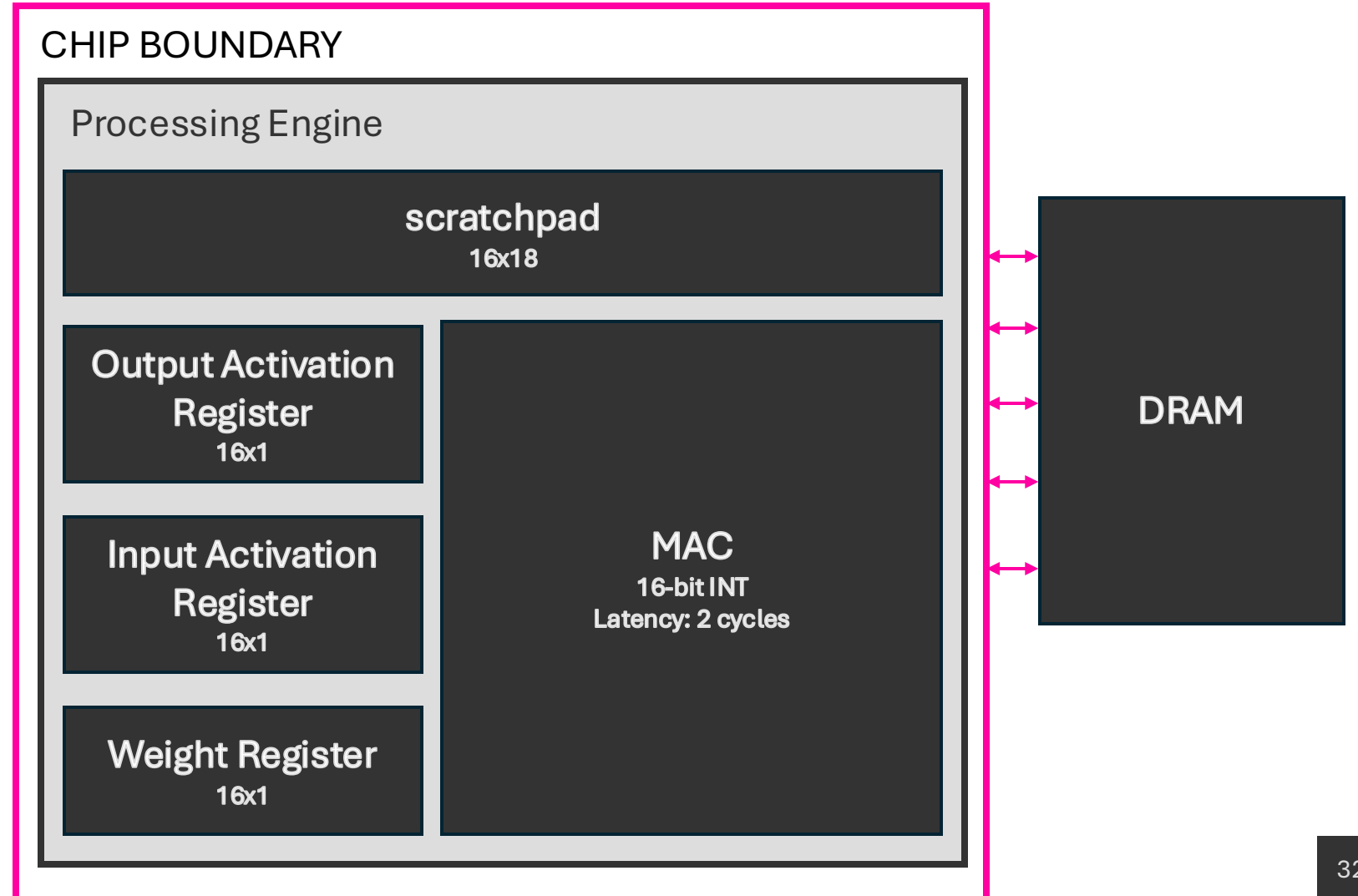
Example single PE architecture run for 45nm CMOS default tool values and QFP projected performance

```
// Single PE loop nest

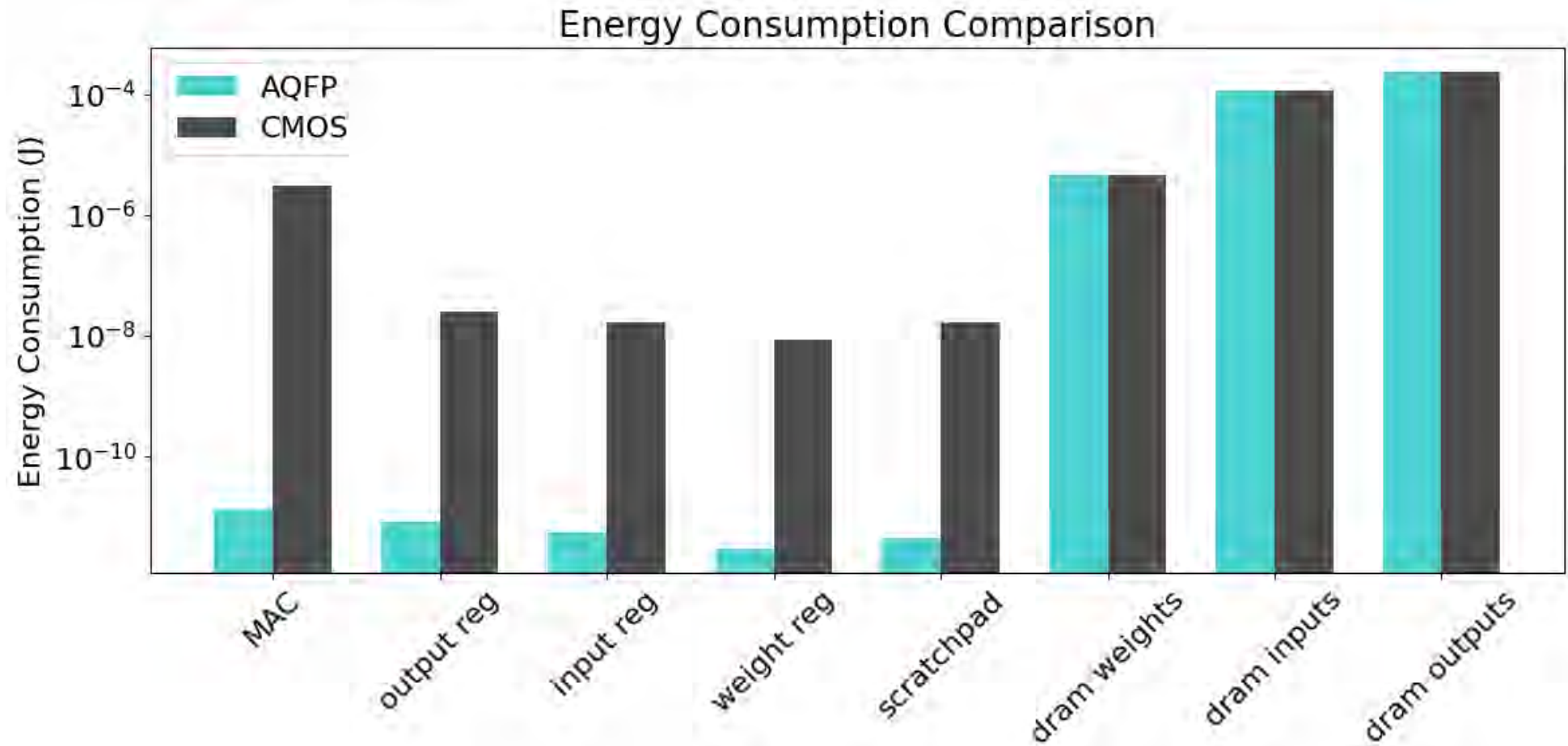
int i[N][C][W][H]; # Input activations
int w[M][C][R][S]; # Filter Weights
int o[N][M][P][Q]; # Output activations

// Level 1 - DRAM temporal
for n1 = [0, N/N0) {
  for m1 = [0, M/M0) {
    for c1 = [0, C/C0) {
      // Level 0 - PE temporal
      for r0 = [0, R) {
        for s0 = [0, S){
          for m0 = [0, M0) {
            for c0 = [0, C0) {
              for n0 = [0, N0) {
                for p0 = [0, P) {
                  for q0 = [0, Q) {
                    n = n1*N0 + n0
                    m = m1*M0 + m0
                    c = c1*C0 + c0
                    r = r0
                    s = s0
                    p = p0
                    q = q0

                    o[n][m][p][q] += i[n][c][p+r][q+s]
                                     * w[m][c][r][s]
                  }
                }
              }
            }
          }
        }
      }
    }
  }
}
```



Single PE example: CMOS vs AQFP



*same mapping for AQFP and CMOS. And no change in DRAM

Next steps for AQFP Architecture Modeling



- Model different types of memory
 - How to account for interconnect length in memory modeling?
 - Compare the tradeoff of different types of superconducting memory
- More accurate primitive models
 - Extend into floating point operations
- Include area estimates
- Explore mapping optimizations on QFP logic versus CMOS
 - Requires capturing the unique tradeoffs in superconductivity vs semiconductor IC



Superconducting Electronics Design



CONTENTS

- Superconducting digital logic timeline
- Review of Superconductivity Basics
 - Macroscopic Quantum Model
 - Flux Quantization
 - Josephson Junctions
- Adiabatic Quantum Flux Parametron
 - AQFP analysis: Node Method
 - AQFP Device Characteristics
 - Energy Dissipation
 - AQFP analysis: Circuit Quantization

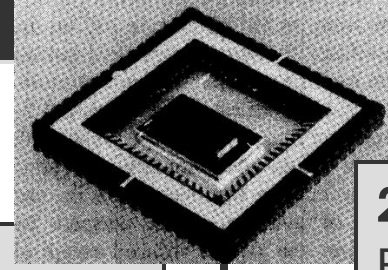
Superconducting Digital Logic

1956 Dudley Buck invents cryotron switching device [1]

1960 Parametron-based tunnel diode pair logic (QFP inspiration) [2]

1970s IBM “Josephson Computer” with voltage state logic [3]

1986 DC Flux parametron, renamed to QFP [5]



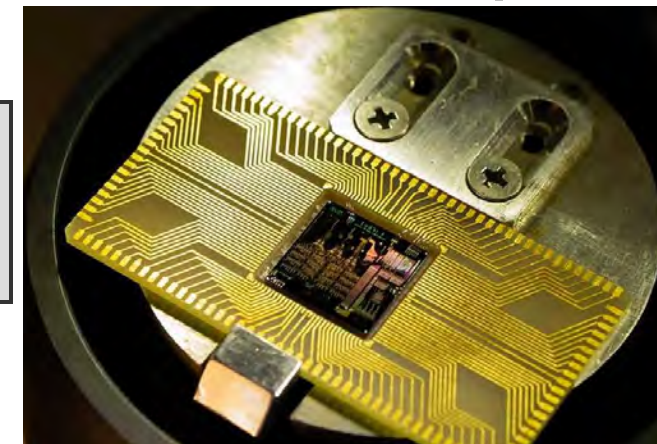
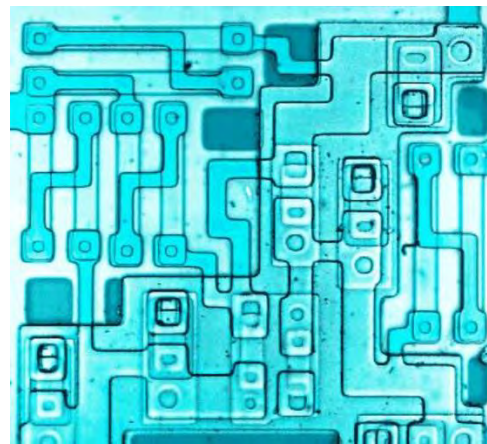
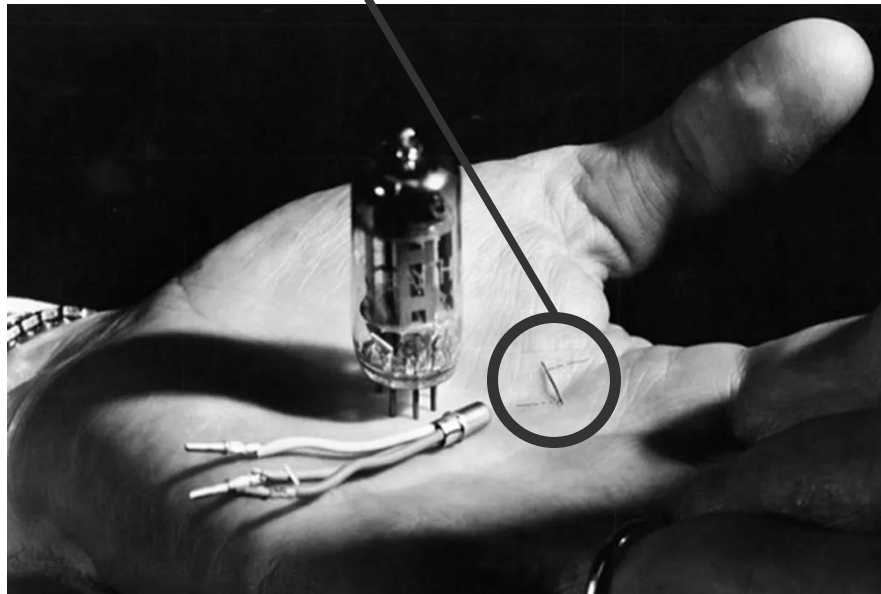
2010s energy efficient RSFQ modifications are explored – ERSFQ, eeSFQ, DSFQ, ...

2011 Adiabatic operation of QFP is revived [7]

1977 Likharev invents parametric quantron (PQ) logic (rf-SQUID) [4]

1991 RSFQ take off for ultrafast operating speed [6]

2020 MANA, first adiabatic superconducting microprocessor [8]

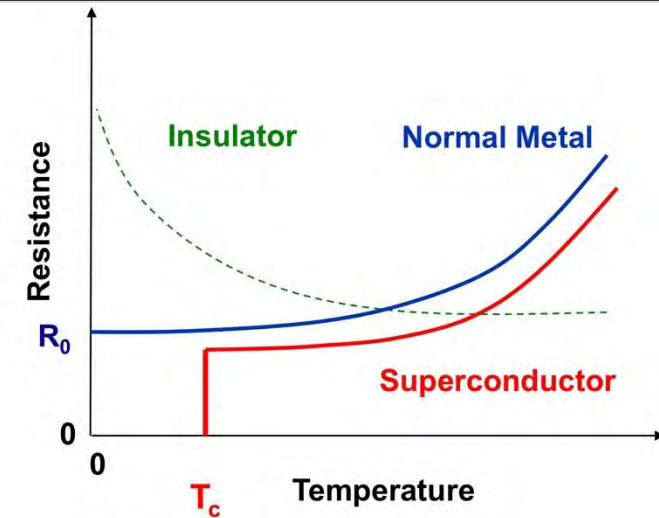


Superconductivity Review

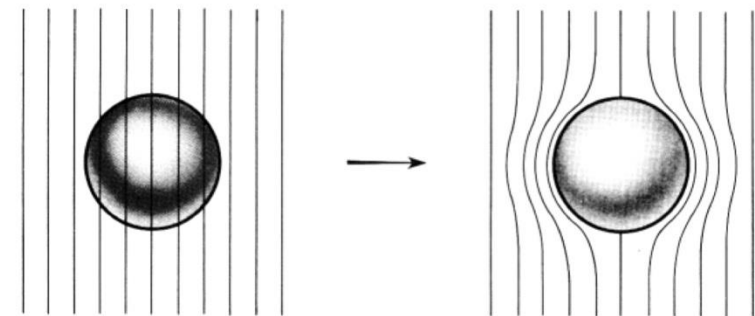
Requirements for a superconductor:

- (1) ZERO electrical resistance below its transition temperature, T_c
 - If injected with DC current, a superconducting loop will have a persistent electric current *forever* → there is no power loss

- (2) Perfect diamagnetism
 - The superconductor expels all magnetic fields (Meissner Effect)
 - More than simple a “perfect conductor” which would preserve trapped fields with screening currents



Meissner Effect

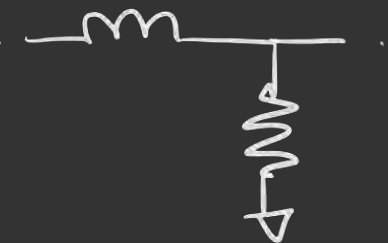


Superconductor Constitutive Laws

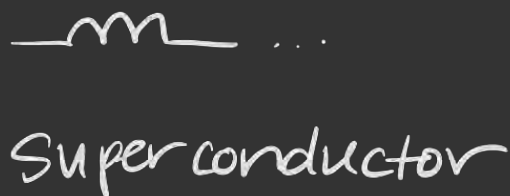
London's First Equation:

$$\vec{E} = \frac{d}{dt} (\Lambda \vec{J})$$

replaces Ohm's law $\rightarrow \Lambda \equiv \frac{m^*}{n^* q^{*2}}$



normal wire

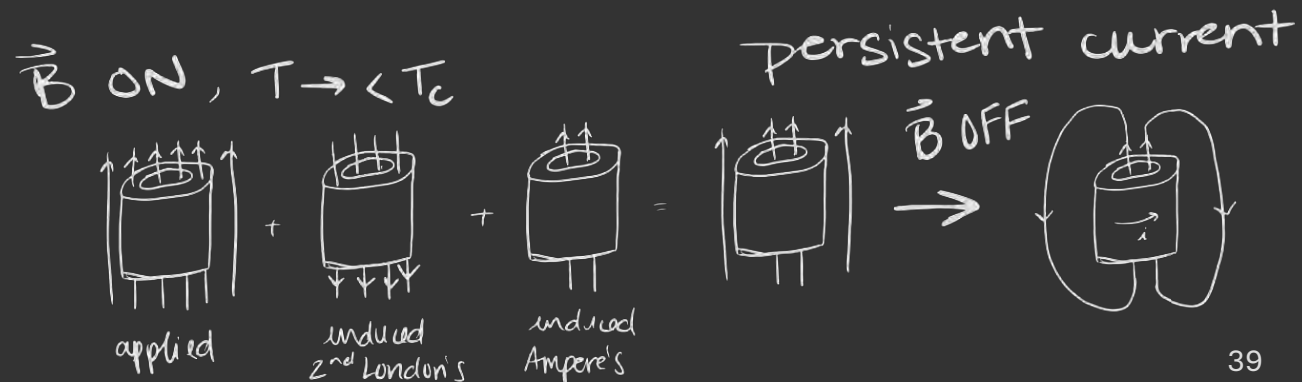


Superconductor
 $(V = L \frac{di}{dt})$

London's Second Equation:

$$\nabla \times (\Lambda \vec{J}) = -\vec{B}$$

enforces Meisner effect by demanding initial conditions on Faraday's Law ($\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$)



Macroscopic Quantum Model



The whole superconducting material can be described by a macroscopic quantum wave function comprised of the superposition of cooper pairs

→ Phase coherence at a macroscopic scale!

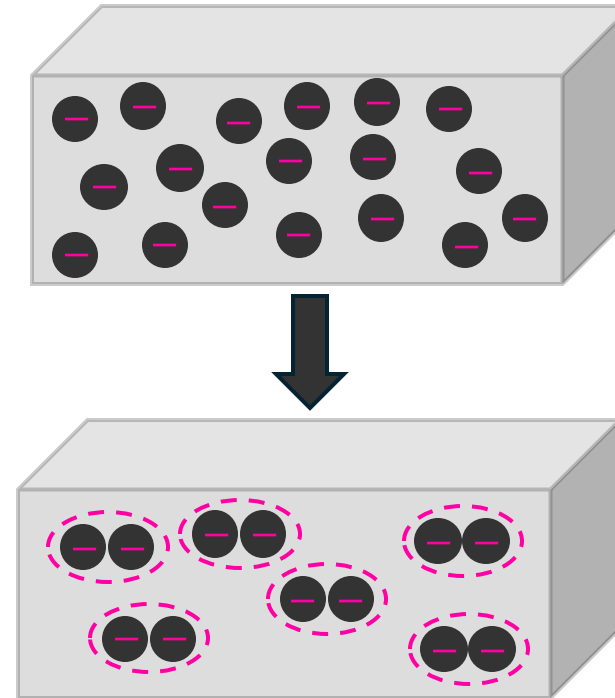
$$\Psi(\mathbf{r}, t) = \sqrt{n^*(\mathbf{r}, t)} e^{i\theta(\mathbf{r}, t)}$$

$$i\hbar \frac{\partial}{\partial t} \Psi(\mathbf{r}, t) = \frac{1}{2m^*} \left(\frac{\hbar}{i} \nabla - q^* \mathbf{A}(\mathbf{r}, t) \right)^2 \Psi(\mathbf{r}, t) + q^* \phi(\mathbf{r}, t) \Psi(\mathbf{r}, t)$$

n^* -- local density of cooper pairs

q^* -- charge of cooper pair

m^* -- mass of cooper pair



$T > T_c$
Normal electrons

$T < T_c$
Superconducting
cooper pairs

Flux Quantization

the quantum wavefunction can derive superconducting current density:

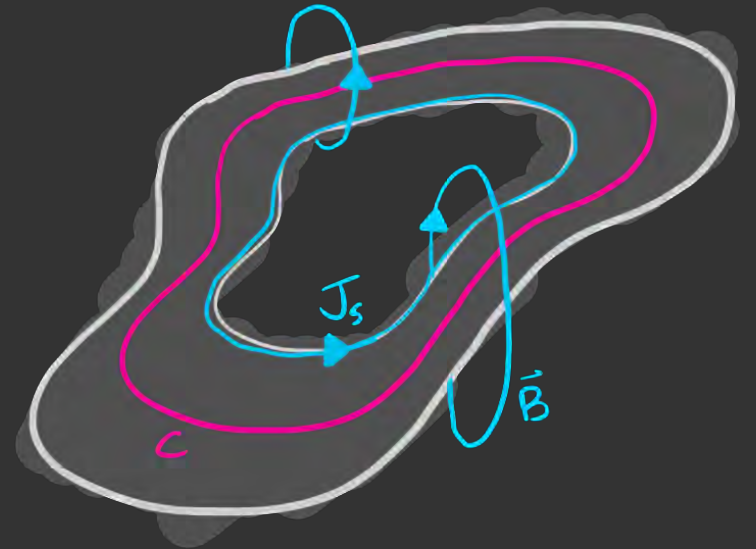
$$\vec{J}_s = -\frac{1}{\Lambda} \left(\frac{\hbar}{2e} \nabla \theta + \vec{A} \right)$$

then the flux is

$$\Phi = \int \vec{B} \cdot d\hat{s} = \oint_C \vec{A} \cdot d\vec{l}$$

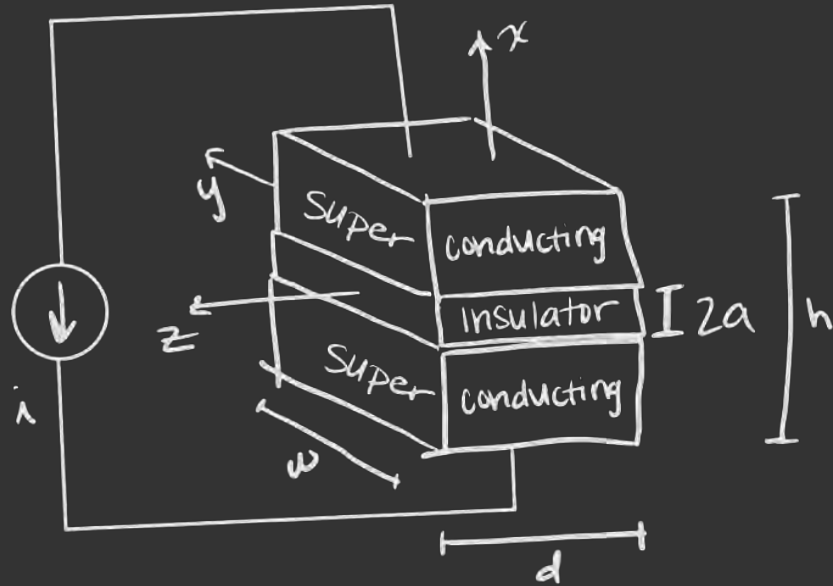
$$\Phi = \oint_C \left(-\Lambda \vec{J}_s + \frac{\hbar}{2e} \nabla \theta \right) \cdot d\vec{l} = \frac{\hbar}{2e} \Delta \theta \xrightarrow{\frac{n}{2\pi}} \frac{\hbar}{2e} n \rightarrow \Phi = n \Phi_0$$

$\rightarrow J_s = 0$ for contour deep below surface

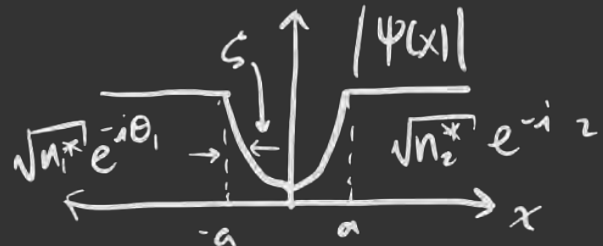
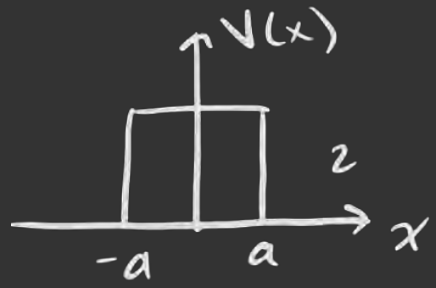
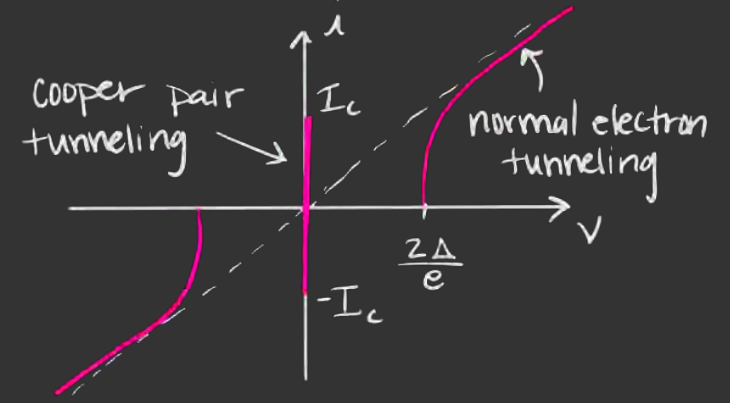


$\Phi_0 = 2.07 \times 10^{-15} \text{ Wb}$
single flux quantum

Josephson Tunneling



$$\vec{J}_s = \frac{q^*}{m^*} \text{Re} \left\{ \Psi^* \frac{\hbar}{i} \nabla \Psi \right\}$$



current-phase

$$J_s(y, z, t) = J_c(y, z) \sin(\theta_1(y, z, t) - \theta_2(y, z, t))$$

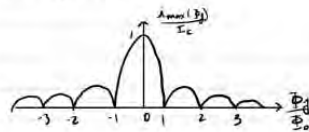
voltage-phase

$$\frac{\partial \phi(y, z, t)}{\partial t} = \frac{2\pi}{\Phi_0} \int_1^2 \vec{E}(\vec{r}, t) \cdot d\vec{l}$$

Extended Josephson junction model

8.5 Short Josephson Junctions

"extended Josephson junctions":
 - gauge invariant phase and current density is NOT uniform across the junction
 - interference patterns across a single junction → single junction SQID
 - vortices can exist within a junction and dissipate power as they move



current density distributions for short jf

"short" requirements:

- magnetic field produced by currents in the junction are negligible compared to external applied magnetic field
- length and width less than λ_j → Josephson penetration depth



Left diagram: $\Phi_j = 0$, $\phi(z) = \phi(0)$, $\phi(\frac{a}{2}) - \phi(-\frac{a}{2}) = 0$, $\phi(0) = \frac{\pi}{2}$, $\frac{I_{max}}{I_c} = 1$

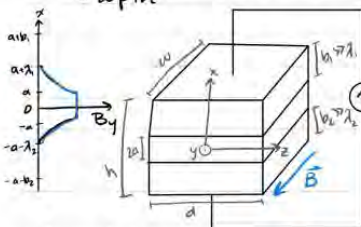
Right diagram: $\Phi_j = \frac{\Phi_0}{2}$, $\phi(z) = \frac{\pi}{2} \frac{z}{a} + \phi(0)$, $\phi(\frac{a}{2}) - \phi(-\frac{a}{2}) = \pi$, $\phi(0) = \frac{\pi}{2}$



Left diagram: $\Phi_j = \Phi_0$, $\phi(z) = 2\pi \frac{z}{a} + \phi(0)$, $\phi(\frac{a}{2}) - \phi(-\frac{a}{2}) = 2\pi$, $\phi(0) = 0$, $\frac{I_{max}}{I_c} = 0$

Right diagram: $\Phi_j = \frac{3\Phi_0}{2}$, $\phi(z) = 3\pi \frac{z}{a} + \phi(0)$, $\phi(\frac{a}{2}) - \phi(-\frac{a}{2}) = 3\pi$, $\phi(0) = -\frac{\pi}{2}$

Vortex + smaller half period current



applying Ampere's law on path through x-z plane and integrating across z AND assuming self induced current fields are zero gives equation for spatially dependent phase

$$\phi(z) = \frac{2\pi}{\Phi_0} B_y h_{eff} z + \phi(0)$$

$h_{eff} = \lambda_j + 2a$
 effective height

plugging in to current-phase relation

$$J_x(z, \phi_0) = I_c \frac{\sin(\frac{2\pi}{\Phi_0} B_y h_{eff} z + \phi_0)}{\sin(\frac{\pi}{2})} \sin(\phi_0)$$

$\Phi_j = \Phi_0 h_{eff} =$ external flux through junction

Energy for short junction

$$W = W_s + W_{in} \quad \text{superconductor storage} \quad \text{insulating region}$$

$$W = \frac{1}{2\mu_0} \int_{\lambda_j}^{\lambda_j} B^2 dv + \frac{1}{2} \int_{\lambda_j}^{\lambda_j} \lambda_j^2 dv + \int_{\lambda_j}^{\lambda_j} \frac{\Phi_0}{2\pi} J_c(y, z) [1 - \cos(\phi(y, z))] dy dz$$

then we can more rigorously define a short junction as one where energy stored in external field is much larger than that due to current flow

8.6 Long Josephson Junctions

Now, the self fields must be taken in to account because the energy stored in them is comparable to the applied field → which happens when $d \sim \lambda_j$

Same as for short junctions - but now $\vec{B}_y \neq B_y \hat{y} \rightarrow$ it is influenced by self fields that must be accounted for with Ampere's law

$$\nabla \times \vec{B} = \mu_0 \vec{J} + \epsilon_0 \mu_0 \frac{\partial E}{\partial t}$$

$$\frac{\partial B_y(z)}{\partial z} = -\mu_0 \vec{J}_x(z)$$

from general equation for gauge invariant flux:

$$\frac{\partial \phi}{\partial z} = \frac{2\pi}{\Phi_0} B_y h_{eff}$$

$$\frac{\partial^2 \phi}{\partial z^2} = -\frac{2\pi \mu_0 h_{eff}}{\Phi_0} \vec{J}_x(z)$$

So our new phase constraint is:

$$\frac{\partial^2 \phi(z)}{\partial z^2} = \frac{\sin \phi(z)}{\lambda_j^2}$$

Josephson penetration depth

$$\lambda_j = \sqrt{\frac{\Phi_0}{2\pi \mu_0 J_c h_{eff}}}$$

for short jf $d \ll \lambda_j \rightarrow \frac{\partial^2 \phi(z)}{\partial z^2} \approx 0$

typical values: for $h_{eff} \approx 500 \text{ nm}$
 $\lambda_j \approx 2 \mu\text{m}$ for $J_c = 10^6 \text{ A/m}^2$
 $\lambda_j \approx 20 \mu\text{m}$ for $J_c = 10^4 \text{ A/m}^2$

constraint can only be solved numerically to the rest of the section just explores special case solutions

particular solution:

$$\phi(z) = -2 \sin^{-1} \left(\text{sech} \left(\frac{z-z_0}{\lambda_j} \right) \right)$$

solution follows:

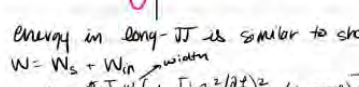
$$B_y(z) = \frac{\Phi_0}{\pi \lambda_j h_{eff}} \text{sech} \left(\frac{z-z_0}{\lambda_j} \right)$$

$$J_x(z) = 2 J_c \tanh \left(\frac{z-z_0}{\lambda_j} \right) \text{sech} \left(\frac{z-z_0}{\lambda_j} \right)$$

with boundary conditions:

$$z=0 \text{ and } \lim_{z \rightarrow \pm \infty} \phi(z) = 0$$

a Josephson vortex is trapped!



Energy in long JJ is similar to short

$$W = W_s + W_{in} \quad \text{width}$$

$$W_{in} = \frac{\Phi_0 J_c \omega}{2\pi} \int dz \left[\frac{1}{2} \left(\frac{\partial \phi}{\partial z} \right)^2 + (1 - \cos \phi) \right]$$

magnetic field intensity for a vortex to "enter" the junction:

$$B_{c1} = \frac{\mu_0 E_y}{\Phi_0} = \frac{2 \Phi_0}{\pi^2 \lambda_j h_{eff}}$$

Vortices can be used to visualise current distribution as jf is driven by voltage

with voltage drive, Ampere's law keeps E term and we now care about time:

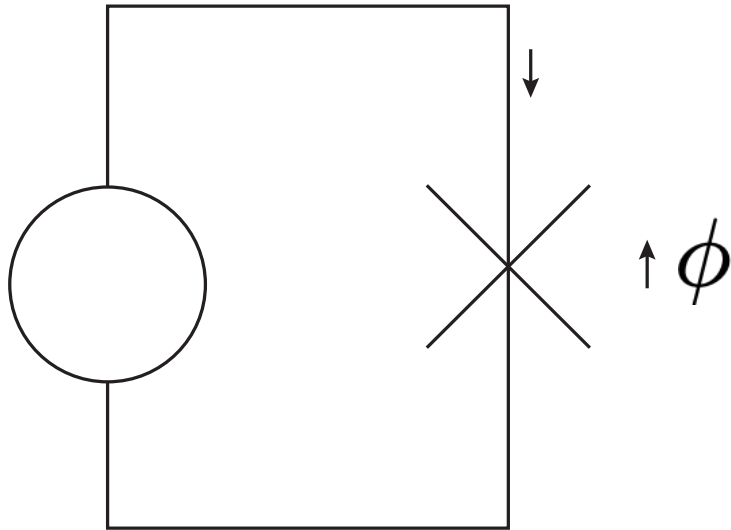
$$\frac{\partial^2 \phi(z,t)}{\partial z^2} = -\frac{2\pi h_{eff}}{\Phi_0} \left[\mu_0 \vec{J}_x(z,t) + \epsilon_0 \mu_0 \frac{\partial E_x}{\partial t} \right]$$

using voltage phase relation, this simplifies to the sine-Gordon equation

$$\frac{\partial^2 \phi}{\partial z^2} - \frac{1}{\lambda_j^2} \frac{\partial^2 \phi}{\partial t^2} = \frac{1}{\lambda_j^2} \sin \phi$$

linearized sine-Gordon equation gives rise to Josephson plasma frequency: below this limit $\omega_{J1}^2 = \frac{4\pi}{\lambda_j^2} \cos \phi_0$ no propagating solutions

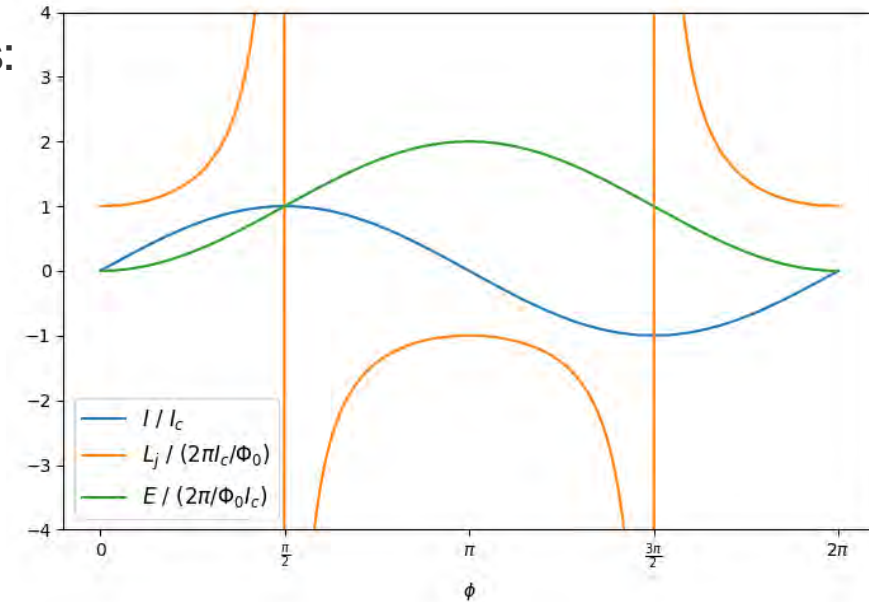
Lumped Element JJ Model



JJ current and voltage relations:

$$i = I_c \sin \phi$$

$$v(t) = \frac{\Phi_0}{2\pi} \frac{d\phi}{dt}$$



Ideal junction can be thought of as a non-linear phase dependent inductor:

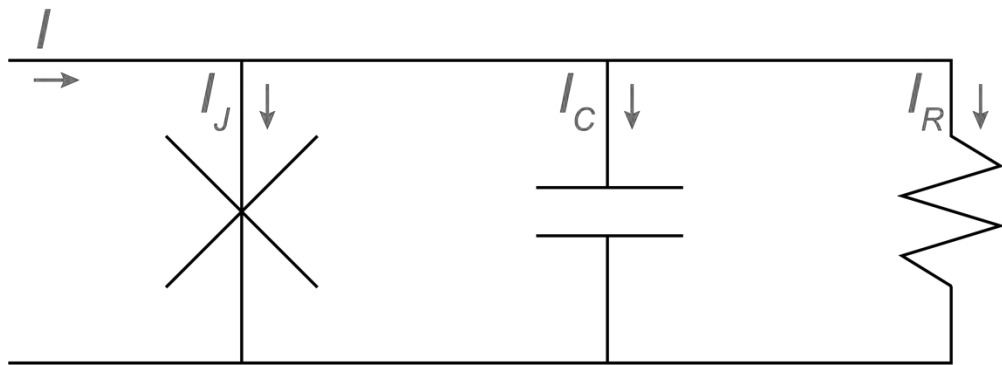
$$L_j = \frac{\Phi_0}{2\pi I_c \cos \phi}$$

Ideal energy dissipation:

$$\begin{aligned} E_{JJ} &= \int IV dt = \int (I_c \sin \phi) \left(\frac{\hbar}{2e} \frac{\partial \phi}{\partial t} \right) dt \\ &= \frac{\Phi_0}{2\pi} I_c \int_0^\phi \sin \phi' d\phi' \\ &= \frac{\Phi_0}{2\pi} I_c (1 - \cos \phi) \end{aligned}$$

JJ as a Circuit Element

Resistively and Capacitively Shunted Junction (RCSJ) model



$$T_a = mgl \sin \phi + \eta \dot{\phi} + \mu \ddot{\phi}$$

Applied torque

viscosity

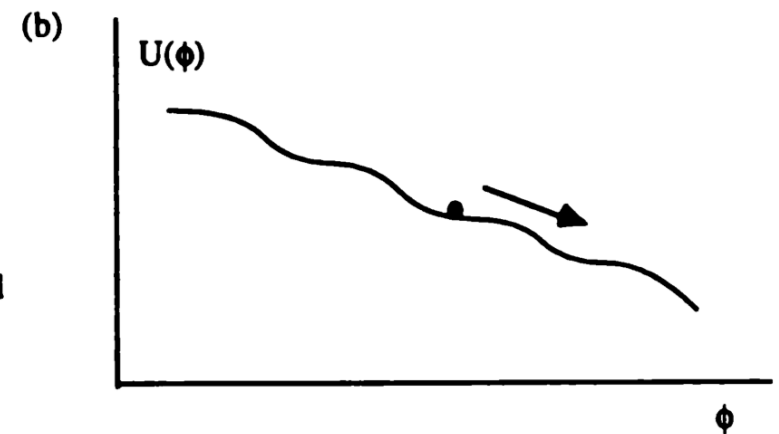
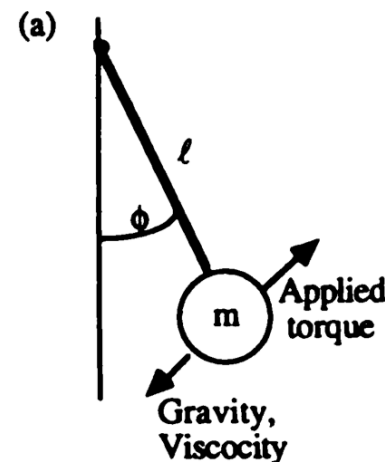
Moment of inertia

Analogous to a driven pendulum, with a washboard potential

$$I = I_J + I_R + I_C$$

$$I = I_c \sin \phi + \frac{1}{R} \frac{\Phi_0}{2\pi} \dot{\phi} + C \frac{\Phi_0}{2\pi} \ddot{\phi}$$

$$\rightarrow U = \frac{\Phi_0}{2\pi} I_c \left(1 - \frac{I}{I_c} \phi - \cos \phi \right)$$



Superconducting Circuit Basics

flux: $\phi = \int_{-\infty}^t v dt$

because of flux quantization:

charge: $Q = \int_{-\infty}^t i dt$

phase: $\varphi = \frac{2\pi\phi}{\Phi_0}$

all branch elements can be described by constitutive relations.

capacitive:

$$v_b = f(Q_b)$$

inductive:

$$\lambda_b = g(\phi_b)$$

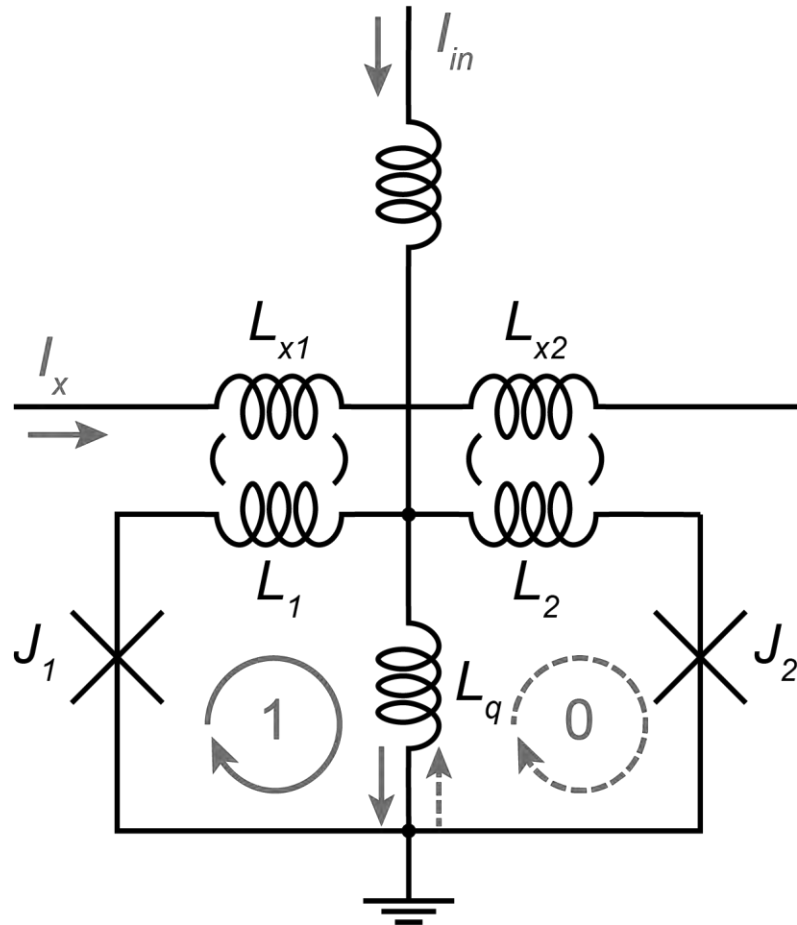
e.g. for inductor:

$$\lambda_b = \frac{\phi_b}{L}$$

or JJ:

$$\lambda_b = I_c \sin\left(\frac{2\pi}{\Phi_0} \phi_b\right)$$

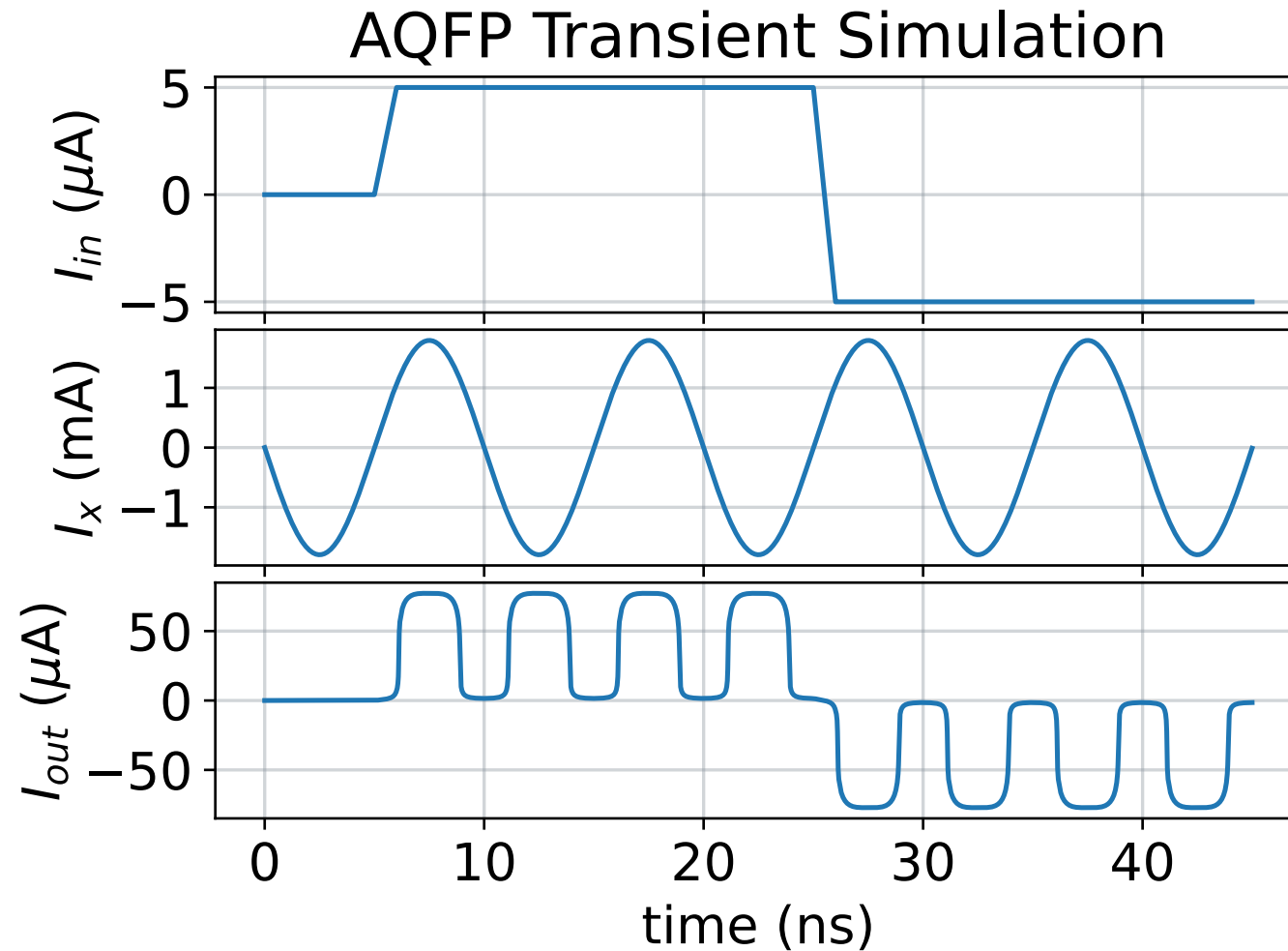
The Adiabatic Quantum Flux Parametron



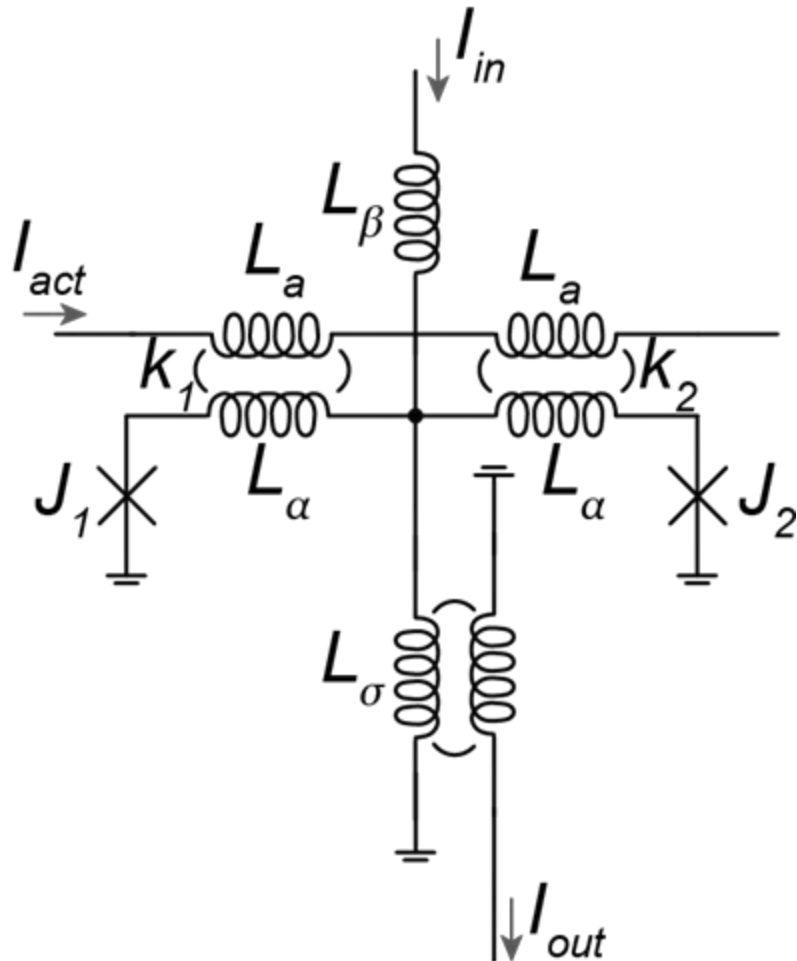
Depending on the polarity of a small input current, I_{in} , a single magnetic flux quantum will be trapped in either the left or right loop, corresponding to a digital 1 or 0 value

The fluxon will only be trapped if the AQFP is activated with an excitation signal, I_x , which forces the Josephson junctions into their low-impedance state

The Adiabatic Quantum Flux Parametron



AQFP Circuit Analysis: Node Method

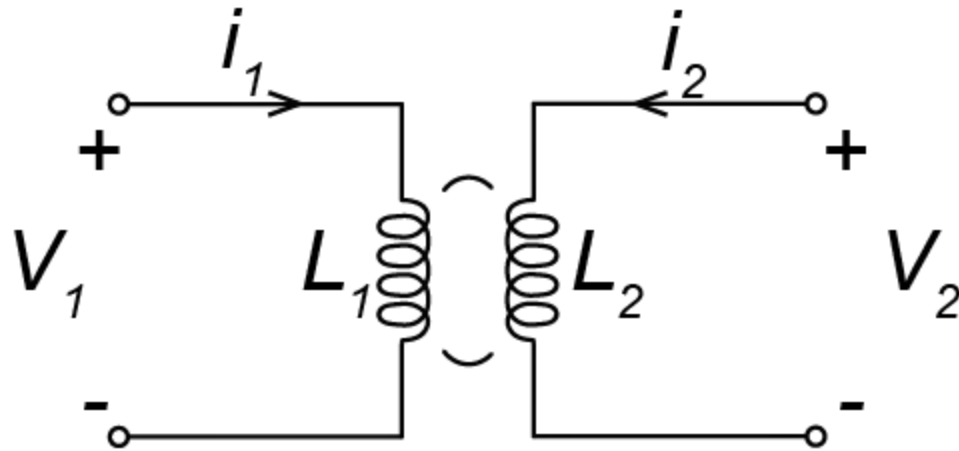


GOAL: There are two dynamical degrees of freedom within the AQFP circuit (one for each JJ) and we want to find the operating point of the circuit given some input and activation signal, so we are solving for the output signal.

1. Define circuit topology with Kirchoff's current laws
2. Then express KCLs in terms of branch variable dynamics to constrain the system to a particular operating point

But before starting, we need to understand how to handle the inductive coupling transformers.

AQFP Circuit Analysis: Transformers



M : mutual inductance

$$emf_1 = M \frac{di_2}{dt} \rightarrow \Phi_1 = Mi_2$$

$$\begin{bmatrix} \Phi_1 \\ \Phi_2 \end{bmatrix} = \begin{pmatrix} L_1 & M \\ M & L_2 \end{pmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

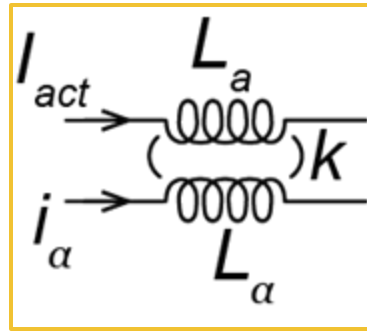
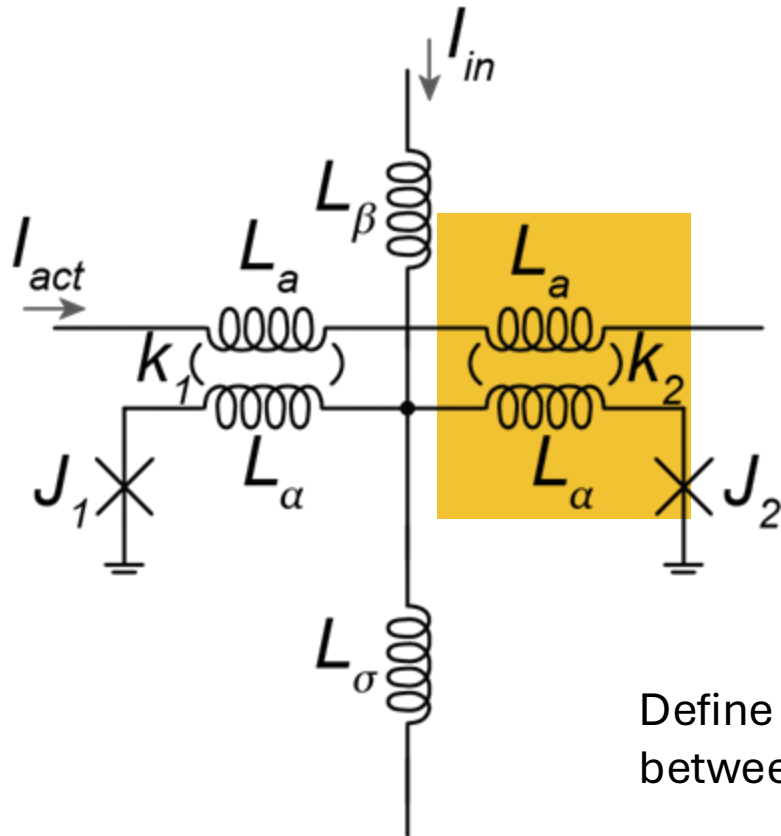
k : coupling constant
 n : inductor ratio

$$M = k\sqrt{L_1L_2}$$

$$n^2 = L_2/L_1$$

$$\rightarrow \begin{bmatrix} \Phi_1 \\ \Phi_2 \end{bmatrix} = L_1 \begin{pmatrix} 1 & nk \\ nk & n^2 \end{pmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

AQFP Circuit Analysis: Transformers



$$\begin{bmatrix} \Phi_a \\ \Phi_\alpha \end{bmatrix} = L_a \begin{pmatrix} 1 & nk \\ nk & n^2 \end{pmatrix} \begin{bmatrix} i_a \\ i_\alpha \end{bmatrix}$$

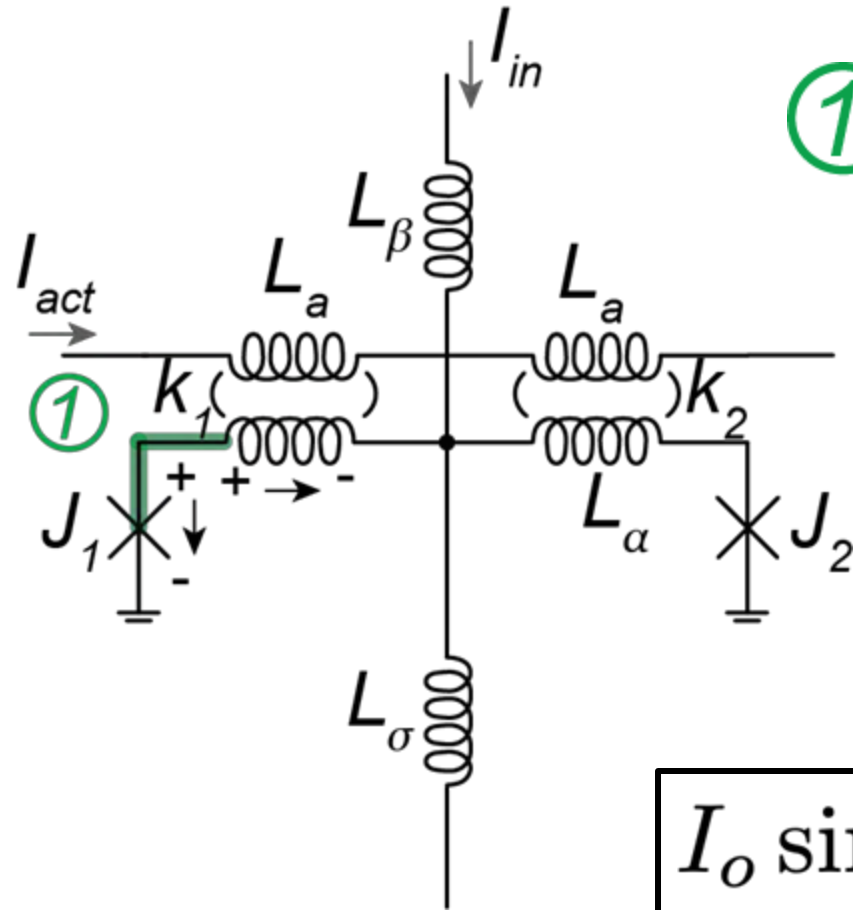
$$i_\alpha = \frac{1}{L_\alpha(1 - k^2)} (\phi_\alpha - \phi_a nk) \bar{\Phi}_o$$

Flux has been replaced by phase: $\Phi = \frac{\Phi_o}{2\pi} \phi = \bar{\Phi}_o \phi$

Define phase angle that characterizes the relationship between activation inductor and loop inductor: $\alpha \equiv \frac{1}{1 - k^2} (\phi_a - \frac{k}{n} \phi_\alpha)$

$$i_\alpha = \frac{\bar{\Phi}_o}{L_\alpha} (\phi_\alpha - nk\alpha)$$

QFP Circuit Analysis: Node Method



$$\textcircled{1} -i_{j1} - i_{\alpha1} = 0$$

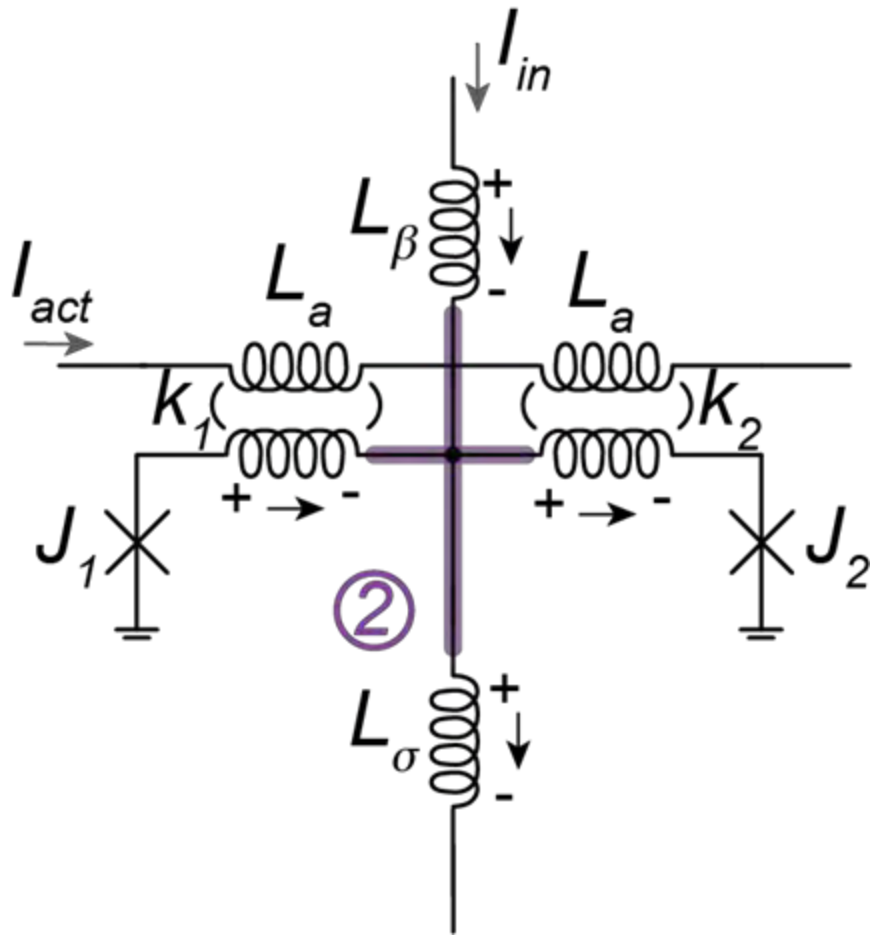
$$i_{\alpha1} = \frac{\bar{\Phi}_o}{L_\alpha} (\phi_{\alpha1} - nk_1\alpha)$$

$$\phi_{\alpha1} = \phi_{j1} - \phi_\sigma$$

Define inverse inductance: $\ell = \frac{\bar{\Phi}_o}{L}$

$$I_o \sin \phi_{j1} + \ell_{\alpha1} (\phi_{j1} - \phi_\sigma - nk_1\alpha) = 0$$

QFP Circuit Analysis: Node Method



$$\textcircled{2} \quad i_\beta + i_{\alpha 1} - i_{\alpha 2} - i_\sigma = 0$$

$$i_{\alpha 2} = \frac{\bar{\Phi}_o}{L_\alpha} (\phi_{\alpha 2} - nk_2\alpha)$$

$$\hookrightarrow \phi_{\alpha 2} = \phi_\sigma - \phi_{j2}$$

$$l_\beta(\phi_\beta - \phi_\sigma) + l_{\alpha 1}(\phi_{j1} - \phi_\sigma - nk_1\alpha)$$

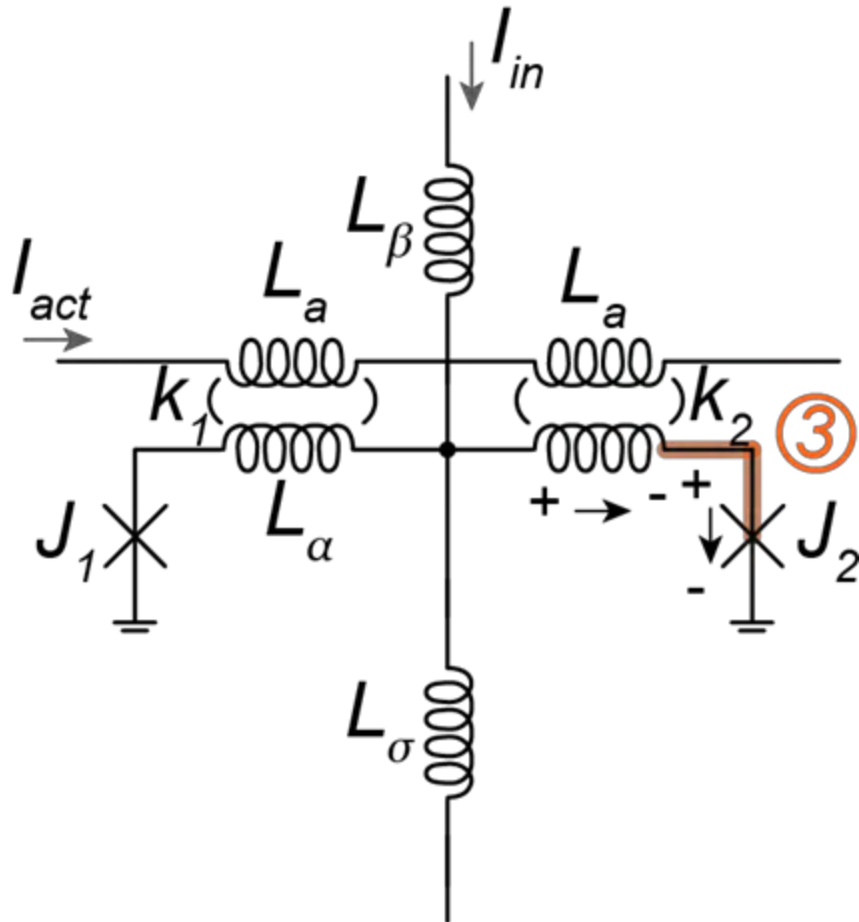
$$- l_{\alpha 2}(\phi_\sigma - \phi_{j2} - nk_2\alpha) - l_\sigma\phi_\sigma = 0$$

assume $l_{\alpha 1} = l_{\alpha 2}$

$$l_\alpha(\phi_{j1} + \phi_{j2} - 2\phi_\sigma + n(k_2 - k_1)\alpha)$$

$$+ l_\beta(\phi_\beta - \phi_\sigma) - l_\sigma\phi_\sigma = 0$$

QFP Circuit Analysis: Node Method

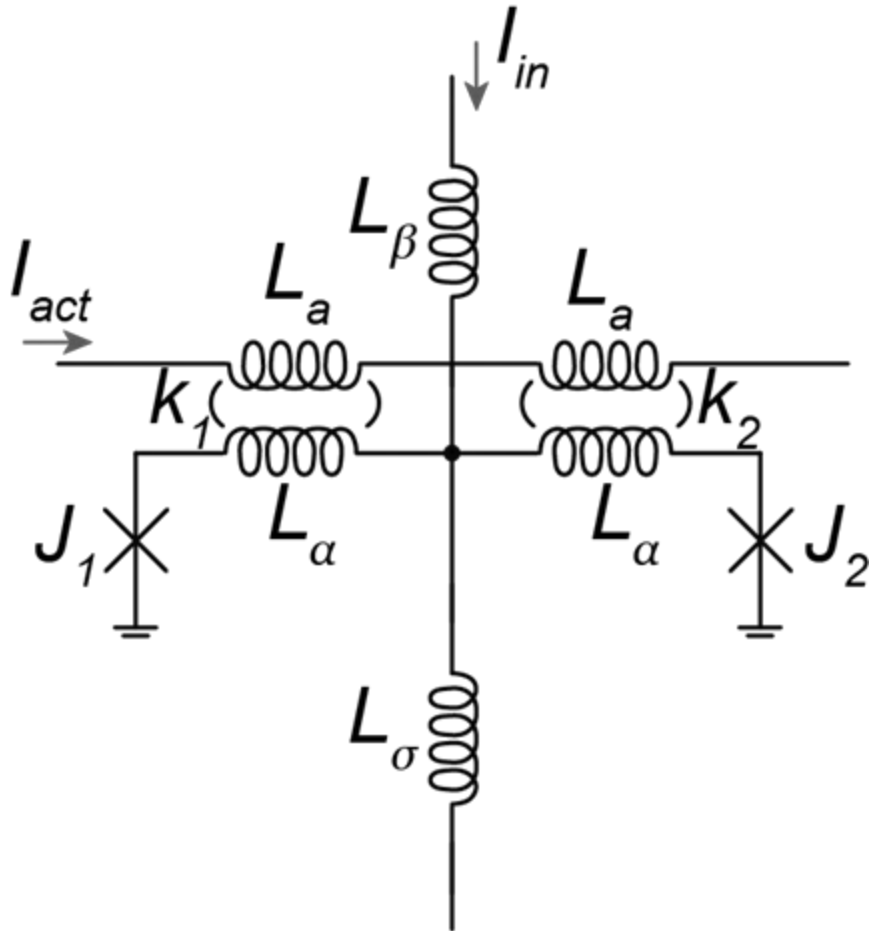


$$\textcircled{3} \quad i_{\alpha 2} - i_{j 2} = 0$$

$$l_{\alpha 2}(\phi_{\sigma} - \phi_{j 2} - nk_2\alpha) - I_o \sin \phi_{j 2} = 0$$

$$I_o \sin \phi_{j 2} + l_{\alpha 2}(\phi_{j 2} - \phi_{\sigma} + nk_2\alpha) = 0$$

QFP Circuit Analysis: Circuit Constraints



KCL summary :

$$\textcircled{1} I_o \sin \phi_{j1} + l_{\alpha 1}(\phi_{j1} - \phi_\sigma - nk_1\alpha) = 0$$

$$\textcircled{2} l_\alpha(\phi_{j1} + \phi_{j2} - 2\phi_\sigma + n(k_2 - k_1)\alpha) + l_\beta(\phi_\beta - \phi_\sigma) - l_\sigma\phi_\sigma = 0$$

$$\textcircled{3} I_o \sin \phi_{j2} + l_{\alpha 2}(\phi_{j2} - \phi_\sigma + nk_2\alpha) = 0$$

QFP Circuit Analysis: Circuit Constraints

We have an extra equation for only two degrees of freedom, so we can express equations in terms of sum and difference across both JJs:

$$\phi_+ = \frac{1}{2}(\phi_{j1} + \phi_{j2}) \quad \phi_- = \frac{1}{2}(\phi_{j1} - \phi_{j2})$$

$$\textcircled{1} + \textcircled{3}$$

$$2I_o \sin \phi_+ \cos \phi_- + l_\alpha (2\phi_+ - 2\phi_\sigma + n(k_2 - k_1)\alpha) = 0$$

$$\textcircled{1} - \textcircled{3}$$

$$2I_o \cos \phi_+ \sin \phi_- + l_\alpha (2\phi_- + n(k_2 + k_1)\alpha) = 0$$

QFP Circuit Analysis: Circuit Constraints

Use (2) to solve for ϕ_σ :

$$\phi_\sigma = \frac{l_\beta \phi_\beta + l_\alpha (2\phi_+ + n(k_2 - k_1)\alpha)}{2l_\alpha + l_\sigma + l_\beta}$$

① + ③

$$2I_o \sin \phi_+ \cos \phi_- + l_+ \left(2\phi_+ + n(k_2 - k_1)\alpha + \frac{2l_\beta}{l_\sigma + l_\beta} \phi_\beta \right) = 0$$

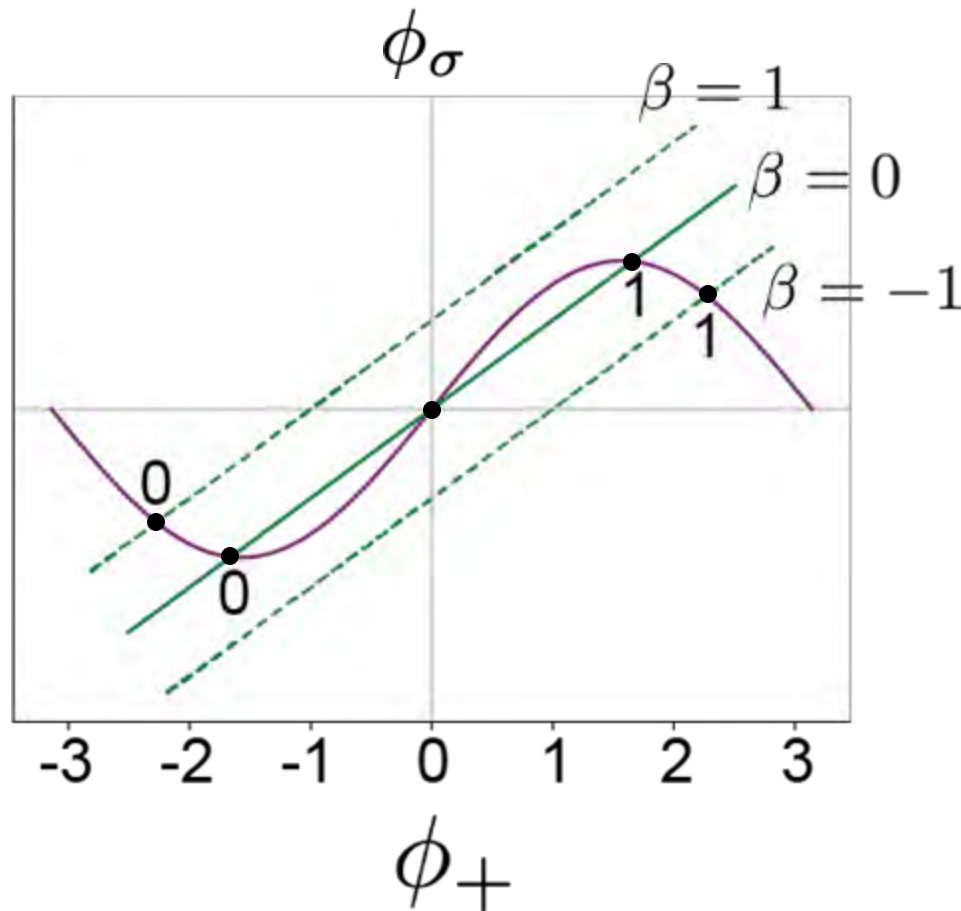
① - ③

$$l_+ = \frac{l_\alpha (l_\sigma + l_\beta)}{2l_\alpha + l_\sigma + l_\beta}$$

$$2I_o \cos \phi_+ \sin \phi_- + l_\alpha (2\phi_- + n(k_2 + k_1)\alpha) = 0$$

Solved when $\alpha = \pm \frac{2\pi}{n(k_2 + k_1)}$ and $\phi_- = \mp \pi \rightarrow$ which corresponds to double well potential

QFP Circuit Analysis: Load Line

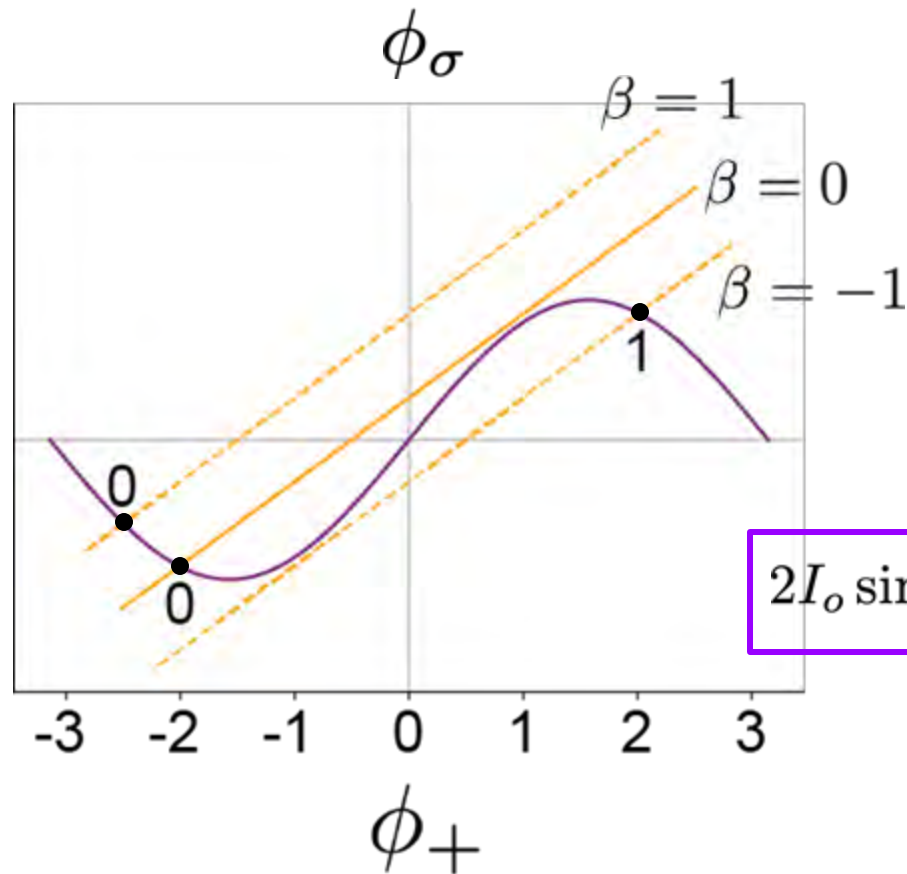


$$k_1 = k_2 \rightarrow \mathbf{BUF}$$

No α dependence on logic state

$$2I_o \sin \phi_+ + l_+ \left(2\phi_+ + \frac{2l_\beta}{l_\sigma + l_\beta} \phi_\beta \right) = 0$$

QFP Circuit Analysis: Load Line



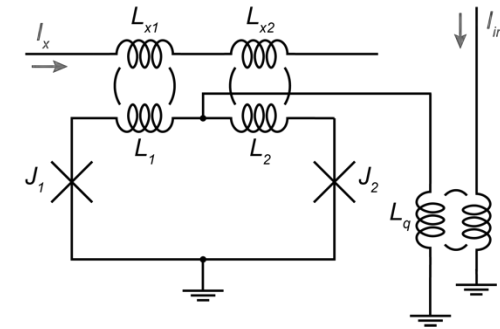
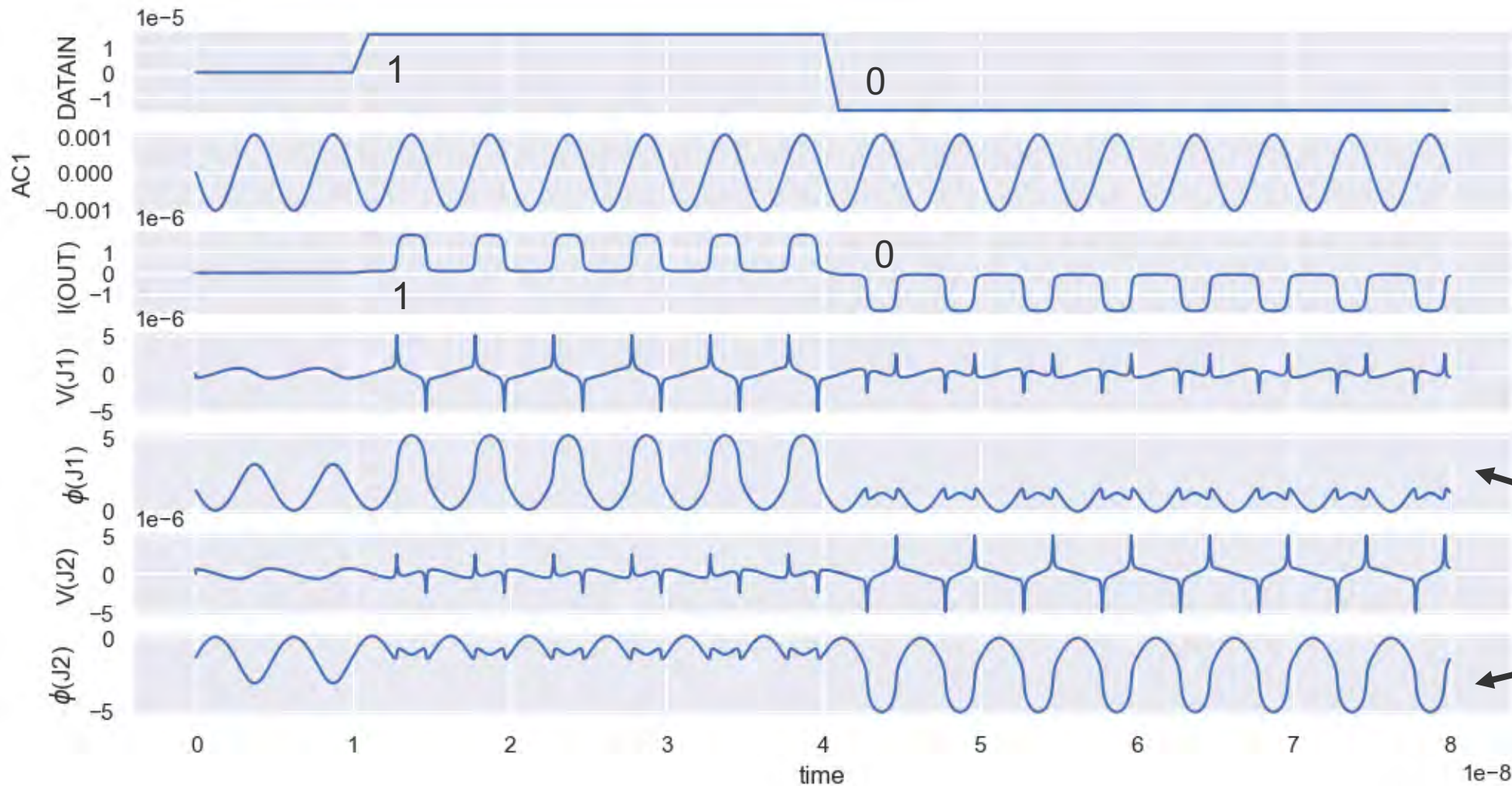
$$k_1 > k_2$$

α dependence on logic state behaves as a current source in one loop, causing the null input to favor one side

$$2I_o \sin \phi_+ + l_+ \left(2\phi_+ + n(k_2 - k_1)\alpha + \frac{2l_\beta}{l_\sigma + l_\beta} \phi_\beta \right) = 0$$

Add a guide on variables

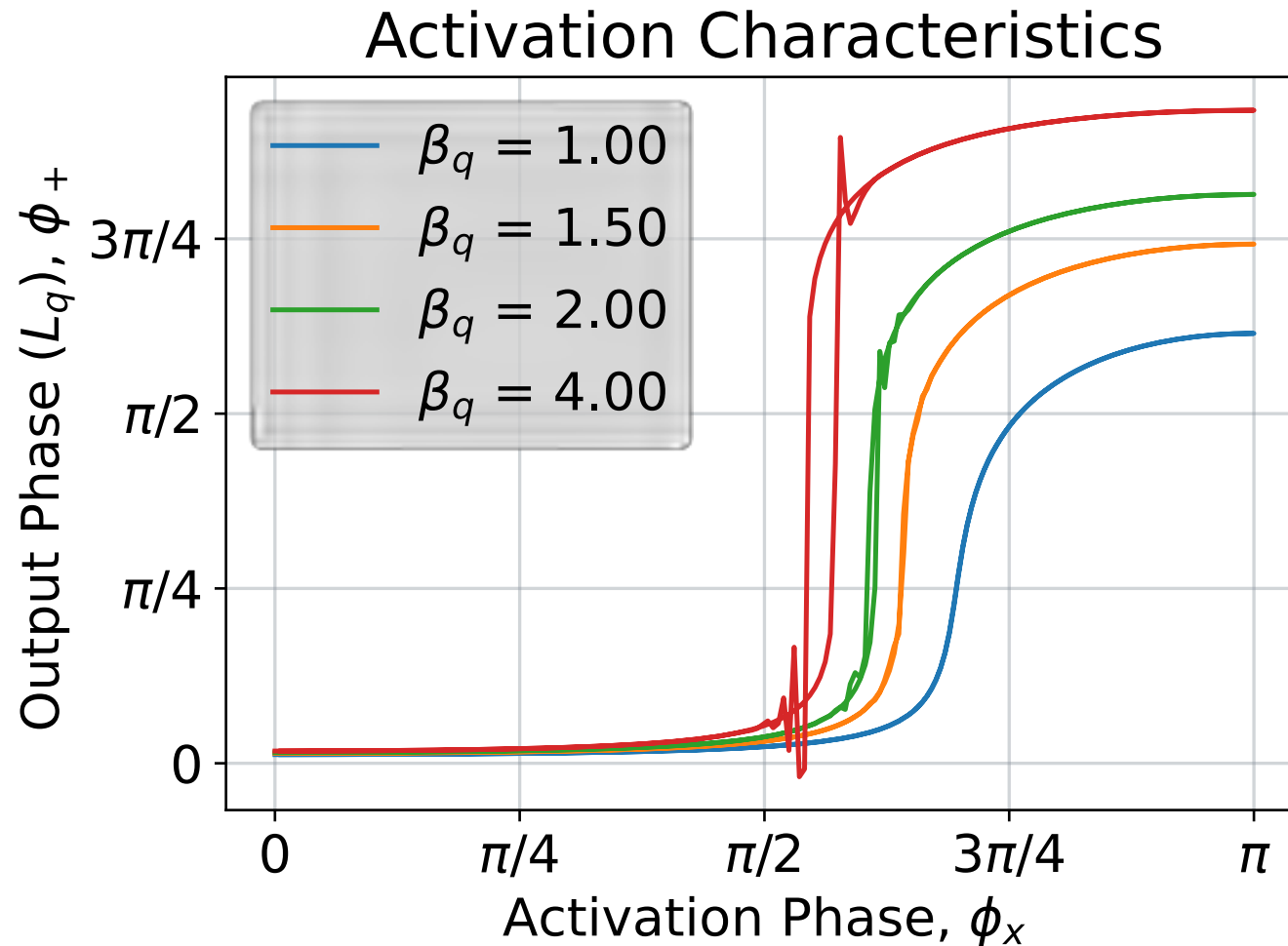
Simulated Transient Behavior of AQFP



200MHz output signal

2π phase shift between both junctions for each data pulse

Activation Characteristics

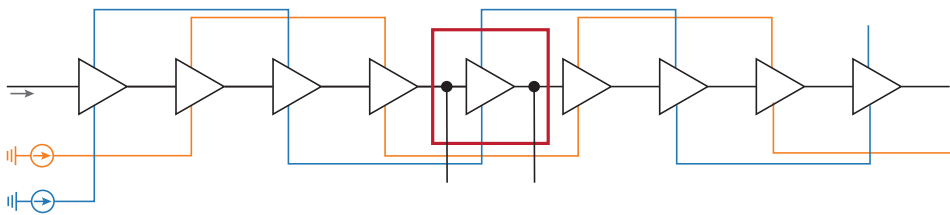


$\beta_q \rightarrow \ell_\sigma$

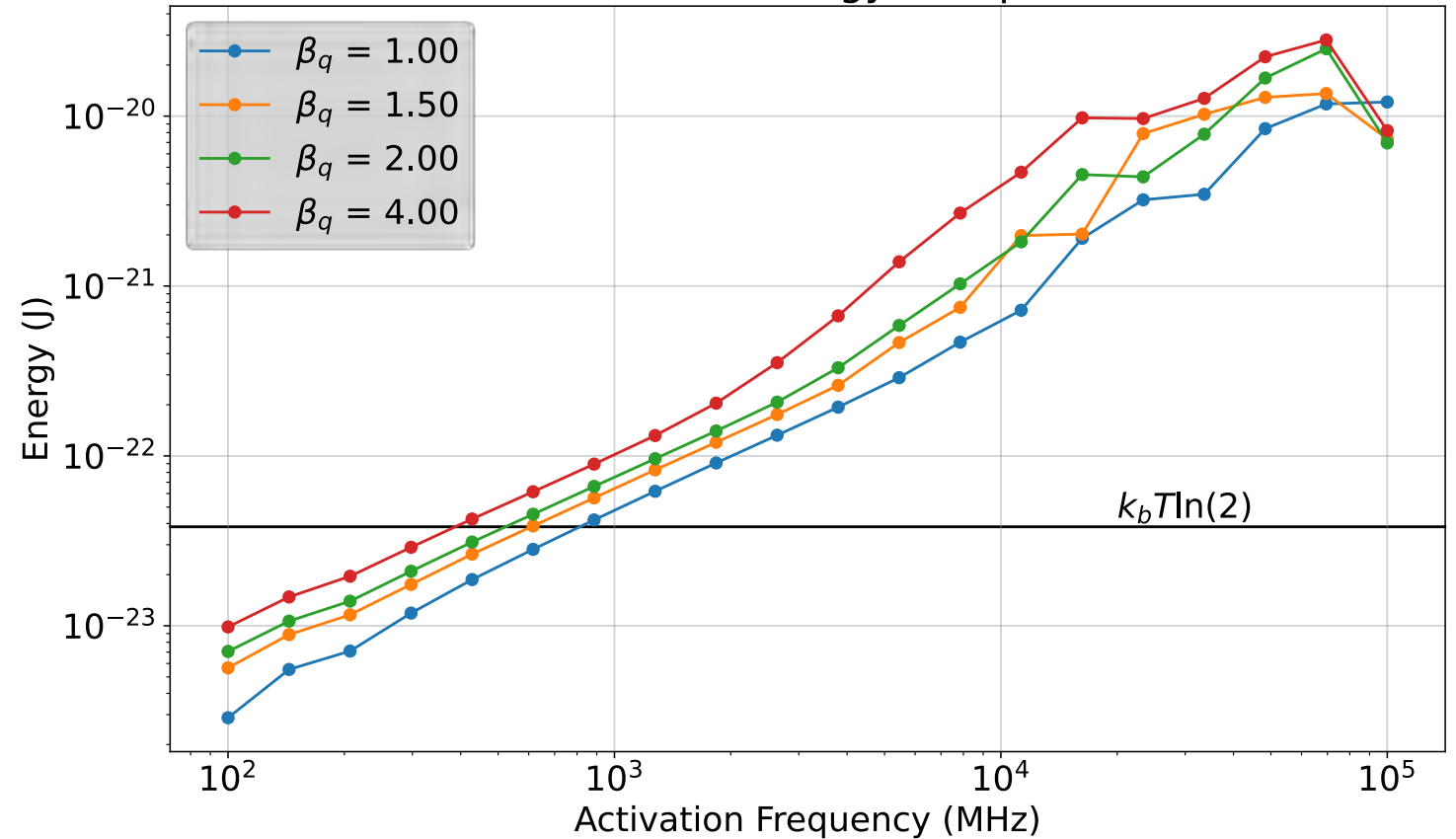
SPICE Extracted Switching Energy



$$E_{\text{diss}} = \int_0^{1/f} I_{x1} \cdot (V_{\text{out}} - V_{\text{in}}) dx$$



AQFP Buffer Energy Dissipation



AQFP Energy Dissipation



Energy required for a single QFP switching, phase across the junction, ϕ , increases by 2π and the energy dissipated can be described with the voltage across the JJ resistor

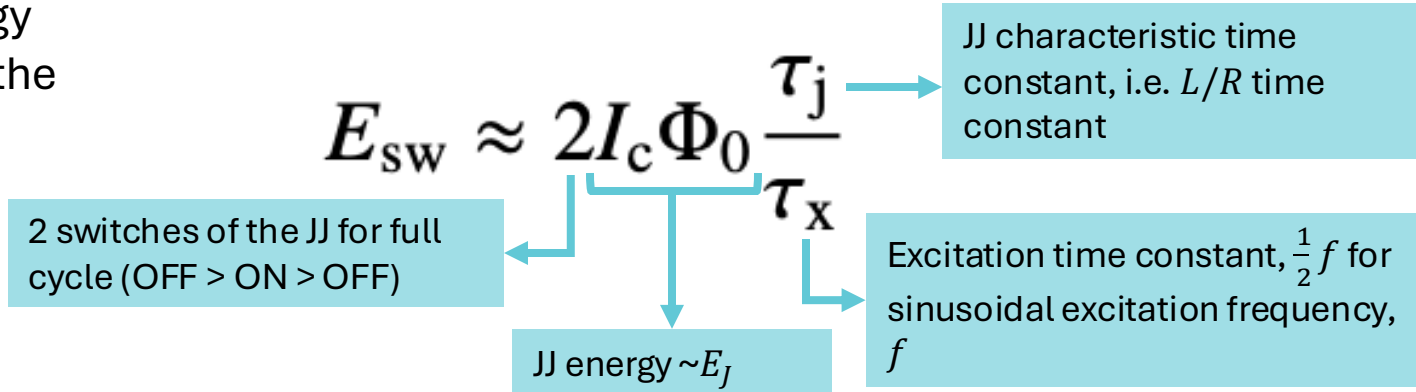
$$E_x = \int_0^{\tau_x} \frac{V_1^2}{R} dt = \frac{1}{R} \left(\frac{\Phi_0}{2\pi} \right)^2 \int_0^{\tau_x} \left(\frac{d\phi_1}{dt} \right)^2 dt$$

$$\approx \frac{1}{R} \left(\frac{\Phi_0}{\tau_x} \right)^2 \int_0^{\tau_x} dt = \frac{\Phi_0^2}{R\tau_x}$$

Then for excitation and reset to single well, the total switching energy is $2E_x$

$$E_{sw} = E_x + E_r \approx \frac{2\Phi_0^2}{R\tau_x}$$

Alternative phase-evolution derivation:



$$\tau_j \approx 2\pi \frac{L_j}{R} = \frac{\Phi_0}{I_c R} = \sqrt{\frac{2\pi \Phi_0 C_s}{\beta_c J_c}}$$

Junction capacitance per area

McCumber parameter:

$$\beta_c = Q^2 = \frac{2\pi R^2 C I_c}{\Phi_0}$$

Critical current density

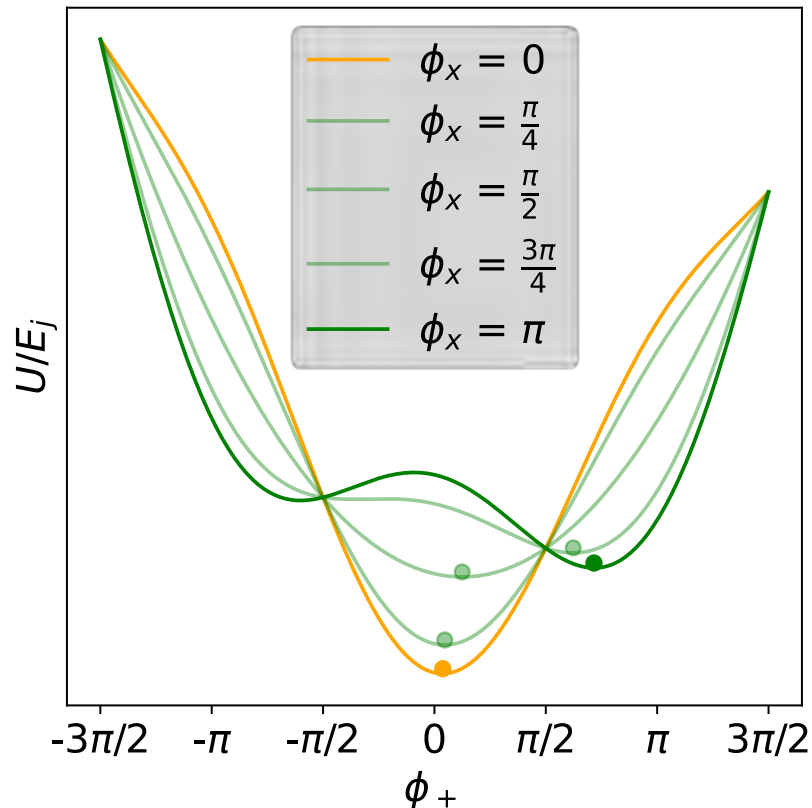
More Fundamental Energy Analysis?



- How accurate is the classical SPICE $\int (I \cdot V)dt$ method for determining the energy dissipation limits of the AQFP ?
- Could it actually operate in a reversible adiabatic regime?
- Circuit quantization, a method for linking a physical circuit to its corresponding quantum Hamiltonian, could provide a path to a more rigorous definition for the energy dissipated when an AQFP undergoes a classical bit-flip
- Additionally, circuit quantization provides a formalism for deriving the potential energy for the circuit, providing another perspective on AQFP circuit behavior

AQFP Potential Energy

$$\frac{U_{2D}}{E_j} = \frac{(\phi_+ - \phi_{in})^2}{2\beta_q} - 2 \cos \phi_x \cos \phi_+$$



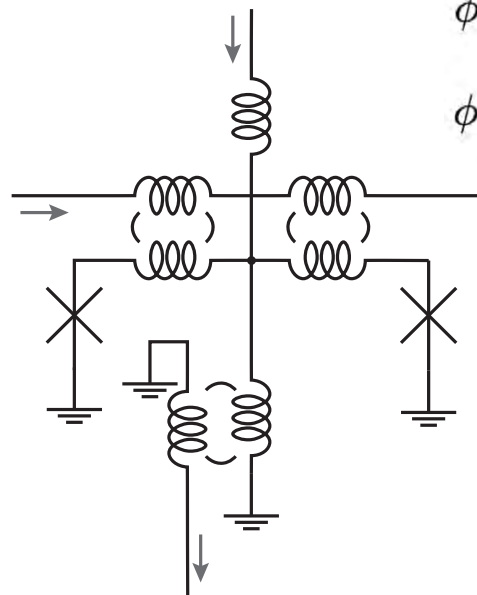
$$E_j = \frac{I_c \Phi_0}{2\pi} \rightarrow \text{energy normalization factor}$$

$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0} \rightarrow \text{normalized inductance value for } L_q$$

$$\beta_L = \frac{2\pi L_L I_c}{\Phi_0} \rightarrow \text{normalized inductance value for } L_L$$

$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2) \rightarrow \text{sum mode of JJ phases}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2) \rightarrow \text{difference mode of JJ phases}$$



QFP Analysis: Circuit Quantization

Most circuit quantization methods assume that all external flux relevant to the circuit is not time dependent → NOT true for the AQFP, which relies on time-dependent external flux for its state change, so we will follow method from [1]

Circuit quantization workflow:

1. Write down Lagrangian in terms of branch fluxes ($\Phi_{b1}, \Phi_{b2}, \dots, \Phi_{bn}$) and charges ($\dot{\Phi}_{b1}, \dot{\Phi}_{b2}, \dots, \dot{\Phi}_{bn}$), with $\mathbf{C} = \text{diag}(C_{b1}, C_{b2}, \dots, C_{bn})$ and $\mathbf{L}^{-1} = \text{diag}(L_{b1}^{-1}, L_{b2}^{-1}, \dots, L_{bn}^{-1})$

$$\mathcal{L} = \mathcal{L}_T - \mathcal{L}_V$$

Kinetic energy stored in capacitive components Potential energy stored in inductive components

$$\mathcal{L} = \frac{1}{2} \dot{\Phi}_b^T \mathbf{C} \dot{\Phi}_b - \frac{1}{2} \Phi_{bL}^T \mathbf{L}^{-1} \Phi_{bL} + \sum_{i=1}^n \frac{\Phi_0}{2\pi} I_c \cos\left(\frac{2\pi}{\Phi_0} \Phi_{b_{J_i}}\right)$$

QFP Analysis: Circuit Quantization

Circuit quantization workflow:

2. Next, we want to find the optimal coordinates to express the Lagrangian, i.e. irrotational degrees of freedom, $\tilde{\Phi}$, and external flux factors, Φ_{ex} . So we impose two constraints through two matrix operations

Flux quantization:

$$\Phi_{ex} = R\Phi_b$$

$$R_{ij} = \begin{cases} 1 & \text{if } \Phi_{b,j} \text{ is enclosed in } \Phi_{ex,i} \text{ loop with same orientation} \\ -1 & \text{if } \Phi_{b,j} \text{ is enclosed in } \Phi_{ex,i} \text{ loop with opposite orientation} \\ 0 & \text{if } \Phi_{b,j} \text{ is not enclosed } \Phi_{ex,i} \text{ loop} \end{cases}$$

Kirchoff's voltage law:

$$\tilde{\Phi} = M\Phi_b$$

And M is further set by the irrotational constraint to ensure that result does not depend on $\dot{\Phi}_{ex}$, to match time-independent solutions

$$\longrightarrow RC^{-1}M^T = 0$$

QFP Analysis: Circuit Quantization

Circuit quantization workflow:

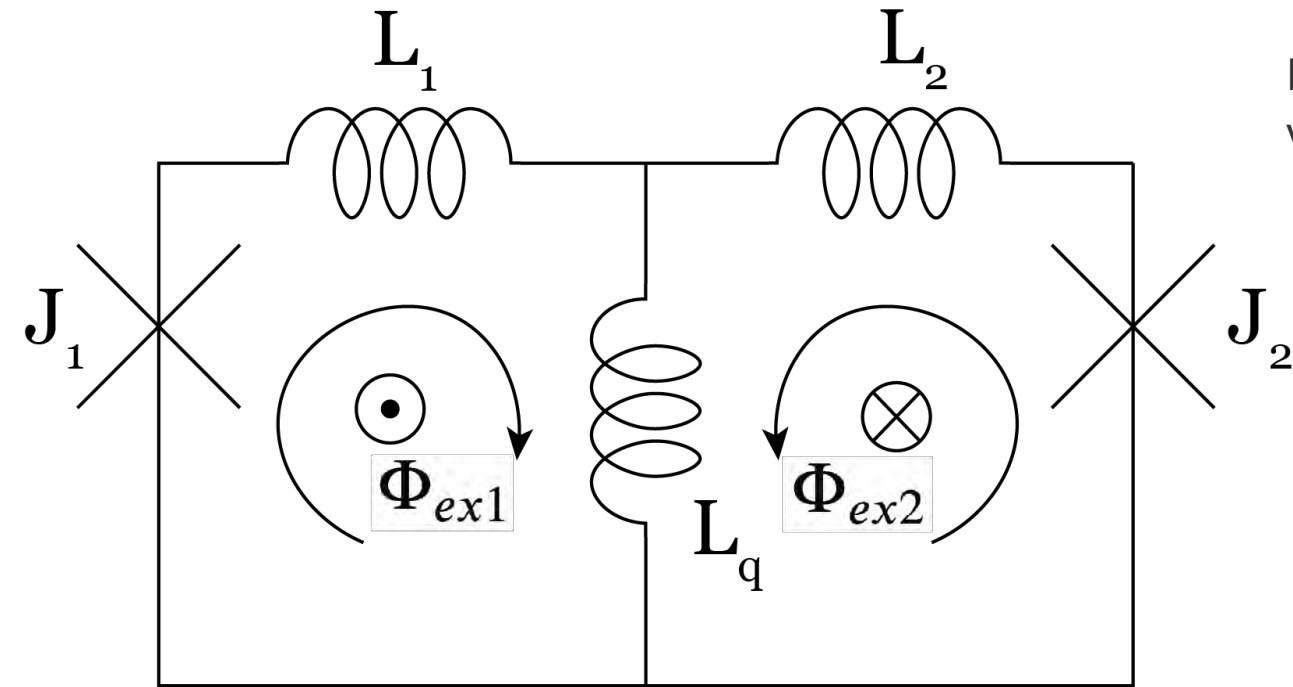
2. Then you can express the Lagrangian in terms of dynamical degrees of freedom with simple substitution $\Phi_b = \mathbf{M}_+^{-1} \tilde{\Phi}_+$ where

$$\tilde{\Phi}_+ := \begin{pmatrix} \tilde{\Phi} \\ \Phi_x \end{pmatrix}$$

$$\mathbf{M}_+ := \begin{pmatrix} M \\ R \end{pmatrix}$$

Then it's just a Legendre transformation to derive the Hamiltonian from the Lagrangian

QFP Analysis: Circuit Quantization



branch variables $\Phi_b = \begin{pmatrix} \Phi_{J_1} \\ \Phi_{J_2} \\ \Phi_{L_1} \\ \Phi_{L_2} \\ \Phi_{L_q} \end{pmatrix} \longrightarrow$ optimized variables $\Phi_{ex} = \begin{pmatrix} \Phi_{ex1} \\ \Phi_{ex2} \end{pmatrix}$

optimized variables $\tilde{\Phi} = \begin{pmatrix} \tilde{\Phi}_1 \\ \tilde{\Phi}_2 \\ \tilde{\Phi}_3 \end{pmatrix}$

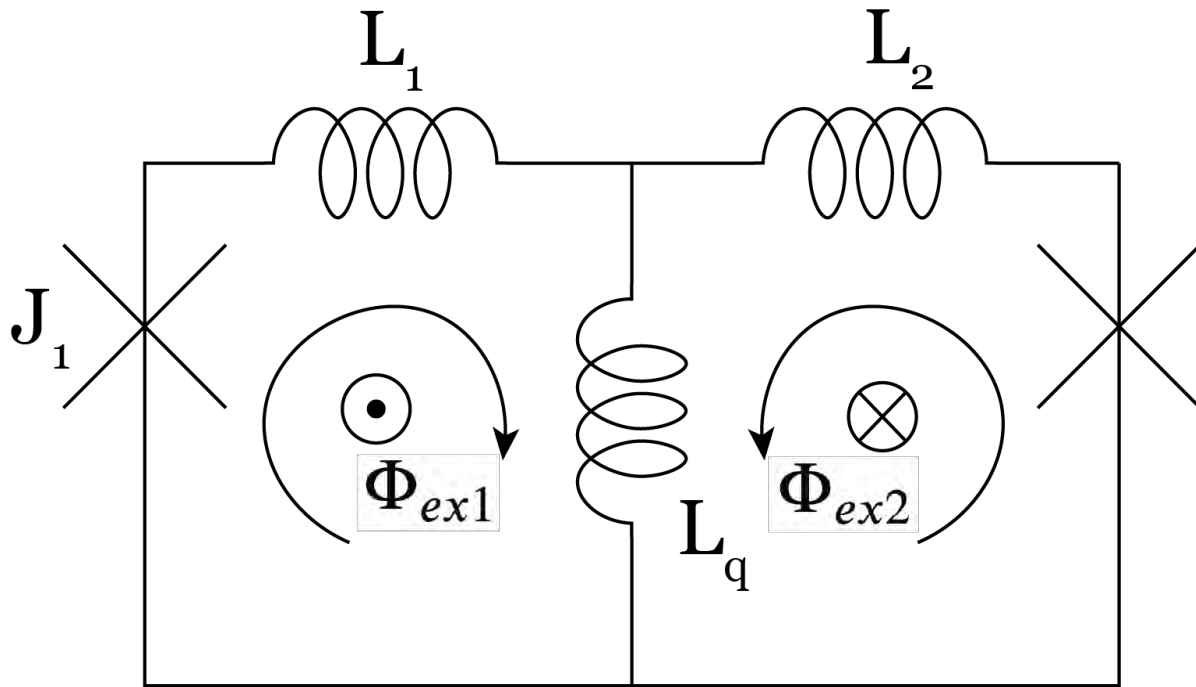
Flux quantization constraint

$$R = \begin{bmatrix} 1 & 0 & -1 & 1 & 0 \\ 0 & 1 & 1 & 0 & -1 \end{bmatrix}$$

Irrotational constraint $CM_{i1} + M_{i3} - M_{i5} = 0$
 $CM_{i2} - M_{i4} + M_{i5} = 0$

$$\longrightarrow M = \begin{bmatrix} 1/2 & 1/2 & \frac{1}{2}C & \frac{3}{2}C & C \\ -1/2 & 1/2 & \frac{3}{2}C & \frac{3}{2}C & C \\ 0 & 0 & 1 & 1 & 1 \end{bmatrix} \xrightarrow{\lim_{C \rightarrow 0} M} M_+ = \begin{bmatrix} 1/2 & 1/2 & 0 & 0 & 0 \\ -1/2 & 1/2 & 0 & 0 & 0 \\ 0 & 0 & 1 & 1 & 1 \\ 1 & 0 & 1 & 0 & -1 \\ 0 & 1 & 0 & -1 & 1 \end{bmatrix}$$

QFP Analysis: Circuit Quantization



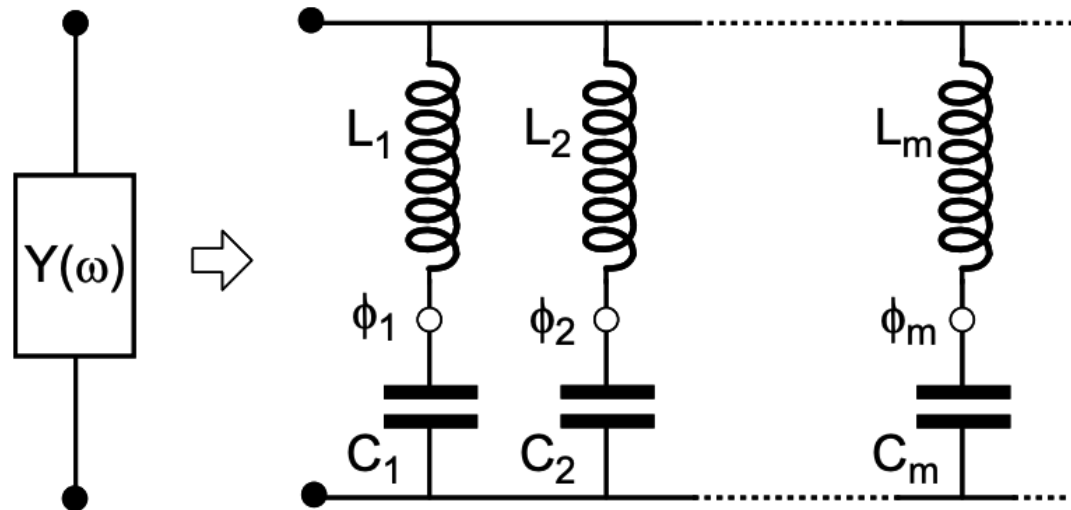
$$\mathbf{J}_2 \begin{pmatrix} \Phi_{J_1} \\ \Phi_{J_2} \\ \Phi_{L_1} \\ \Phi_{L_2} \\ \Phi_{L_q} \end{pmatrix} = \begin{pmatrix} \tilde{\Phi}_1 - \tilde{\Phi}_2 \\ \tilde{\Phi}_1 + \tilde{\Phi}_2 \\ \frac{1}{3}(-\tilde{\Phi}_1 + \tilde{\Phi}_2 + \tilde{\Phi}_3 + 2\Phi_{ex1} + \Phi_{ex2}) \\ \frac{1}{3}(3\tilde{\Phi}_1 + \tilde{\Phi}_2 + \tilde{\Phi}_3 - \Phi_{ex1} - 2\Phi_{ex2}) \\ \frac{1}{3}(-2\tilde{\Phi}_2 + \tilde{\Phi}_3 - \Phi_{ex1} + \Phi_{ex2}) \end{pmatrix}$$

Usually $\Phi_{ex1} = \Phi_{ex2}$

$$\begin{aligned}
 \mathcal{L} = & \frac{1}{2} C_j (\dot{\tilde{\Phi}}_1^2 + \dot{\tilde{\Phi}}_2^2) \\
 & - \frac{1}{9L_1} (-\tilde{\Phi}_1 + \tilde{\Phi}_2 + \tilde{\Phi}_3 + 3\Phi_{ex})^2 \\
 & - \frac{1}{9L_2} (3\tilde{\Phi}_1 + \tilde{\Phi}_2 + \tilde{\Phi}_3 - 3\Phi_{ex})^2 \\
 & - \frac{1}{9L_q} (-2\tilde{\Phi}_2 + \tilde{\Phi}_3)^2 \\
 & + E_J \cos(\tilde{\varphi}_1 - \tilde{\varphi}_2) + E_J \cos(\tilde{\varphi}_1 + \tilde{\varphi}_2)
 \end{aligned}$$

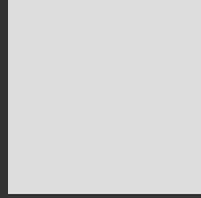
Next Steps

- Add dissipation to the circuit: extend the circuit Hamiltonian with the Caldeira-Leggett model for admittance to represent a dampening resistor in parallel with the JJ





Fundamental Physical Limits of Computation



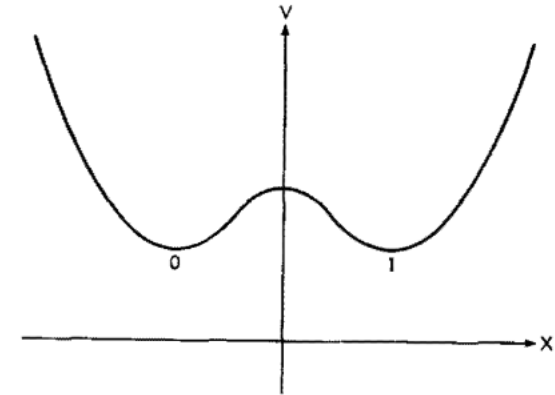
CONTENTS

- Landauer Limit
- Reversible Computing
 - Reversible Computing in AQFP
- Szilard Engine
 - Experimental Szilard Engine
 - “AQFP” Szilard Engine

Landauer Limit

The minimum energy requires to erase one bit of information is set by

$$E \geq k_b T \ln(2)$$



- Note that this only applies to computational information that is correlated with other available information, as opposed to be random and independent

Reversible Computing



- Logically Reversible :
 - Known information is not discarded from the digital state of the machine through ejection into the thermal environment
 - Every desired irreversible computation can always be embedded into a functionally equivalent reversible one [1]
- Thermodynamically Reversible :
 - The total increase in entropy from the machine's operation per useful computational operation should be extremely small, and asymptotically approach zero as the technology improves
- Bypass Landauer's limit by never erasing anything

Reversible Computing



“the ideal of physically reversible computing is by no means an easy path forward, it is the only way that general digital computing can continue to move forward indefinitely, with no clear limits in the foreseeable future—in contrast with the conventional, non-reversible computing paradigm, which is necessarily limited by Landauer’s principle” [1]

Reversible Computing

- In modern day adiabatic devices, there's typically a tradeoff between the energy dissipated and the delay interval required to carry out a primitive digital operation

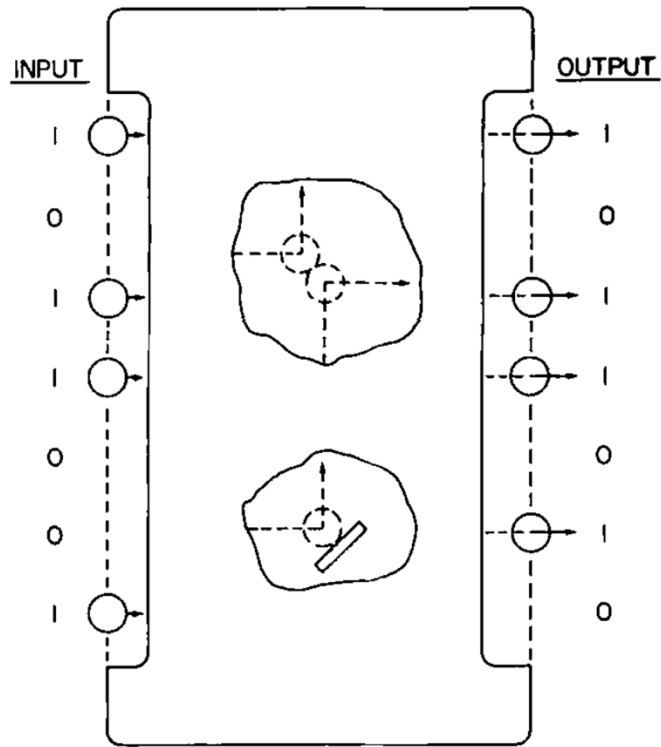
- dissipation-delay product (DdP):

$$E_{diss} * t_{delay} = c_e$$

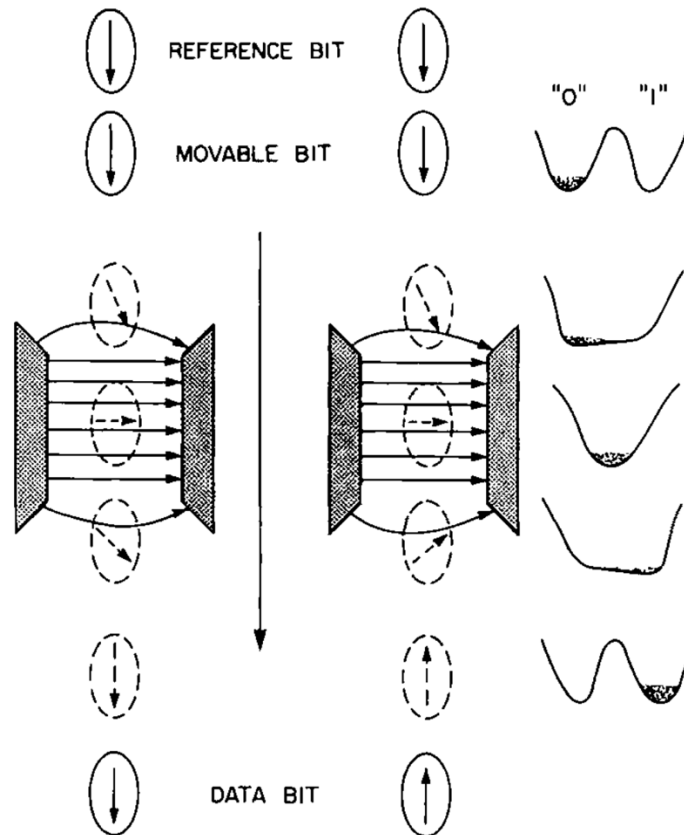
where c_e is the energy coefficient of the technology, or the dissipation-delay constant

- there are no known technology-independent boundaries on the dissipation-delay constant

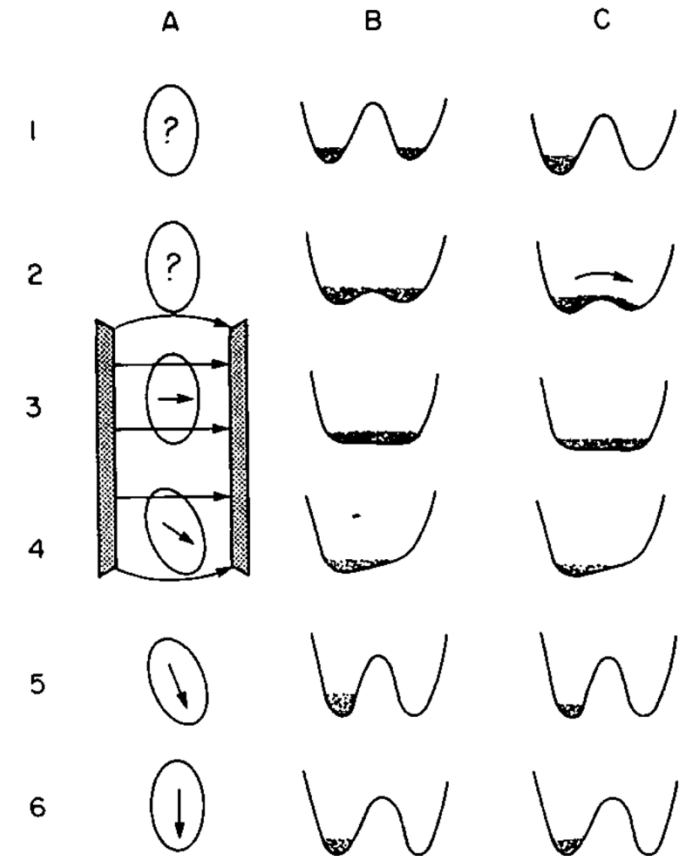
Reversible Computing: Toy Examples



Logically reversible ballistic computer
The input is always conserved in the output

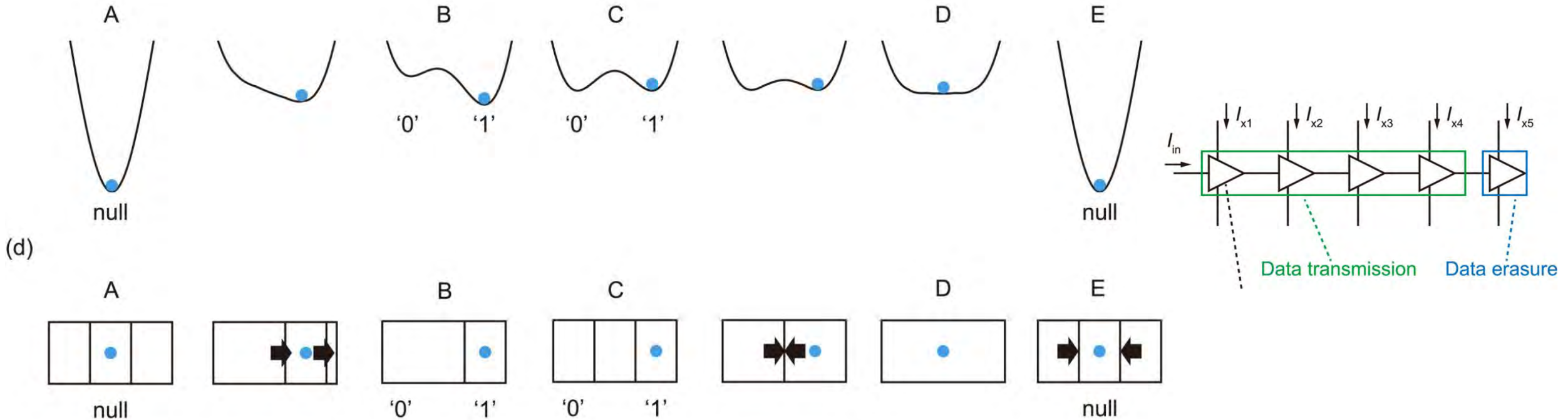


Reversible copying using a one-domain ferromagnet



Erasure of bistable one-domain ferromagnet

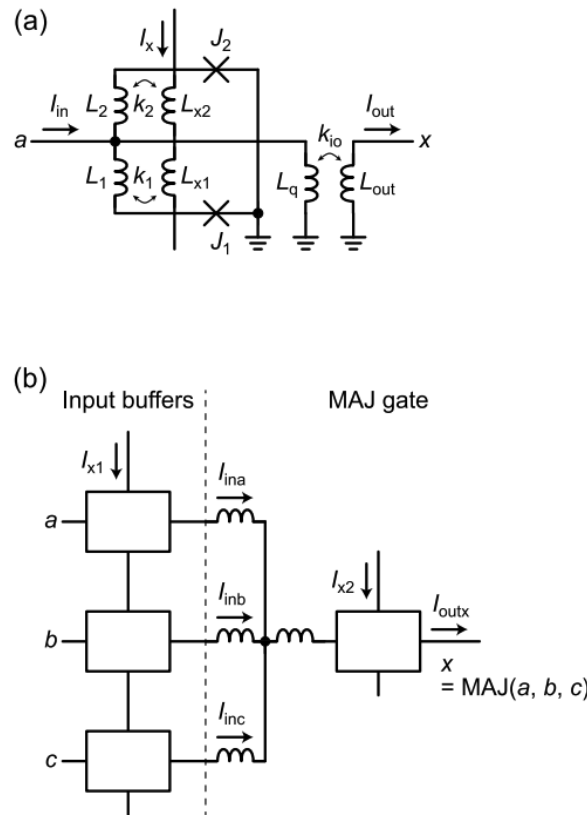
Reversible Computing in AQFP



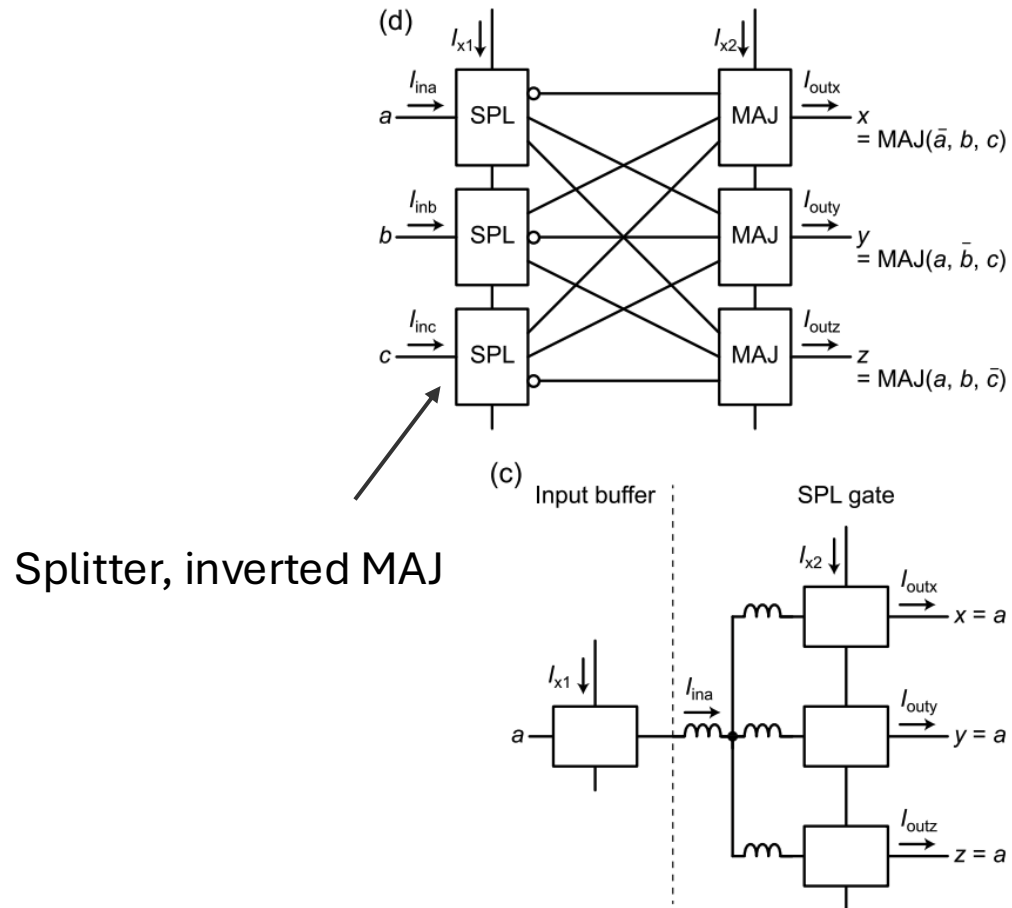
The erasure comes whenever the QFP is not balance on both input and output, i.e. where it appears in the chain

AQFP Reversible Computing

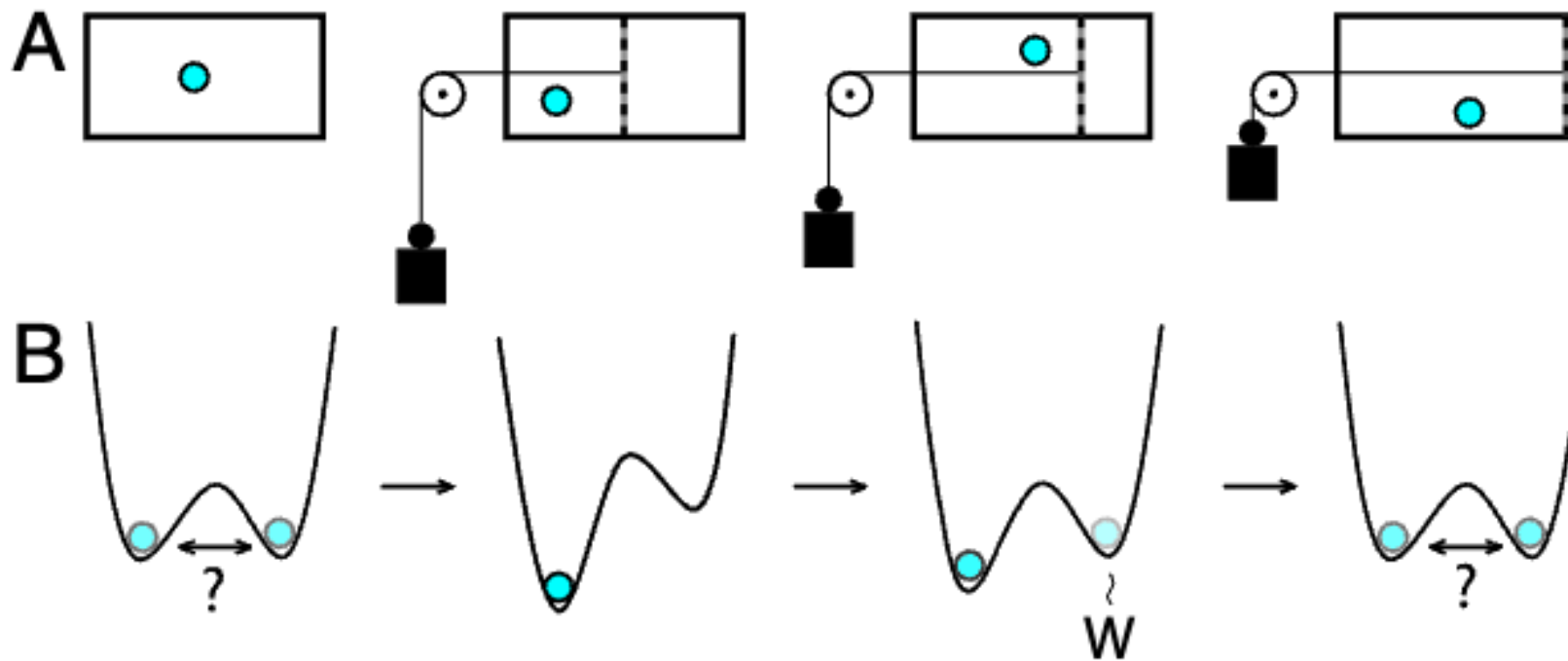
AQFP irreversible logic gates:



RQFP reversible logic gates:

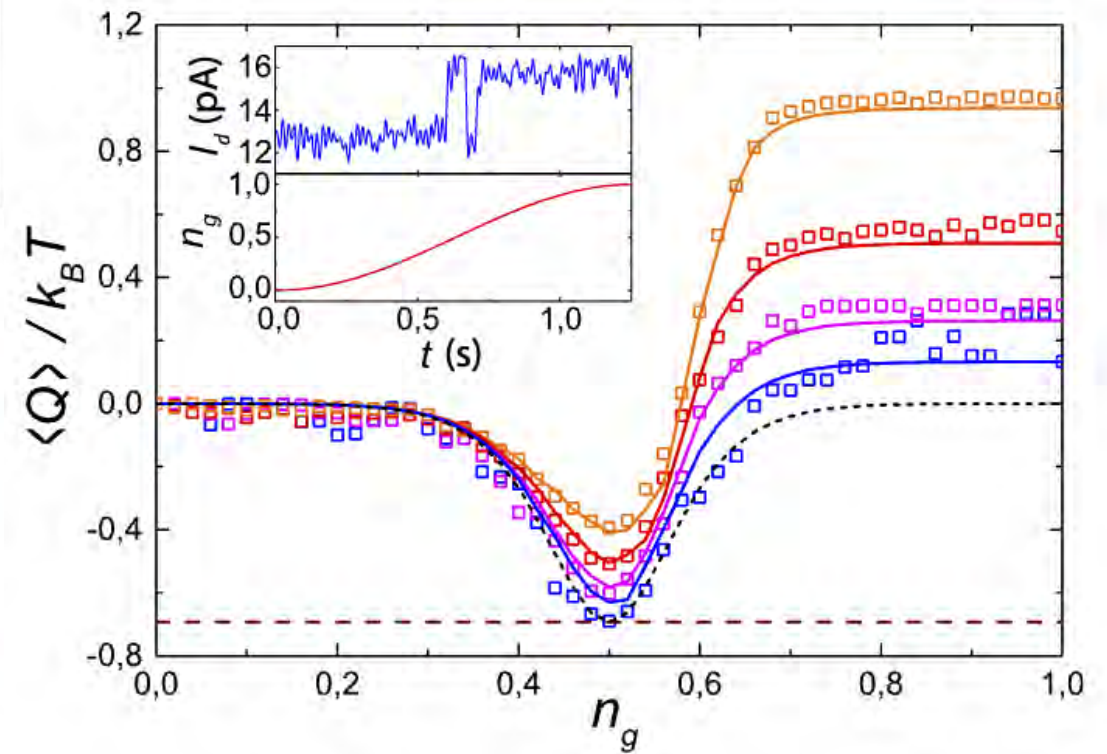
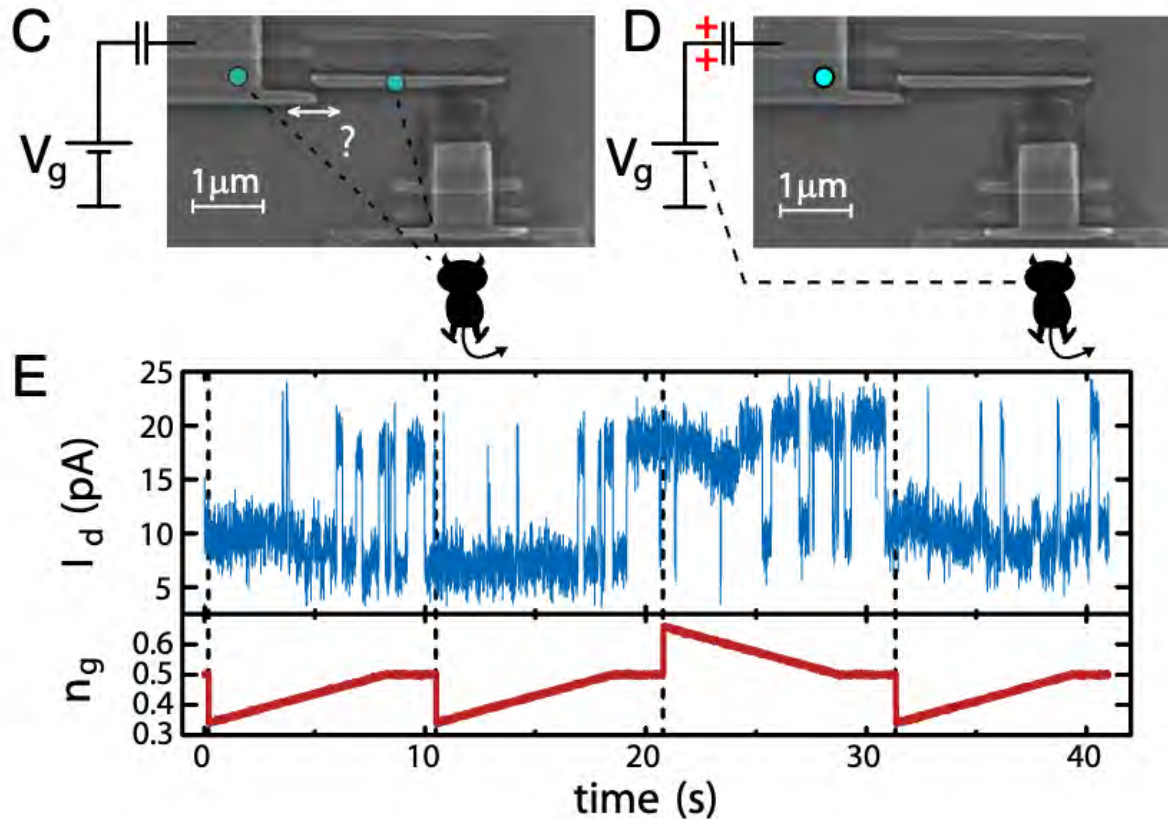


Szilard Engine – Thought Experiment

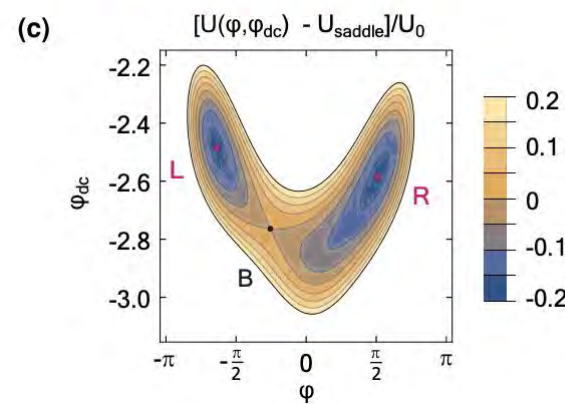
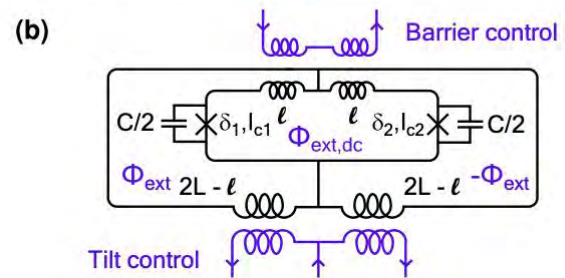


A Szilard engine uses the information about the location of a bit in a box to extract $k_b T \ln(2)$ of work

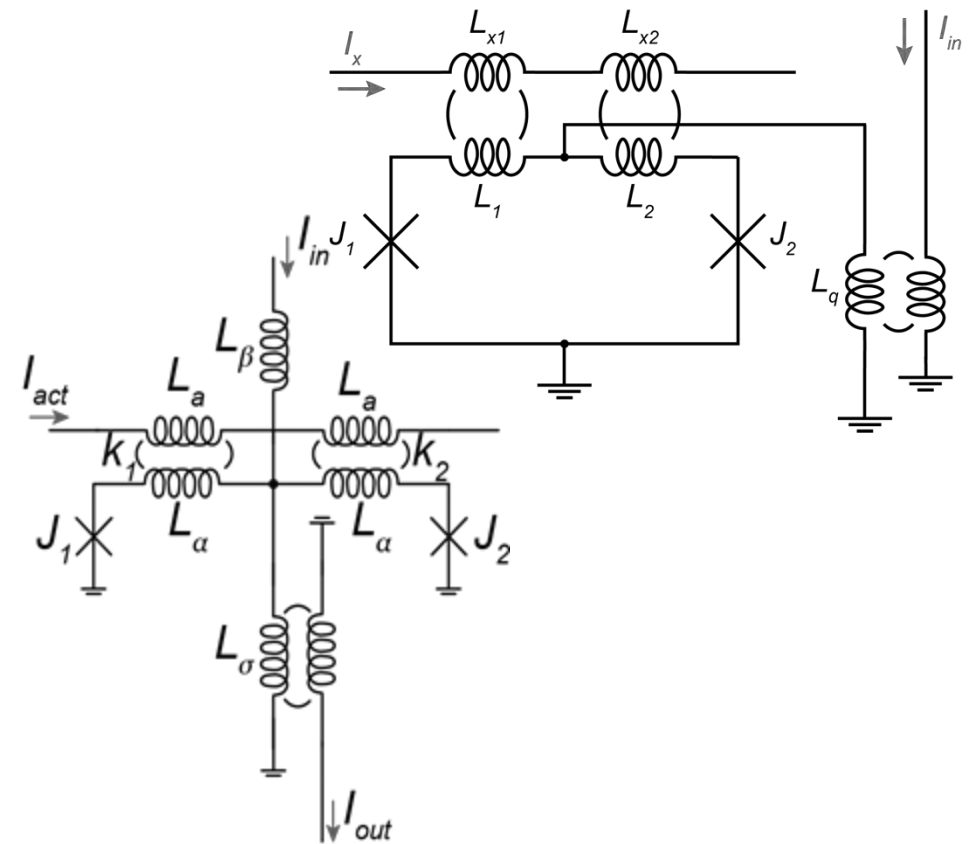
Single electron Szilard Engine



“AQFP” Szilard Engine



QFP!



$$H = \frac{Q^2}{2C} + \frac{Q_{dc}^2}{C/2} + U_0 f(\varphi, \varphi_{dc}),$$

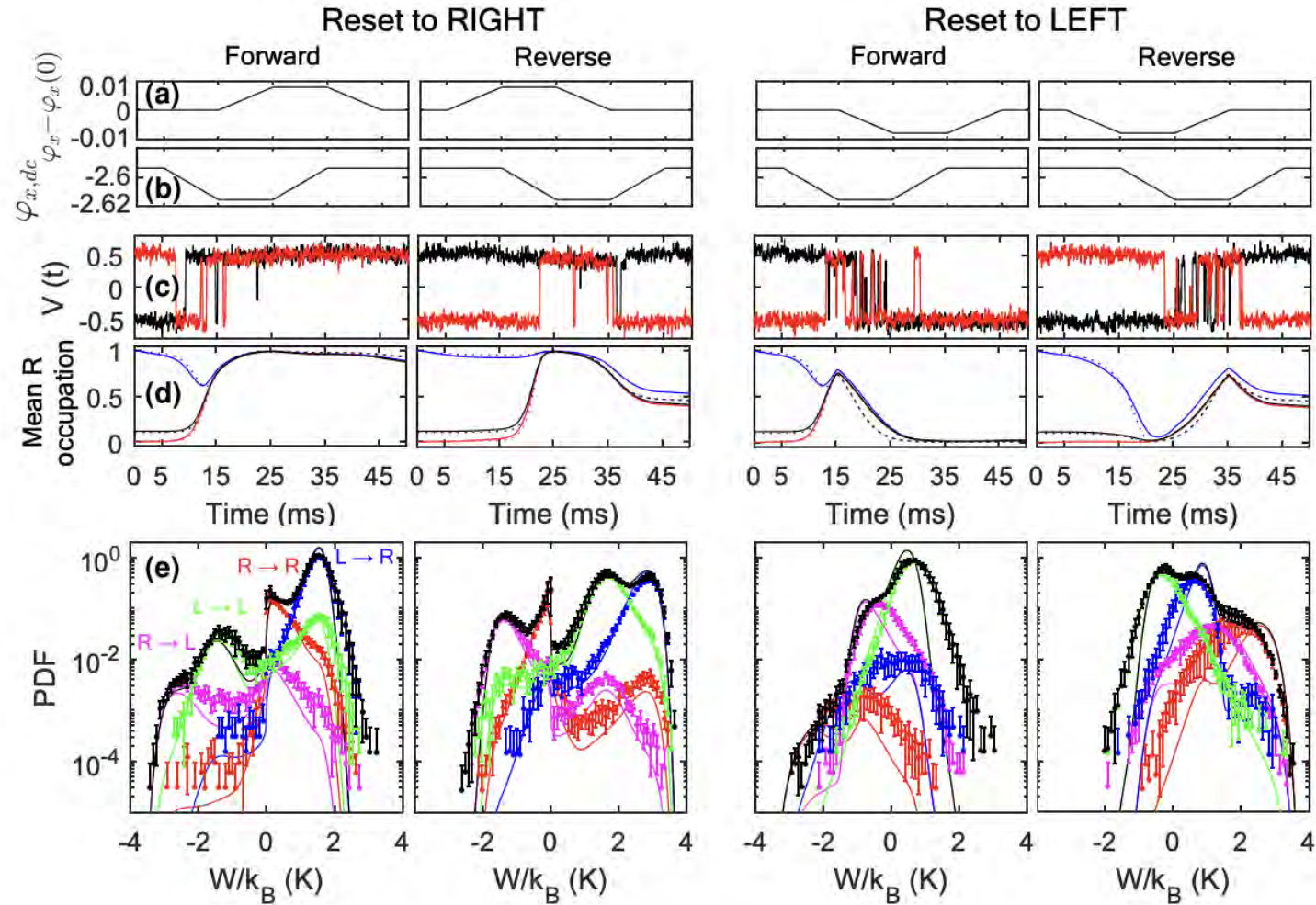
$$f(\varphi, \varphi_{dc}) = \frac{1}{2}(\varphi - \varphi_x)^2 + \frac{\gamma}{2}(\varphi_{dc} - \varphi_{x,dc})^2$$

$$+ \beta_L \cos \frac{\varphi_{dc}}{2} \cos \varphi + \delta \beta \sin \frac{\varphi_{dc}}{2} \sin \varphi.$$

“AQFP” Szilard Engine

$\varphi_x - \varphi_x(0) \rightarrow$ data signal
 $\varphi_{x,dc} \rightarrow$ activation signal

Red trace \rightarrow left well state
 Blue trace \rightarrow right well state

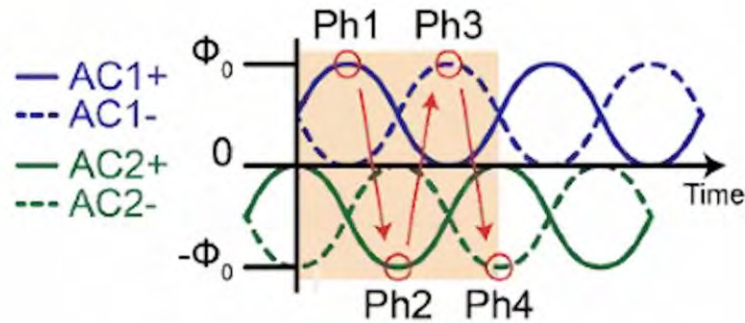
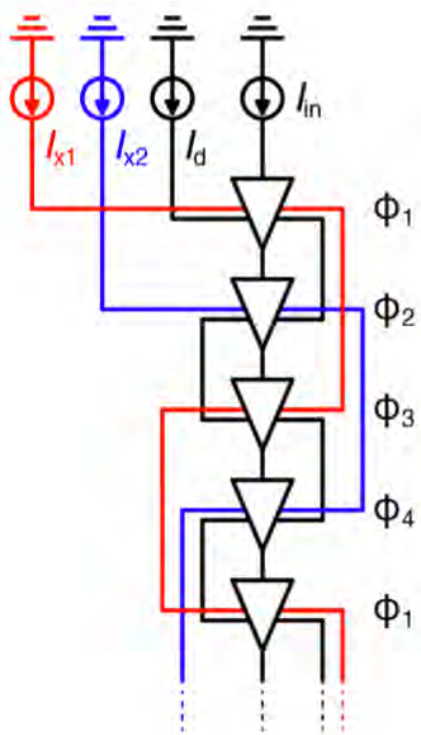




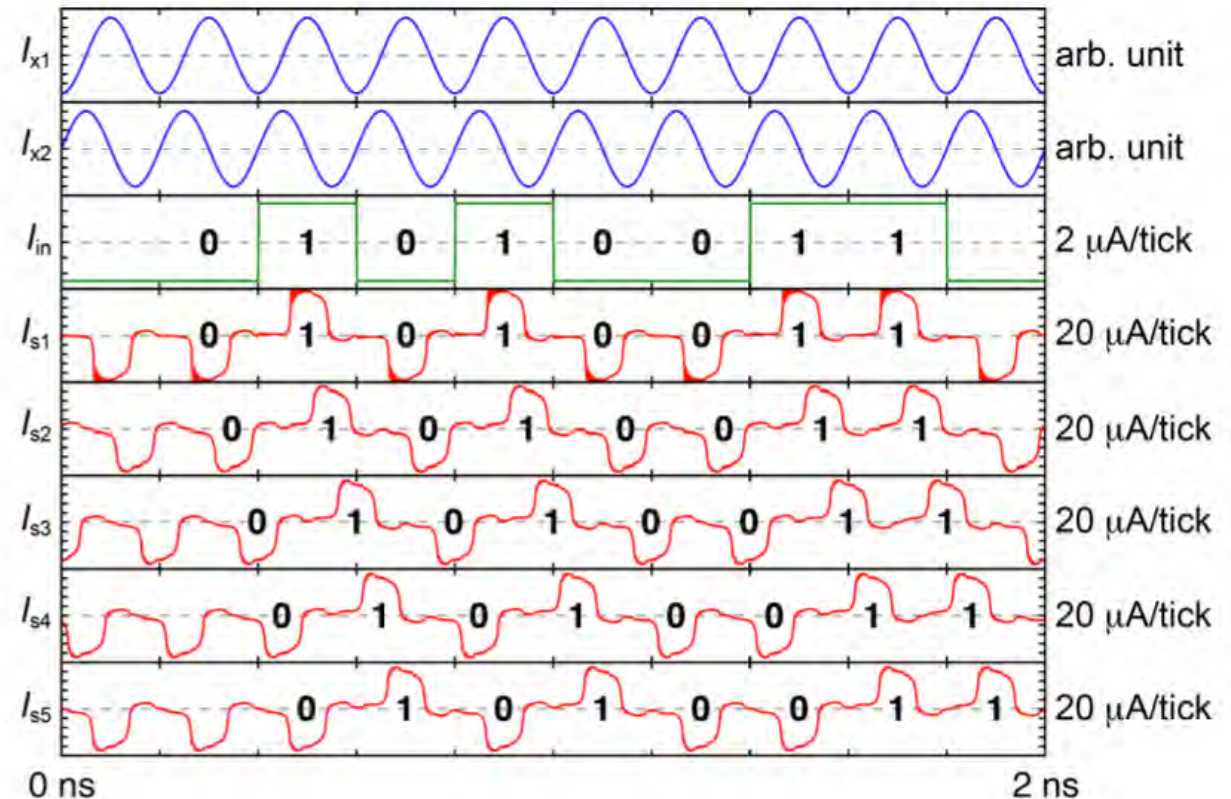
Additional Slides

AQFP Four Phase Clocking

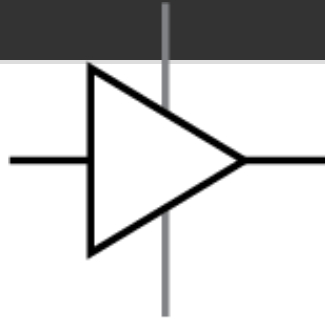
Logic states are determined by the polarity of a current pulse that is baton-passed between chains of AQFP devices, therefore a multiphase clocking scheme is needed for logic propagation.



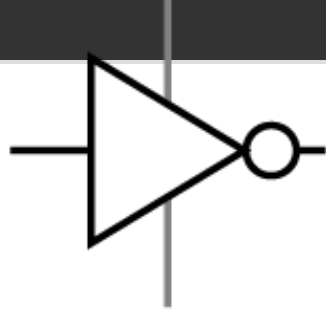
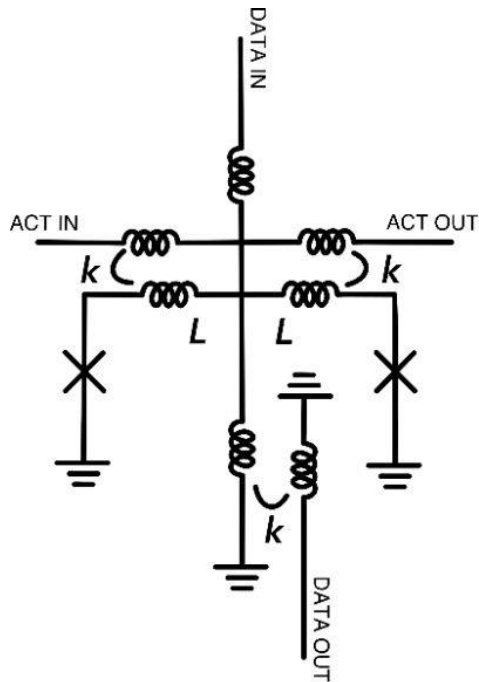
Therefore, some notion of synchronous clock is required for AQFP logic



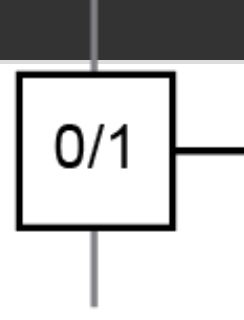
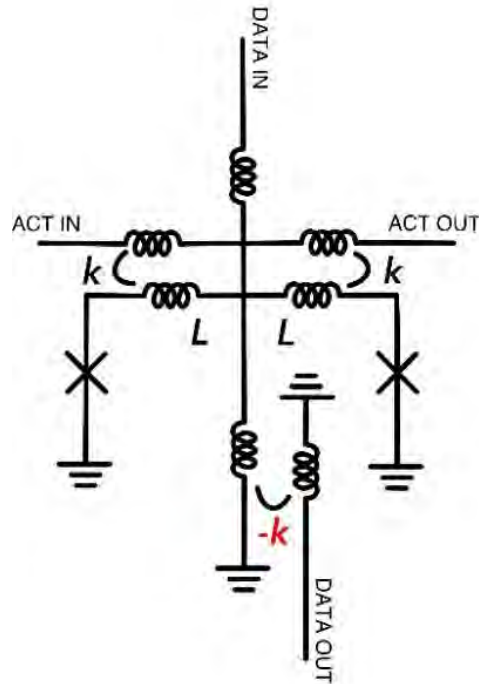
AQFP Logic Library



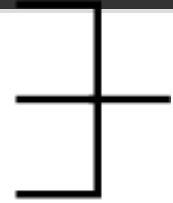
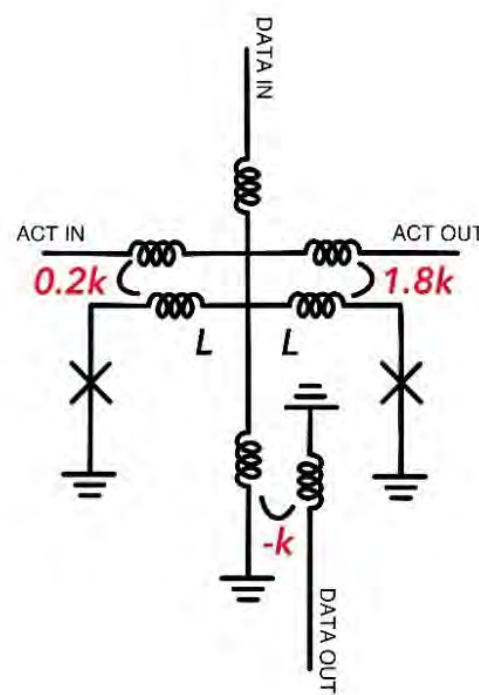
BUF



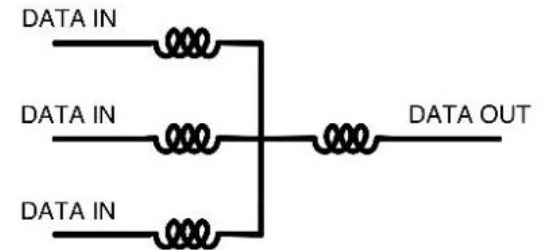
INV



CONST 0/1

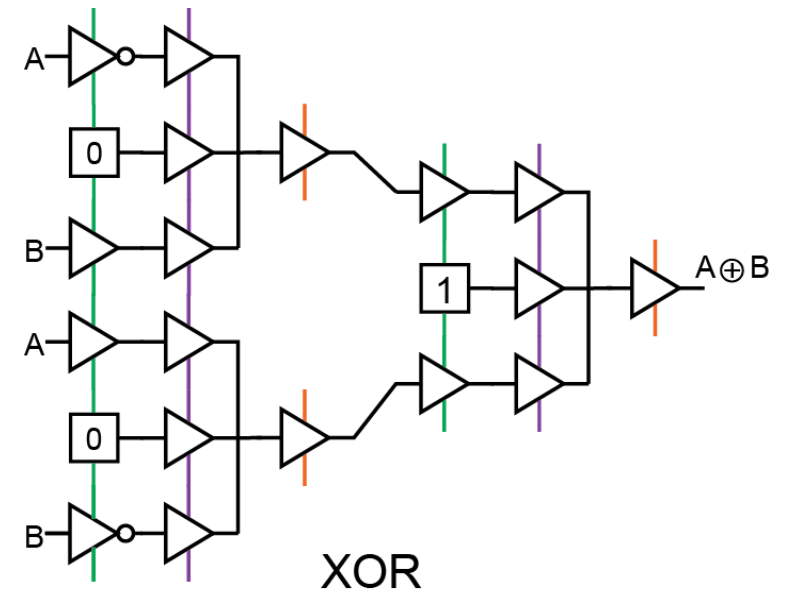
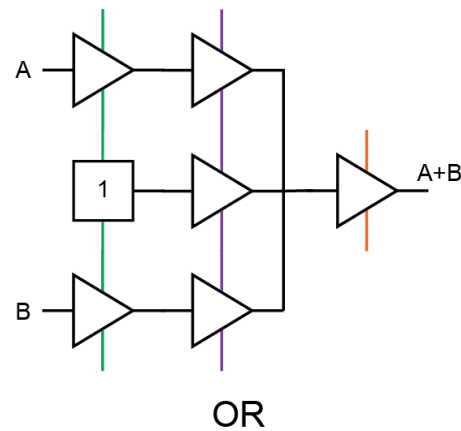
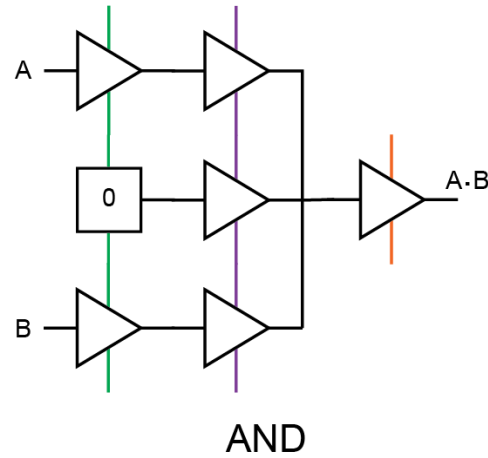
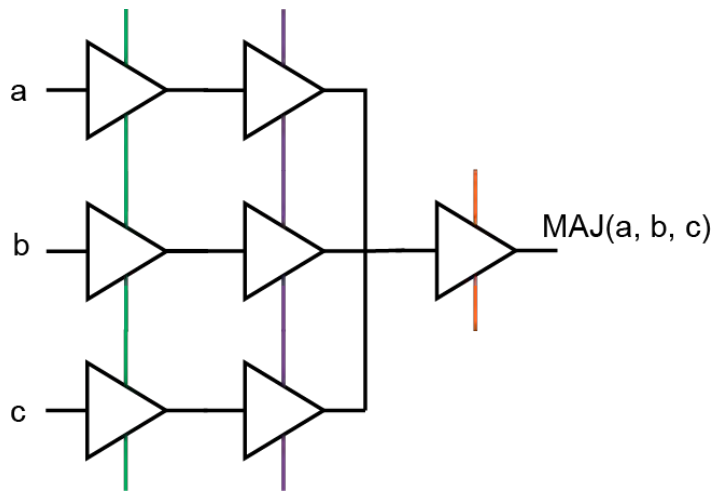


MAJ



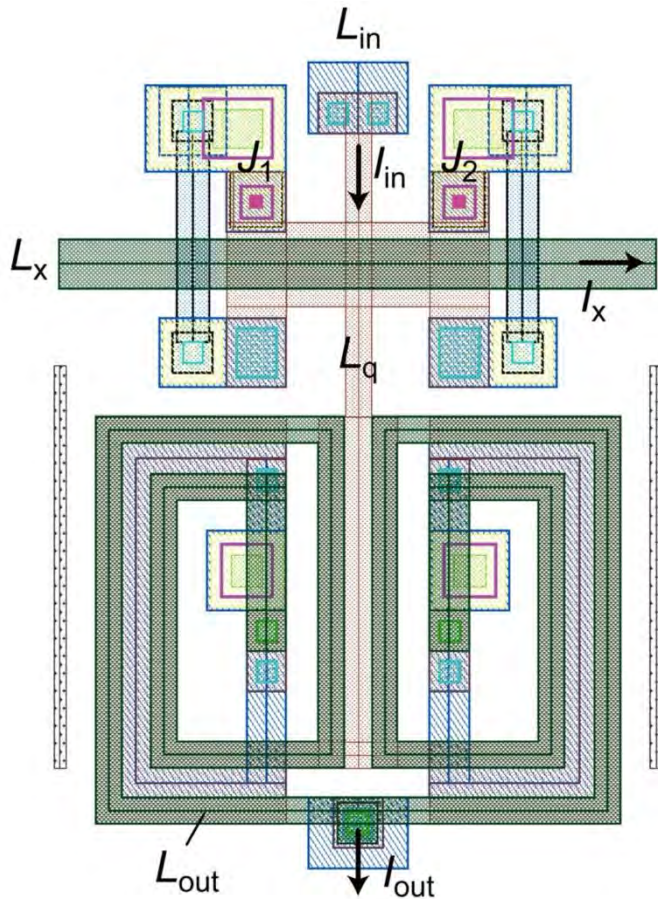
AQFP Combinational Logic

Majority gate logic:



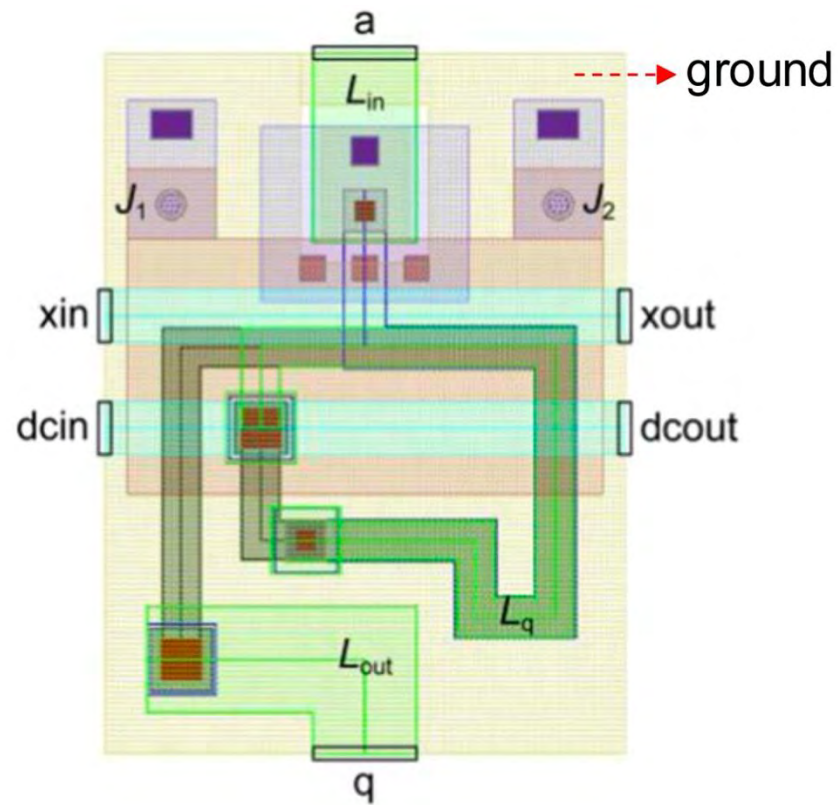
AQFP Layouts

30 μm x 40 μm , AIST-STP2 process



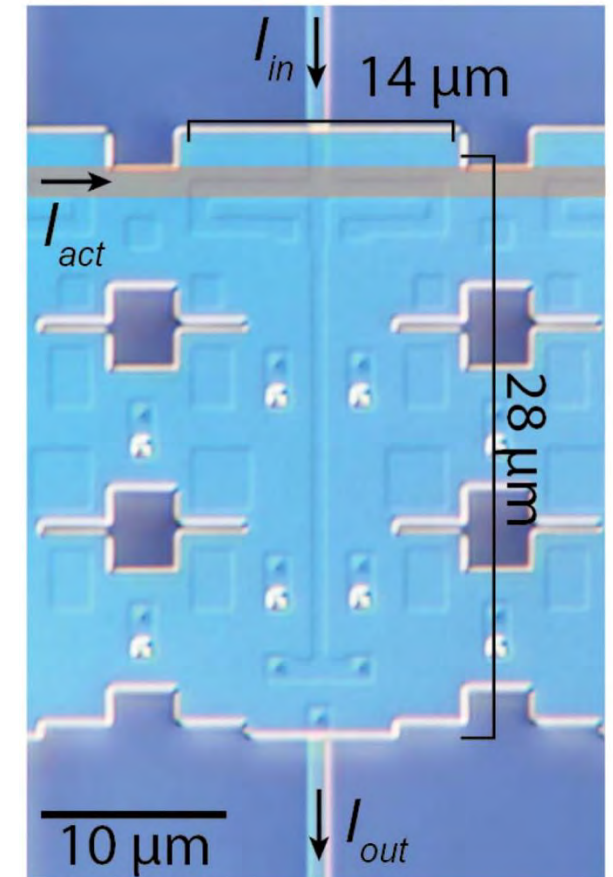
N. Takeuchi et. al., J. Appl. Phys. 117, 173912 (2015)

15 μm x 20 μm , MITLL SFQ5ee process



Y. He et. al., Supercond. Sci. Technol. 33 (2020)

MITLL SFQ5ee process



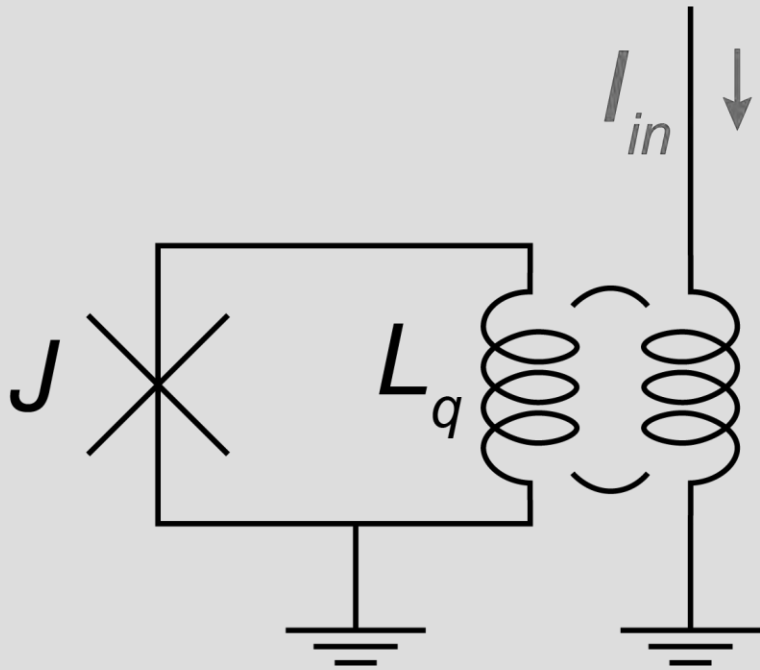
L.C. Blackburn et. al., IEEE TAS, vol. 33, 5, (2023)

AQFP Potential Energy derivation (from circuit elements instead of Lagrangian)

rf-SQUID TODO: update variable names

Superconducting Quantum Interference Device (SQUID)

rf-SQUID: single junction in a loop



$$U_{\text{rf}} = U_J + U_m$$

$$U_J = -E_j \cos \phi$$

$$U_m = \frac{E_j \phi_L^2}{2\beta_L} = \frac{1}{2} L i^2$$

$$E_j = \frac{I_c \Phi_0}{2\pi}$$
$$\beta_L = \frac{2\pi L I_c}{\Phi_0}$$

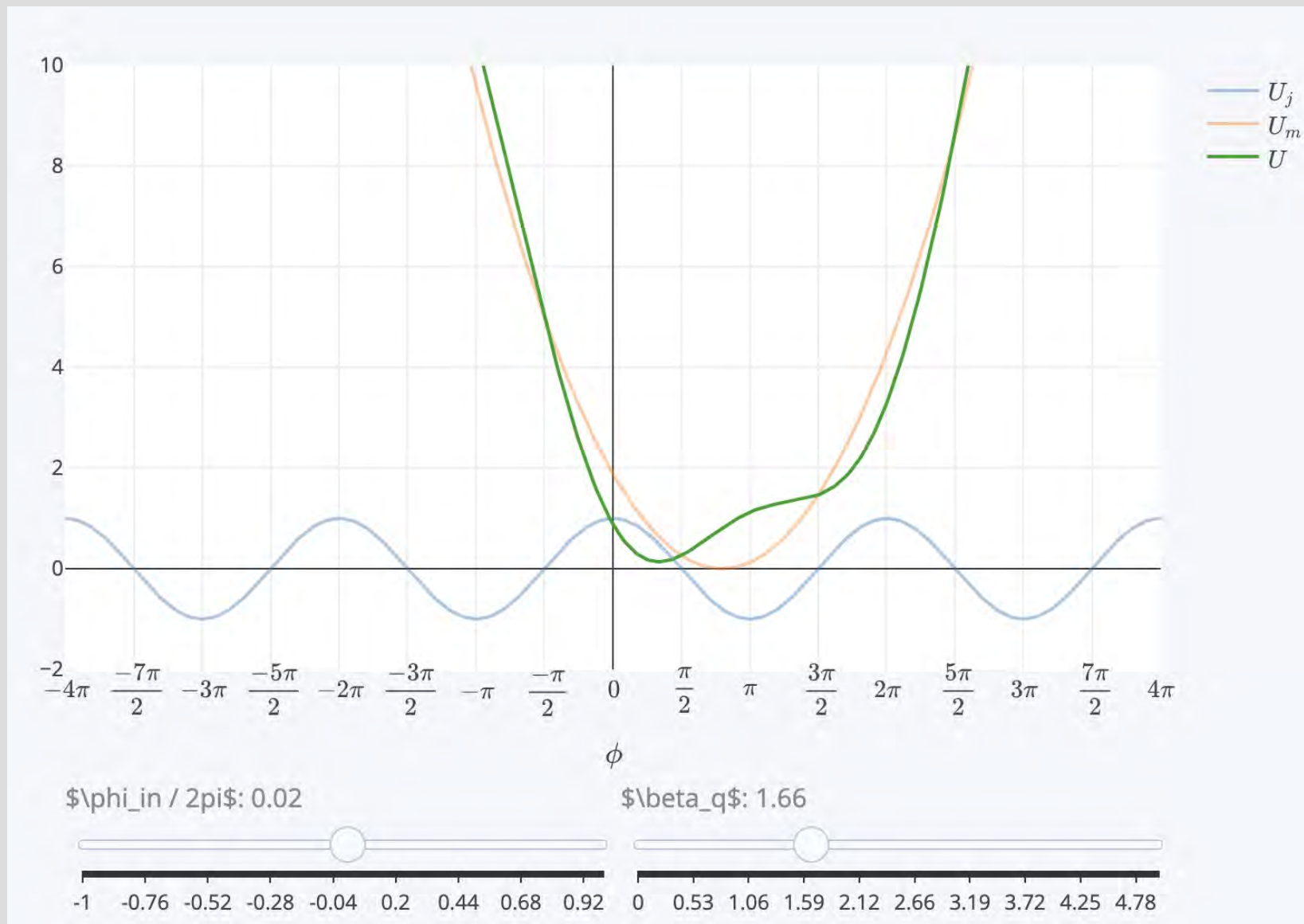
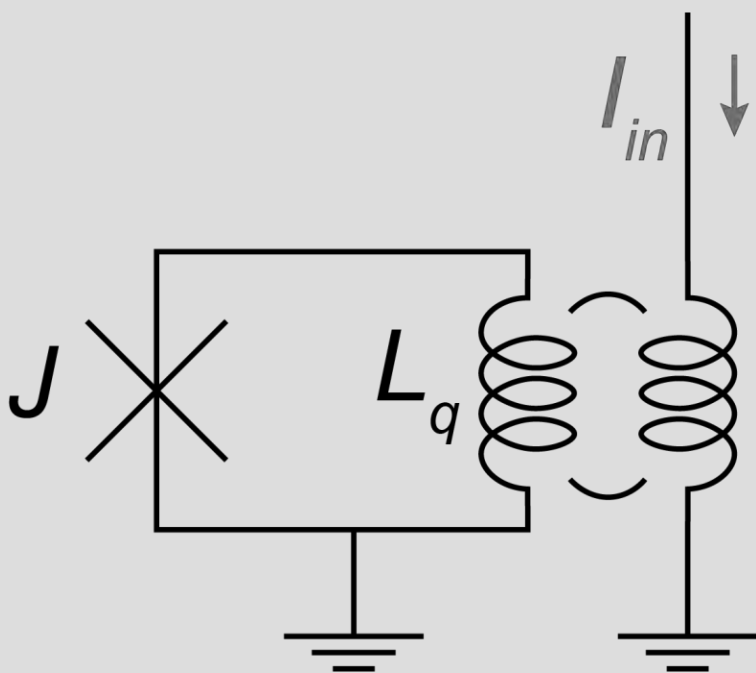
Conservation of flux / current:

$$\phi - \phi_L = \phi_b$$

$$\frac{U_{\text{rf}}}{E_j} = \frac{(\phi - \phi_b)^2}{2\beta_L} - \cos \phi$$

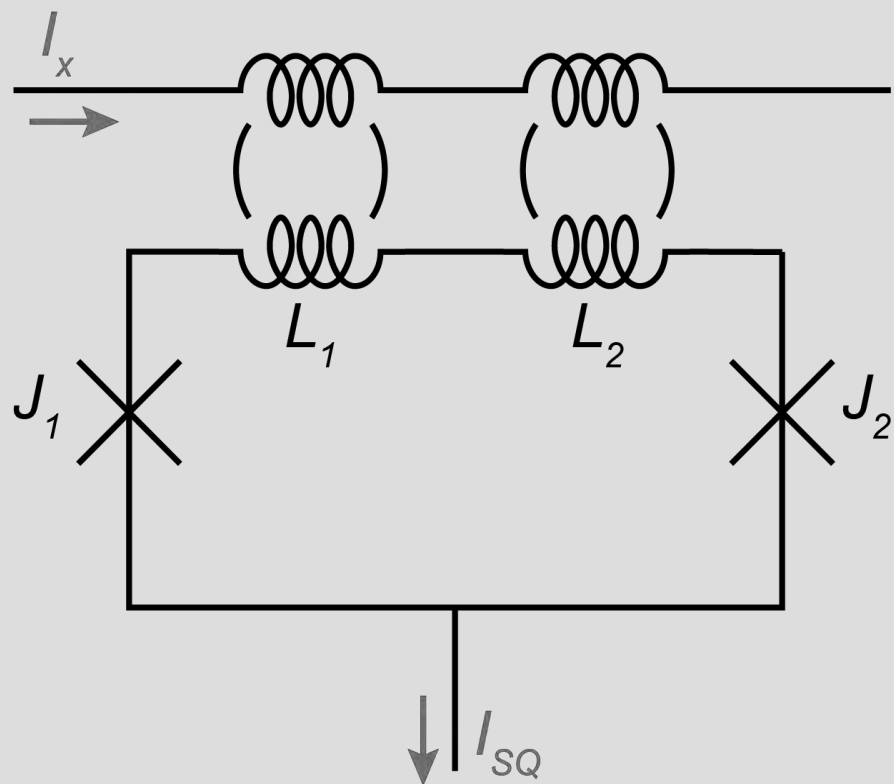
rf-SQUID

$$\frac{U_{\text{rf}}}{E_j} = \frac{(\phi - \phi_b)^2}{2\beta_L} - \cos \phi$$



dc-SQUID

dc-SQUID: two junctions inside a loop

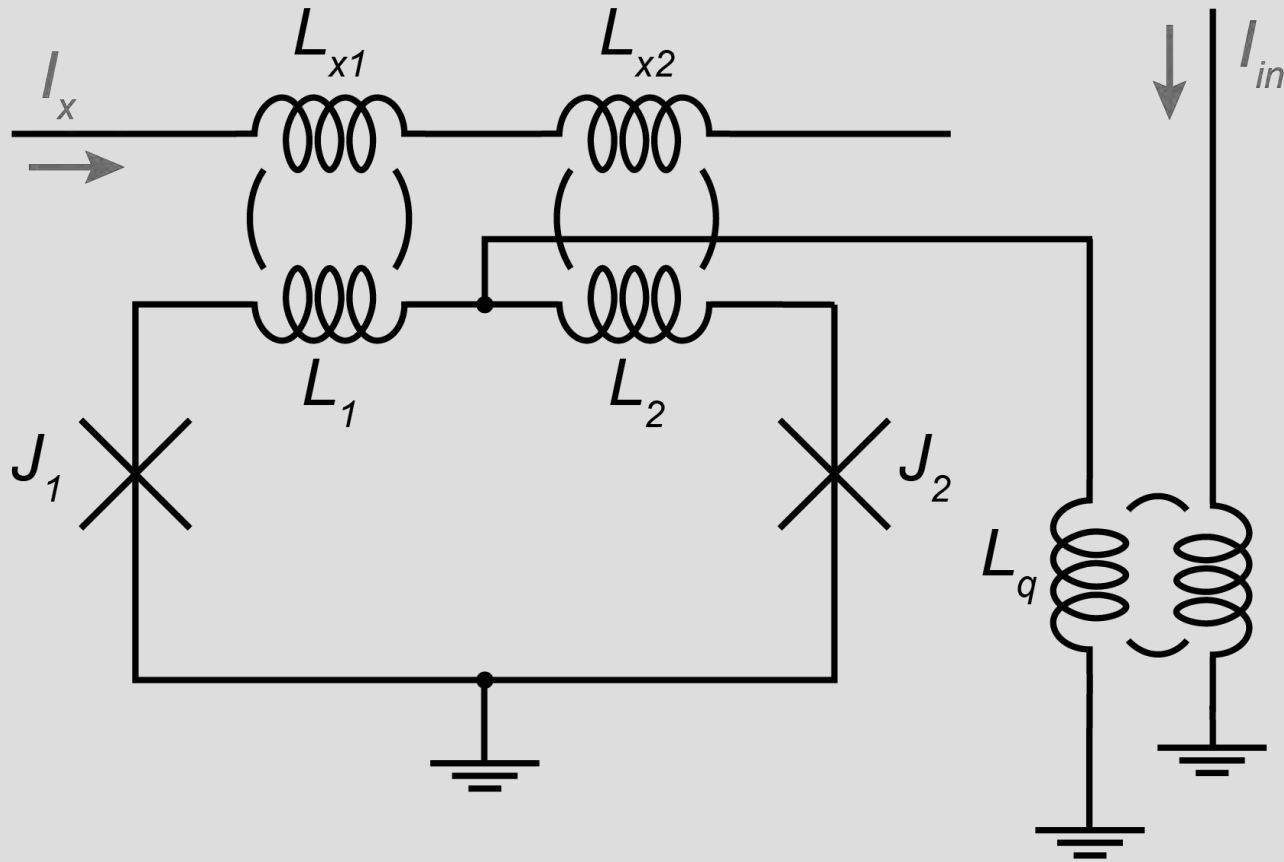


Behaves like a JJ with a tunable I_c , dependent on an externally applied flux, Φ_{ext} (in this case, I_x coupled through the transformer)

If we ignore the loop inductance and assume that both junctions are identical, the new critical current of the effective JJ is

$$I_{c,SQ} = 2I_c \cos \frac{\pi \Phi_{ext}}{\Phi_0}$$

QFP Potential

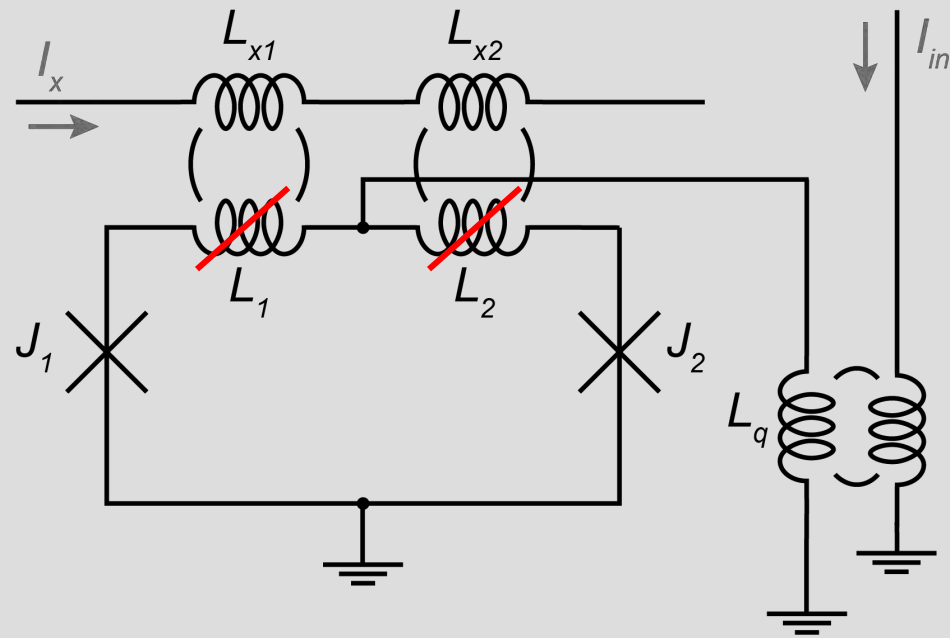


Quantum Flux Parametron (QFP) can be thought of as an rf-SQUID with the single JJ replaced by a tunable dc-SQUID

I_x : activation signal

I_{in} : data signal (input/output shares a net)

QFP Potential



$$U_{\text{qfp}} = U_J + U_m$$

To start, let's assume that L_1 and L_2 are small and their energy contributions can be ignored

$$\begin{aligned} U_J &= U_{J_1} + U_{J_2} \\ &= E_J (-\cos \phi_1 - \cos \phi_2) \\ &= -2E_J \cos \phi_+ \cos \phi_- \end{aligned}$$

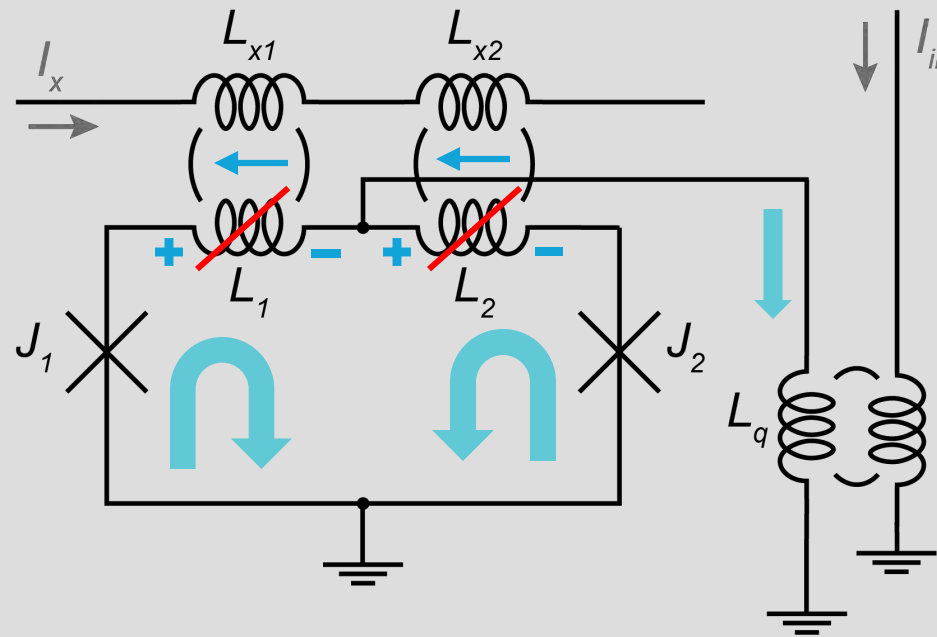
$$U_m = \frac{E_j \phi_q^2}{2\beta_q}$$

$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2)$$

$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2)$$

QFP Potential



Conservation of flux / current:

$$\phi_1 - \phi_x = \phi_2 + \phi_x = \phi_q + \phi_{in}$$

$$\rightarrow \phi_q = \phi_+ - \phi_{in}$$

$$\rightarrow \phi_- = \phi_x$$

$$U_{\text{qfp}} = U_J + U_m$$

To start, let's assume that L_1 and L_2 are small and their energy contributions can be ignored

$$\begin{aligned} U_J &= U_{J_1} + U_{J_2} \\ &= E_J (-\cos \phi_1 - \cos \phi_2) \\ &= -2E_J \cos \phi_+ \cos \phi_- \end{aligned}$$

$$U_m = \frac{E_j \phi_q^2}{2\beta_q}$$

$$\frac{U_{\text{qfp}}}{E_j} = \frac{(\phi_+ - \phi_{in})^2}{2\beta_q} - 2 \cos \phi_x \cos \phi_+$$

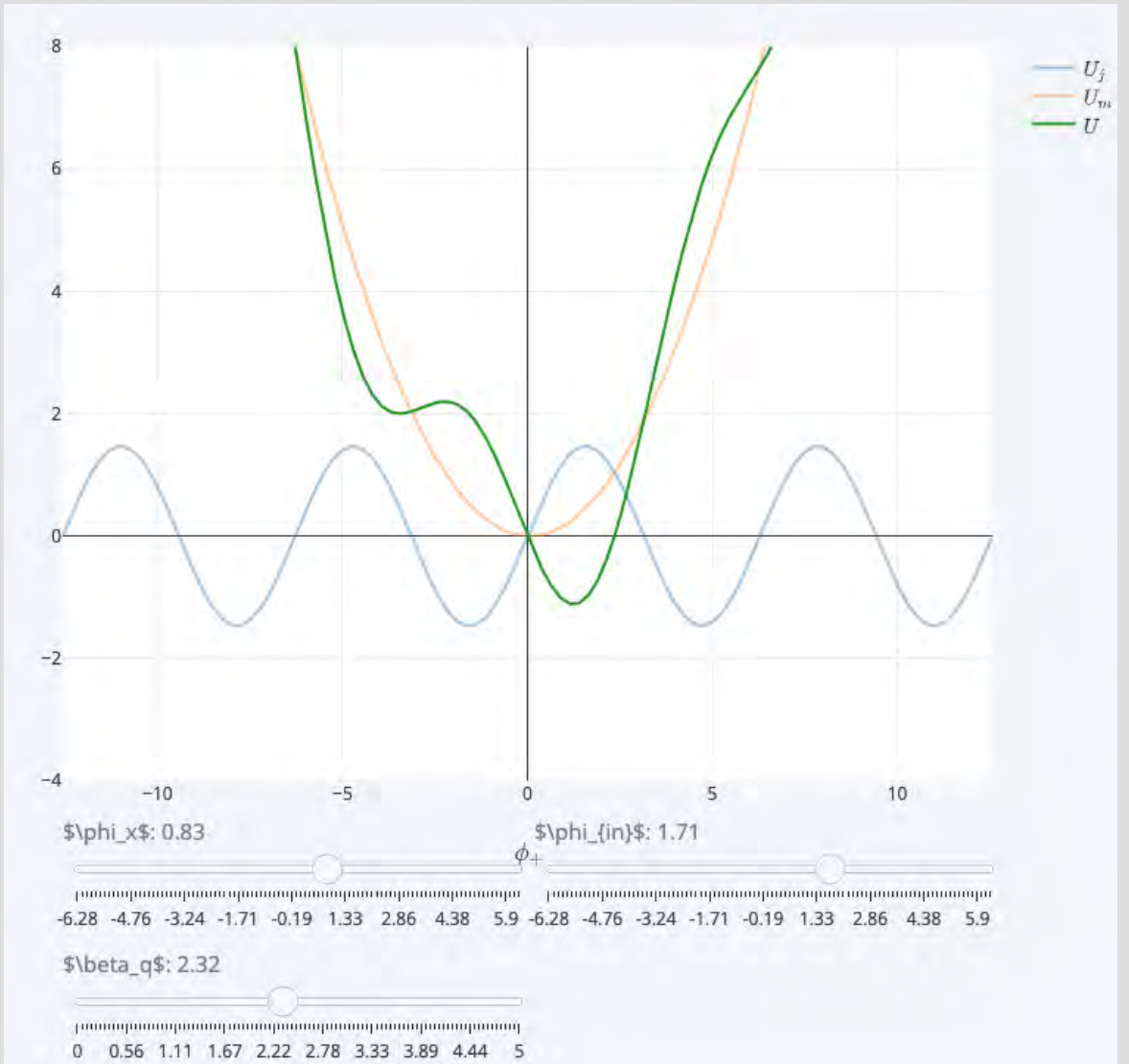
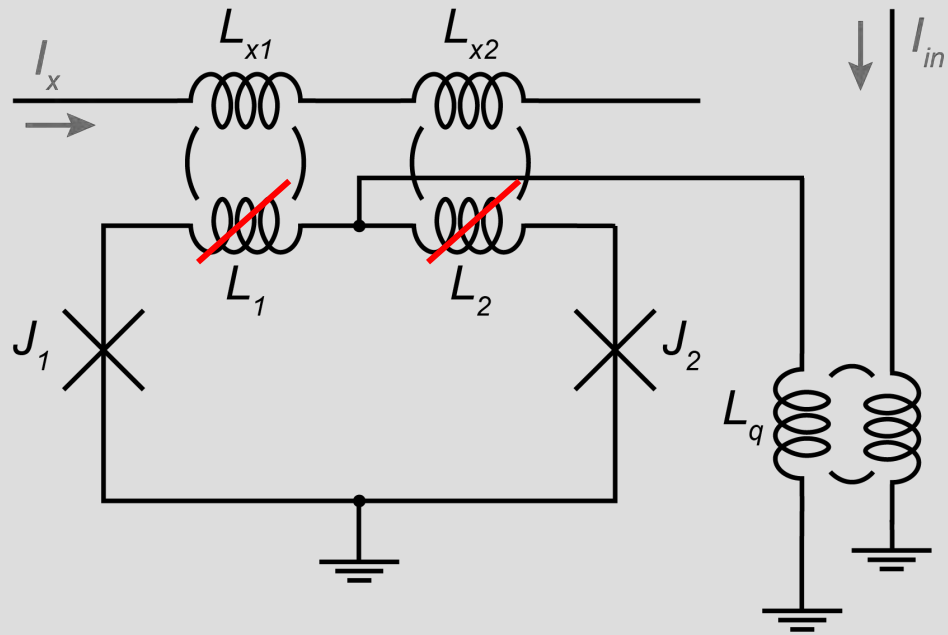
$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2)$$

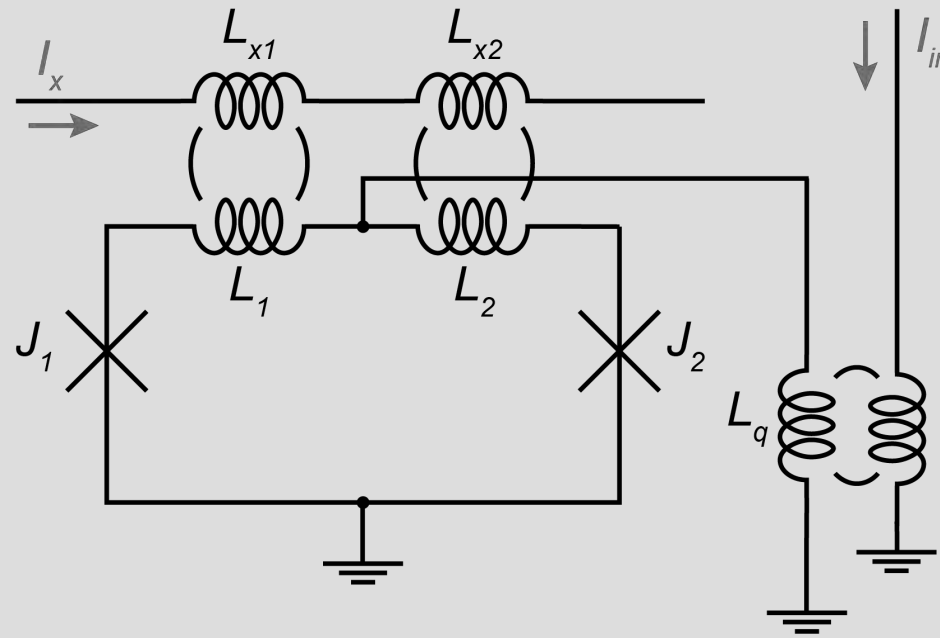
$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2)$$

QFP Potential

$$\frac{U_{\text{qfp}}}{E_j} = \frac{(\phi_+ - \phi_{\text{in}})^2}{2\beta_q} - 2 \cos \phi_x \cos \phi_+$$



QFP Potential



$$U_{\text{qfp}} = U_J + U_m$$

A more accurate QFP potential includes dc-SQUID inductors

$$U_J = -2E_J \cos \phi_+ \cos \phi_-$$

$$U_m = \frac{E_j(\phi_{L_1}^2 + \phi_{L_2}^2)}{2\beta_L} + \frac{E_j\phi_q^2}{2\beta_q}$$

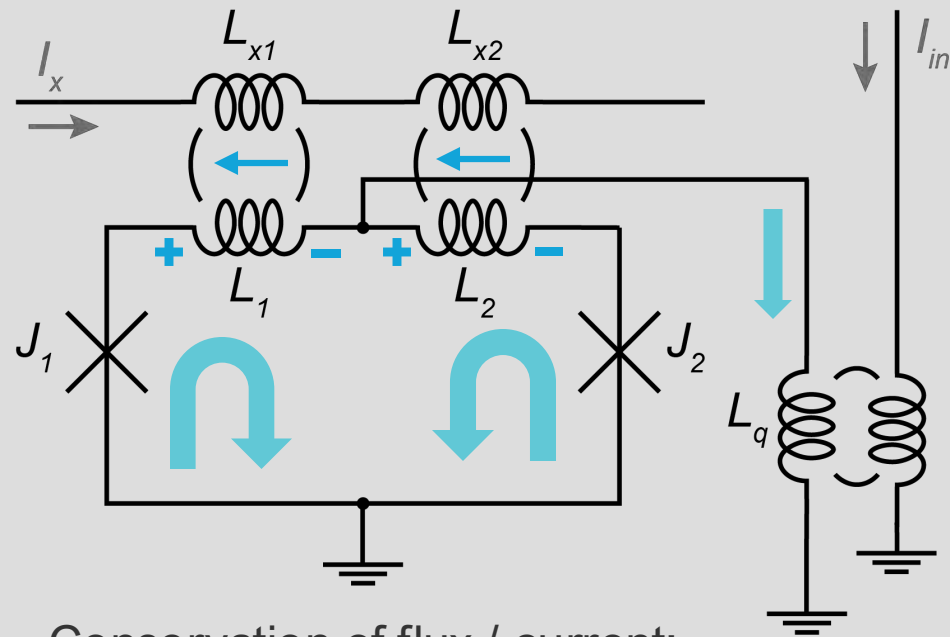
$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2)$$

$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2)$$

$$\beta_L = \frac{2\pi L I_c}{\Phi_0}$$

QFP Potential



$$U_{\text{qfp}} = U_J + U_m$$

A more accurate QFP potential includes dc-SQUID inductors

$$U_J = -2E_J \cos \phi_+ \cos \phi_-$$

$$U_m = \frac{E_j(\phi_{L_1}^2 + \phi_{L_2}^2)}{2\beta_L} + \frac{E_j\phi_q^2}{2\beta_q}$$

$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2)$$

$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2)$$

$$\beta_L = \frac{2\pi L I_c}{\Phi_0}$$

Conservation of flux / current:

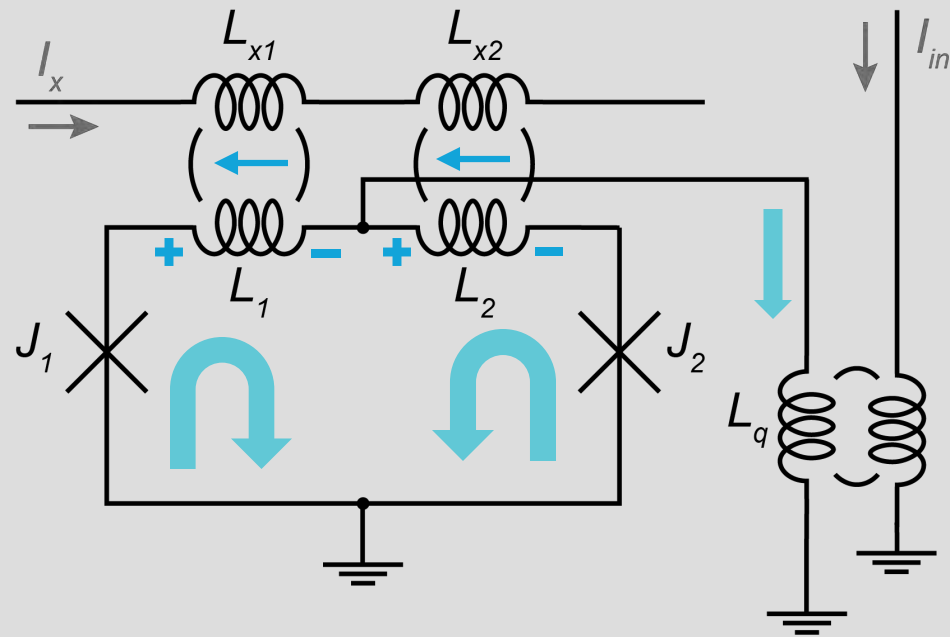
$$\phi_1 + \phi_{L_1} - \phi_x = \phi_2 + \phi_{L_2} + \phi_x = \phi_q + \phi_{\text{in}}$$

$$\rightarrow \phi_{L_1} = -[(\phi_+ - \phi_q - \phi_{\text{in}}) + (\phi_- - \phi_x)]$$

$$\rightarrow \phi_{L_2} = -[(\phi_+ - \phi_q - \phi_{\text{in}}) - (\phi_- - \phi_x)]$$

$$\rightarrow \phi_{L_1}^2 + \phi_{L_2}^2 = 2[(\phi_+ - \phi_q - \phi_{\text{in}})^2 + (\phi_- - \phi_x)^2]$$

QFP Potential



$$U_{\text{qfp}} = U_J + U_m$$

A more accurate QFP potential includes dc-SQUID inductors

$$U_J = -2E_J \cos \phi_+ \cos \phi_-$$

$$U_m = \frac{E_j(\phi_{L_1}^2 + \phi_{L_2}^2)}{2\beta_L} + \frac{E_j\phi_q^2}{2\beta_q}$$

$$\beta_q = \frac{2\pi L_q I_c}{\Phi_0}$$

$$\phi_- = \frac{1}{2}(\phi_1 - \phi_2)$$

$$\phi_+ = \frac{1}{2}(\phi_1 + \phi_2)$$

$$\beta_L = \frac{2\pi L I_c}{\Phi_0}$$

... after some approximations to remove ϕ_q and a but of algebra:

$$\frac{U_{\text{qfp}}}{E_j} \approx \frac{(\phi_+ - \phi_{\text{in}})^2}{2\beta_q + \beta_L} + \frac{(\phi_- - \phi_x)^2}{\beta_L} - 2 \cos \phi_- \cos \phi_+$$

QFP Potential

$$\frac{U_{\text{qfp}}}{E_j} \approx \frac{(\phi_+ - \phi_{\text{in}})^2}{2\beta_q + \beta_L} + \frac{(\phi_- - \phi_x)^2}{\beta_L} - 2 \cos \phi_- \cos \phi_+$$

